## BLACKFALDS CROSSING AREA STRUCTURE PLAN

NE 22-39-27-W4M TOWN OF BLACKFALDS, AB

### TRAFFIC IMPACT ASSESSMENT

Project No. 151-02471-00

Prepared for: Elkay Developments Ltd. Spire General Partner Ltd.

Date: November 28, 2016

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### CORPORATE AUTHORIZATION

This report titled "Blackfalds Crossing ASP Traffic Impact Assessment" was prepared by WSP Canada Inc. for Elkay Developments Ltd. and Spire General Partner Ltd. The guality of information, conclusions and estimates contained herein is consistent with the level of effort provided by WSP Canada Inc. and are based on: i) information available at the time of preparation, ii) data supplied by outside sources, and iii) the assumptions, conditions and qualifications set forth in this report. This report is intended to be used by Elkay Developments Ltd. and Spire General Partner Ltd. only, subject to the terms and conditions of its contract with WSP Canada Inc. Any other use of, or reliance on, this report by any third party is at that party's sole risk



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### REVISION HISTORY

VERSION	DATE	Description
1	October 8, 2015	Issued for Town of Blackfalds Review
2	November 25, 2015	Issued for Alberta Transportation Review
3	November 28, 2016	Revised with New Site Plan Issued for Alberta Transportation Approval

## **EXECUTIVE SUMMARY**

WSP Canada Inc. was retained by Elkay Developments Ltd. and Spire General Partner Ltd. (Elkay / Spire) to complete a traffic impact assessment for the proposed Blackfalds Crossing Area Structure Plan (ASP) located within the southern limits of the Town of Blackfalds in NE 22-39-27-W4M.

i.

The purpose of this study is to identify and assess the potential traffic impacts on the study intersections associated with the proposed development, and to suggest required mitigation measures (if any) to allow that the adjacent roadways safely accommodate the proposed development.

The proposed Blackfalds Crossing Area Structure Plan (ASP) is located west of Highway 2A and north of Highway 597 encompassing a total of approximately 40 hectares of land. The proposed ASP area is anticipated to be developed in four stages. According to the development concept plan (Appendix A), Stage 1 will include a food anchored shopping centre along Highway 2A. Stage 2 will include highway commercial development along Highway 597 and row housing and multi-family residential development. Stages 3 and 4 will include single family, row housing, and live/work mixed use housing residential development. A total of 602 units of residential housing are anticipated to be developed in the proposed ASP area. It is anticipated that Stages 1 and 2 will be completed within 3 years by 2018 and the entire development will be fully built out by 2025. The land at the northeast corner of the NE 22-39-27-W4M is anticipated to be developed by others and is included in this study.

Primary vehicular access to the development will be obtained via Highway 2A, Highway 597, Broadway Avenue, East Railway Street, a proposed North-South Collector Road onto Highway 597 (South Access), and a proposed East-West Collector Road onto Highway 2A (East Access). The following intersections were analyzed in this study:

- → Highway 2A / Highway 597,
- → Highway 2A / Proposed East-West Collector Road,
- → Highway 597 / Proposed South Access, and
- → South Street / East Railway Street.

The existing Highway 2A / 597 intersection is a four-legged intersection. A two-lane modern roundabout was recently constructed at this intersection. Highway 2A was widened to four lanes from Highway 597 to Broadway Avenue.

The existing Highway 2A / Broadway Avenue intersection is a three-legged intersection with two northbound through lanes. This intersection is currently controlled by a stop sign on Broadway Avenue with free flow conditions on Highway 2A. It is anticipated that Broadway Avenue will be realigned and intersect with the proposed east-west collector road when the proposed subdivision is developed.

The existing South Street / East Railway Street intersection is a three-legged intersection and is controlled by a stop sign on the east approach with free flow conditions in the north and west directions.

The following conclusions and recommendations were reached:

#### HIGHWAY 2A / HIGHWAY 597

→ All traffic movements at the Highway 2A / Highway 597 intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 10 year horizon and LOS D or better at the 20 year horizon under the post-development traffic conditions. The roundabout at the

Highway 2A / Highway 597 intersection will be capable of accommodating the forecasted post-development traffic.

#### HIGHWAY 2A / BROADWAY AVENUE / EAST-WEST COLLECTOR

- → The eastbound traffic movements on Broadway Avenue currently operate at LOS E during the AM peak hours at the existing Highway 2A / Broadway Avenue intersection.
- → Traffic signals will be warranted at the proposed Highway 2A / East-West Collector Road intersection in 2016 when Stage 1 is fully built out.
- → The following intersection lane configurations are recommended when traffic signals are installed at this intersection:
  - Eastbound: two left turn lanes and one right turn lane;
  - Northbound: one left turn lane and two through lanes, and
  - Southbound: two through lanes and one right turn lane.
- When the proposed Highway 2A / East-West Collector Road intersection is under signal control, all traffic movements will operate at an acceptable LOS C or better during both the AM and PM peak periods up to the 20 year horizon. The proposed intersection lane configurations will be capable of accommodating the forecasted post-development traffic.
- → To improve the traffic operational performance at this intersection up to the 20-year horizon, traffic signals are proposed to be installed at the same time as the geometric improvements to an all-directional intersection. As the upgraded intersection nears capacity, the feasibility of a roundabout should be assessed at that time; however, the right of way for a future roundabout should be protected as the surrounding lands are developed.

#### HIGHWAY 597 / SOUTH ACCESS

- → A Type IV left turn lane will be warranted for eastbound traffic under the 3 year horizon postdevelopment traffic conditions. An additional 10 m storage length (total parallel deceleration lane length 65 m) will be required to accommodate the forecasted 20 year horizon traffic. The existing raised median on Highway 597 will need to be removed to provide room for the proposed eastbound left turn lane.
- → It is recommended that two through lanes be provided for the westbound traffic on Highway 597 between the Highway 2A / 597 roundabout and the existing two lanes approximately 200 m west of the proposed South Access. One eastbound through lane is expected to be capable of accommodating the forecasted post-development traffic. The proposed South Access intersection is located east of and out of the eastbound two-lane to one-lane transition zone on Highway 597. The proposed intersection treatment concept plan is shown in Figure 11 and attached in Appendix C.
- Alberta Transportation is requiring that two eastbound through lanes be provided at the South Access intersection up to the existing two lanes west of the Highway 2A / 597 roundabout to provide better safety and operational performance for the eastbound traffic. Alberta Transportation's requested intersection improvement concept plan is shown in Figure 12 and attached in Appendix C. Construction cost sharing with Alberta Transportation is anticipated to be required regarding these upgraded intersection improvements.

- → All traffic movements at the Highway 597 / South Access intersection will operate at an acceptable LOS D or better during both the AM and PM peak periods at the 10 and 20 year horizons under the post-development traffic conditions.
- → The intersection sight distances along Highway 597 at the South Access intersection appear to be adequate.
- $\rightarrow$  Signals will not be warranted at this intersection up to the 20 year horizon.
- → Delineation lighting will be warranted at the Highway 597 / South Access intersection.

#### SOUTH STREET / EAST RAILWAY STREET

- This intersection will become a four-legged intersection with the proposed N-S Collector Road forming the south leg. It is recommended that an additional stop sign be installed on the west approach when the proposed N-S Collector Road is constructed. No auxiliary lane (i.e., left or right turn lane) is recommended for this intersection.
- → All traffic movements at the South Street / East Railway Street intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 20 year horizon. The proposed intersection control type and lane configurations will be capable of accommodating the forecasted post-development traffic. South Street will operate at acceptable level of services with the existing two-lane cross section up to the 20 year horizon.

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## **1** INTRODUCTION

WSP Canada Inc. was retained by Elkay Developments Ltd. and Spire General Partner Ltd. (Elkay / Spire) to complete a traffic impact assessment for a proposed Blackfalds Crossing Area Structure Plan (ASP) located within the southern limits of the Town of Blackfalds in the NE 22-39-27-W4M. The subject site location is shown in Figure 1A.

#### 1.1 STUDY PURPOSE

The purpose of this study is to identify and assess the potential traffic impacts on the study intersections associated with the proposed development, and to suggest required mitigation measures (if any) to allow that the adjacent roadways safely accommodate the proposed development.

#### 1.2 SITE AND VICINITY DESCRIPTION

#### 1.2.1 SITE DESCRIPTION

The proposed Blackfalds Crossing Area Structure Plan area is bounded by Highway 2A to the east, Highway 597 to the south, South Street to the north, and the Blackfalds RCMP and Fire Department to the immediate west. A Canadian Pacific railway line runs north-south across the north-west corner of the proposed ASP area.

The proposed Blackfalds Crossing ASP area is located west of Highway 2A and north of Highway 597 encompassing a total of approximately 40 hectares of land. The proposed development is anticipated to be developed in four stages. According to the development concept plan, Stage 1 will include a food anchored shopping centre along Highway 2A. Stage 2 will include highway commercial development along Highway 597 and row housing and multi-family residential development. Stages 3 and 4 will include single family, row housing, and live/work mixed use housing residential development. The proposed development in the Blackfalds Crossing ASP is summarized in Table 1A. A total of 602 units of residential housing are anticipated to be developed in the proposed ASP area. For the purpose of this study, it is assumed that the Blackfalds Crossing ASP will be fully built out by 2025. The proposed development concept plan is shown in Figure 1B and the proposed staging plan is illustrated in Figure 1C.

The triangular parcel (2.05 hectares) west of the CP rail line is expected to be developed by the Town of Blackfalds for use as a community dog park.

The land at the northeast corner of the NE 22-39-27-W4 is anticipated to be developed by others. The assumed land uses on this land are illustrated in Table 1B. To distinguish the development on this land from the Blackfalds Crossing ASP, hereinafter, the land at the northeast corner of the NE 22-39-27-W4 is called future development.

1

PR	OPOSED DEVELOPMENT	SIZE	ANTICIPATED BUILD OUT YEAR
Stage 1	Food Anchored Shopping Centre	11.80 Acres (Land Area)	2016
	Highway Commercial	7.51 Acres (Land Area)	
Stage 2	Row houses (R-2)	36 units	2018
	Multi-Family Housing (R-4)	140 units	
Stage 3	Single Family Housing (R-1S)	88 units	2023
	Single Family Housing (R-1S)	80 units	
Stage 4	Row houses (R-2)	25 units	2025
	Mixed Use Housing	233 units	
Blackfalds Crossing ASP Total Residential		<b>602</b> Units	2025

#### Table 1A. Proposed Development Summary

#### Table 1B.Future Development (Land at Northeast Corner of NE 22-39-27-W4)

PROPOSED DEVELOPMENT	SIZE	ANTICIPATED BUILD OUT YEAR
Single Family Housing (R-1S)	16 units	2025
Highway Commercial	7.25 Acres (Land Area)	2025

#### 1.2.2 TRANSPORTATION NETWORK

Primary vehicular access to the development will be obtained via Highway 2A, Highway 597, Broadway Avenue, East Railway Street, a proposed north-south collector road onto Highway 597 (South Access), and a proposed east-west collector road onto Highway 2A (East Access). Therefore, the following intersections were analyzed in this study:

- → Highway 2A / Highway 597;
- → Highway 597 / Proposed South Access;
- → Highway 2A / Proposed East Access, and
- → South Street / East Railway Street / North-South Collector Road.

Highway 2A runs north-south parallel to the QE II Freeway and serves as the southern and northern gateway to the Town of Blackfalds. Highway 2A is a two-lane undivided provincial highway with a posted speed limit of 80 km/h in the vicinity of the proposed development. The current Average Annual Daily Traffic (AADT) and Average Summer Daily Traffic (ASDT) are estimated to be approximately 13,430 and 14,050 vehicles per day respectively, of which approximately 4% are trucks.

Highway 597 is a paved undivided provincial highway that connects the QEII and Highway 2A and provides access to the rural communities east of Blackfalds. The traffic volume on Highway 597 at the Highway 2A intersection is approximately 5,290 vehicles per day, of which approximately 11% are trucks. Highway 597 will eventually be twinned from Highway 2A to the CP rail bridge. However, the timing of Highway 597 twinning is unknown at present.

South Street is a two-lane local road with a posted speed limit of 50 km/h and is paved except for the segment between Broadway Avenue and East Railway Street which is graveled. South Street runs east-west and connects with Highway 597 to the west via Vista Trail.

The existing Highway 2A / 597 intersection is a four-legged intersection. A two-lane modern roundabout was recently constructed at this intersection. Highway 2A was widened to four lanes from Highway 597 to Broadway Avenue.

The existing Highway 2A / Broadway Avenue intersection is a three-legged intersection with two northbound through lanes. This intersection is currently controlled by a stop sign on Broadway Avenue with free flow conditions on Highway 2A. It is anticipated that Broadway Avenue will be realigned and intersect with the proposed east-west collector road when the proposed subdivision is developed.

The existing South Street / East Railway Street intersection is a three-legged intersection and is controlled by a stop sign on the east approach with free flow conditions in the north and west directions.

The Town of Blackfalds is planning to complete a Functional Design of Highway 2A from Highway 597 to South Street. It is unknown at present when the Town will commence the functional design.

#### 1.3 ANALYSIS HORIZONS

Three analysis horizons were established in this study:

- $\rightarrow$  3 year short term horizon (2018);
- → 10 year medium term horizon (2025), and
- $\rightarrow$  20 year long term horizon (2035).

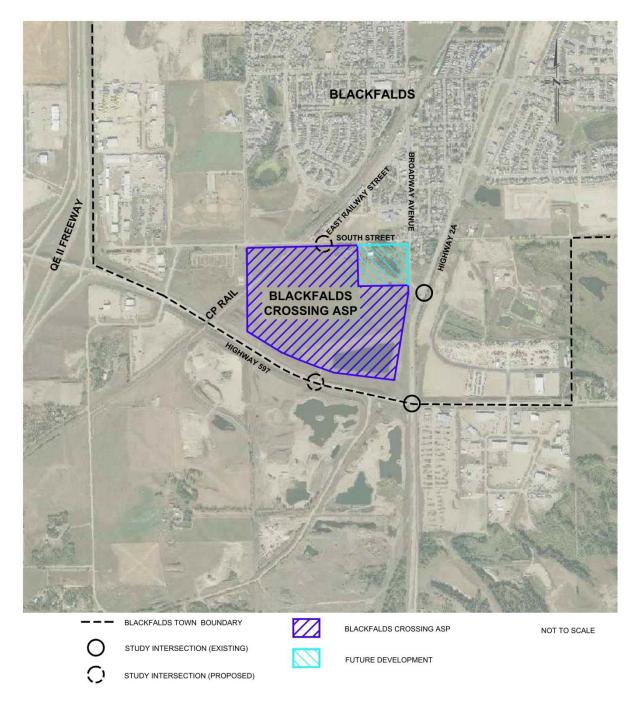


Figure 1A. Site Location

Blackfalds Crossing ASP Traffic Impact Assessment

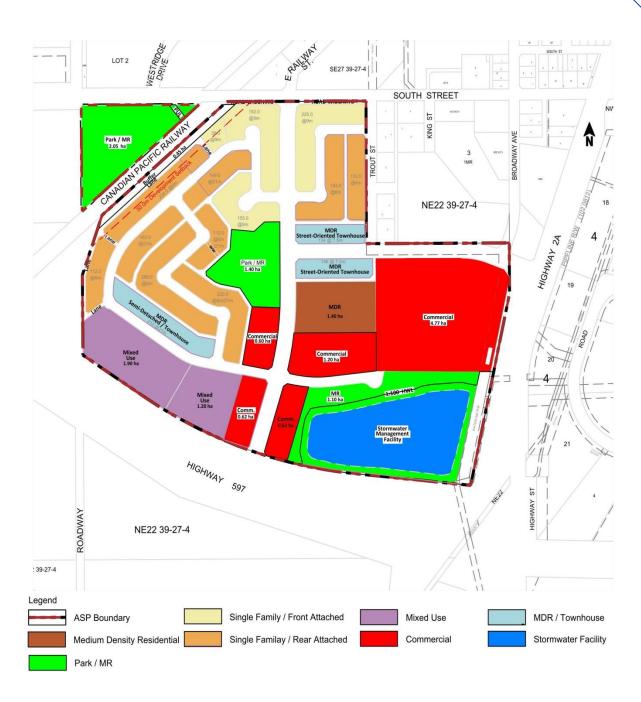
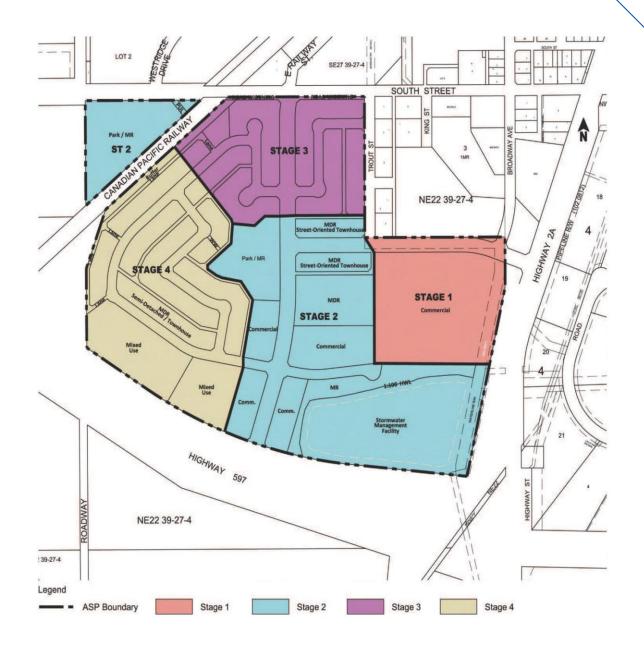


Figure 1B.

**Development Land Use** 





#### 1.4 SCOPE OF WORK

The scope of this study includes the following:

- → Determine current traffic operating conditions for the study intersections.
- → Forecast background traffic volumes at the analysis horizons based on the average annual linear growth rate.
- $\rightarrow$  Determine the number of new trips generated by the proposed development at each stage.
- → Distribute the generated trips to different geographic areas (origins and destinations) that will be served by the development.
- → Assign the generated trips to specific routes to and from the development.
- → Forecast post development (combined) traffic volumes at the study intersections at the analysis horizons.
- → Propose the appropriate lane configurations and traffic control (if needed) for the study intersections.
- $\rightarrow$  Evaluate the traffic operating conditions at the study intersections at each analysis horizon.
- Conduct signal and illumination warrants based on Transportation Association of Canada (TAC) guidelines.
- → Determine roadway, intersection, and access improvements required to provide acceptable levels of service (LOS) and safety.

#### 1.5 METHODOLOGY

In order to meet the study objectives and accomplish the works stated above, the following methodology was used:

- → Conduct AM and PM peak hour traffic counts at the Highway 2A / Broadway Avenue and South Street / East Railway Street intersections.
- → Obtain traffic turning movement information at the Highway 2A / 597 intersection from Alberta Transportation (AT).
- → Obtain historical traffic volumes on Highway 2A and Highway 597 adjacent to the study intersections from AT.
- → Estimate current weekday AM and PM peak hour traffic volumes for each turning movement at the study intersections.
- → Estimate the trips generated by the proposed development based on ITE's *Trip Generation Manual (9<sup>th</sup> Edition).*
- → Conduct left and right tune lane warrant analyses based on the procedure provided in AT's *Highway Geometric Design Guide.*
- → Analyze the delay, LOS and queue lengths of the study intersections at weekday AM and PM peak periods for the analysis horizon traffic using Synchro Studio 9 (Synchro) and SIDRA Intersection 6.1 (SIDRA) software.
- → Identify any improvements necessary for the intersections to accommodate the forecasted traffic volumes.

# 2 TRAFFIC ANALYSIS

This section analyzes the existing (2015), 3 year horizon (2018), 10 year horizon (2025), and the 20 year horizon (2035) traffic conditions for the study intersections. The background traffic volumes at the analysis horizons were determined by applying a linear traffic growth rate to the existing traffic volumes.

#### 2.1 EXISTING TRAFFIC

WSP conducted AM and PM peak hour traffic counts from 7:00 a.m. to 9:00 a.m. and from 4:00 p.m. to 6:00 p.m. on March 19 and July 9, 2015 at the Highway 2A / Broadway Avenue and South Street / East Railway Street intersections, respectively.

To estimate the existing (2015) traffic turning movements at the Highway 2A / 597 intersection, a 2.5% increase was applied to Alberta Transportation 2014 traffic volumes which are the latest available traffic data posted on their website at the time of this study.

Figure 3 shows the existing weekday AM and PM peak hour turning movement traffic volumes at the study intersections.

#### 2.2 TRAFFIC GROWTH

The traffic growth history obtained from Alberta Transportation's website for Highway 2A and Highway 597 adjacent to the study intersections is summarized in Table 1. The complete file is attached in Appendix B.

YEAR	HIGHWAY 2A NORTH of HWY 597		HIGHWAY 597 WEST OF HWY 2	
TEAR	AADT	GROWTH	AADT	GROWTH
2003	9,420	-	2,240	-
2004	9,910	5.2%	2,560	14.3%
2005	10,610	7.1%	2,720	6.3%
2006	11,250	6.0%	2,900	6.6%
2007	11,290	0.4%	2,940	1.4%
2008	11,070	-1.9%	2,940	0.0%
2009	10,800	-2.4%	3,660	24.5%
2010	10,990	1.8%	3,730	1.9%
2011	11,270	2.5%	3,730	0.0%
2012	12,620	12.0%	4,620	23.9%
2013	12,880	2.1%	5,060	9.5%
2014	13,100	1.7%	5,160	2.0%

#### Table 2.Historical Traffic Growth

Based on the historical traffic volumes on Highway 2A and Highway 597, Figure 2 illustrates the traffic growth trends including the linear AADT regression equations on the two highways in the vicinity of the study intersections. Using the regression equation, future traffic volumes on Highway 2A and Highway 597 were calculated and it was found that the future annual growth in traffic on Highway 2A is approximately 2.1% of the estimated 2015 volumes and the annual traffic growth on Highway 597 is approximately 5% of the 2015 traffic volumes.

In consulting with Alberta Transportation, the Ministry advised that the provincial average growth rate of 2.5% would be appropriate to estimate the future traffic for both Highway 2A and Highway 597. Therefore, in this study, a traffic growth rate of 2.5% was used to estimate the future traffic volumes on Highway 2A and Highway 597 at the 10 and 20 year horizons. A growth rate of 5% was used to estimate the 3 year horizon traffic volumes on Highway 597.

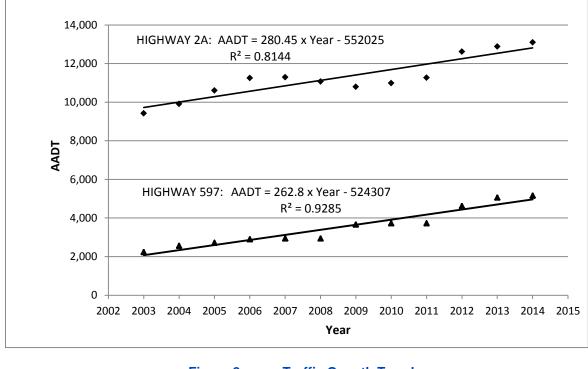
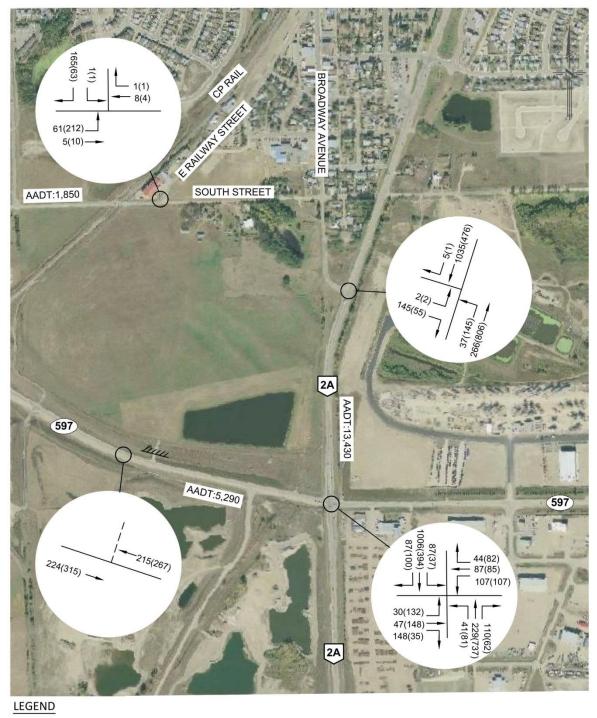


Figure 2. Traffic Growth Trends

#### 2.3 BACKGROUND TRAFFIC

Background traffic (non-site traffic) is the traffic that exists without the addition of the trips generated by the proposed development.

Based on the anticipated traffic growth rates, the forecasted background traffic volumes in terms of weekday AM and PM peak hour traffic at the 3, 10 and 20 year horizons are presented in Figures 4 to 6.

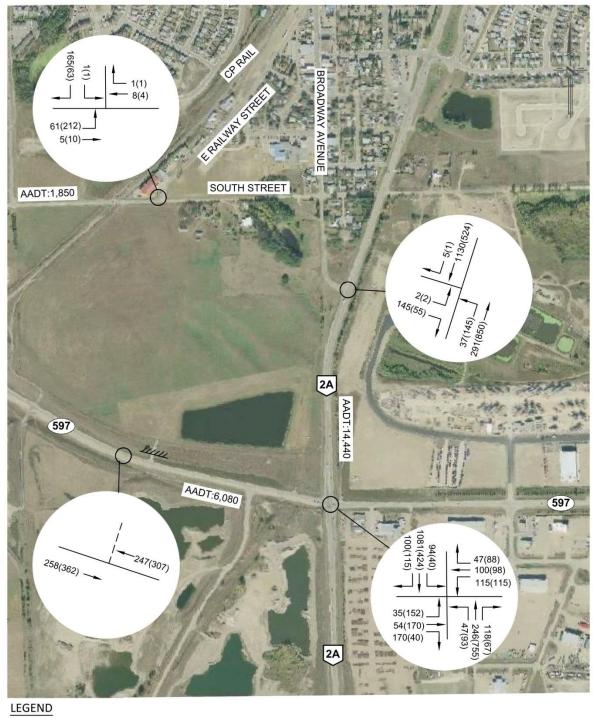


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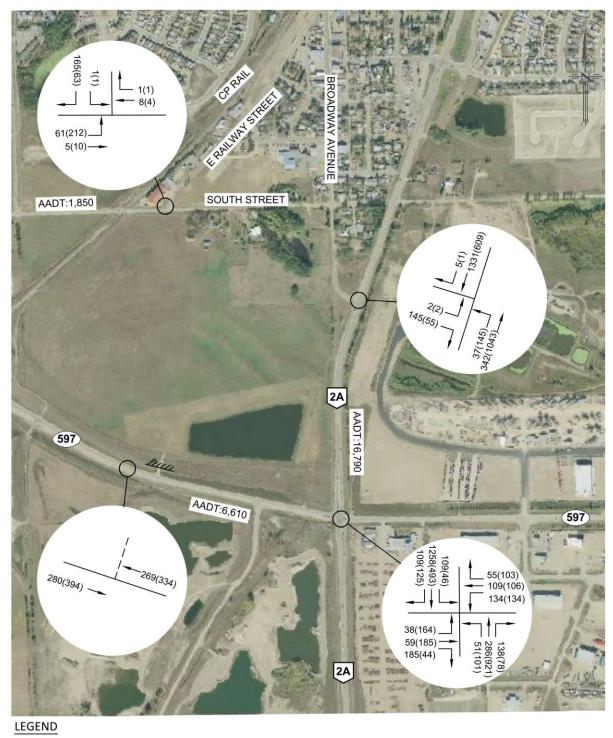
Figure 3.

Existing (2015) Traffic

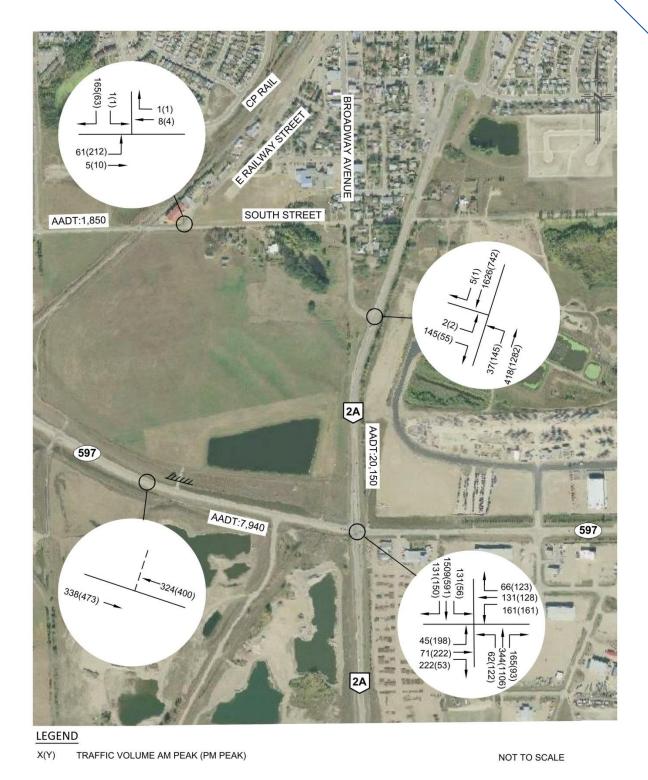
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#### 2.4 TRIP GENERATION

The Institute of Transportation Engineers (ITE) *Trip Generation Manual (9<sup>th</sup> Edition)* was used in this study to estimate the traffic generated by the proposed development.

The corresponding land uses in the ITE *Trip Generation Manual* that were used to estimate the traffic generated by the proposed developments are summarized in Table 3.

Table 3. Corresponding ITE	Land Uses
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PROPOSED DEVELOPMENT	ITE LAND USE (CODE)
Food Anchored Shopping Centre	Supermarket (850)
Highway Commercial	N/A
Single-Family Housing	Single-Family Detached Housing (210)
Row Housing	Residential Condominium / Townhouse (230)
Multi-Family Housing	Mid-Rise Apartment (223)
Mixed Lee Housing	Mid-Rise Apartment (223)
Mixed Use Housing	Shopping Center (820)

It should be noted that Highway Commercial is not a specific land use, and is better defined as a zoning category. In other words, Highway Commercial is defined as a mixed use site and includes a wide variety of land uses such as restaurants, gas bars, truck stops, and hotels. The ITE *Trip Generation Manual* does not provide trip generation rates for Highway Commercial land use.

Bunt & Associates Engineering Ltd. (Bunt) prepared a report for a C-TEP research project *"Trip and Parking Generation Rates for Land Uses in Small Towns in Alberta"* in 2005. In the report, Bunt recommended the AM and PM peak hour trip generation rates for Highway Commercial land use in Alberta. For the purpose of this study, the trip generation rates (AM: 2.56 / 1,000 ft<sup>2</sup>, PM: 4.21 / 1,000 ft<sup>2</sup>) recommended by Bunt were used to estimate the trips generated by the proposed highway commercial development. The trip directional distributions for Highway Commercial are based on the trip directional distribution rates for Shopping Center (Code: 820) in the ITE *Trip Generation Manual.* 

The Mixed Use Live/Work housing land use combines living and working quarters for individuals who can live and work in the same building. The ground floor will be used for business purposes, such as office, retail, or service. For the purpose of this study, it was assumed that 60% of the ground area of the mixed use housing would be used for commercial. The trip generation rates for Shopping Center were used to estimate the traffic that would be generated by the mixed use housing commercial uses.

A Floor Area Ratio (FAR) of 0.20 was used to calculate the Gross Floor Area (GFA) of the proposed food anchored shopping centre and commercial development.

#### 2.4.1 THREE YEAR HORIZON

In accordance with the developer, Stages 1 and 2 will be completed within three years by the year 2018. The estimated traffic volumes generated by the proposed developments in the two stages are illustrated in Tables 4A to 4D. It is anticipated that the proposed Stages 1 and 2 developments would generate a total of approximately 13,535 daily trips, 582 AM peak hour trips, and 1,151 PM peak hour trips

SUPERMARKET	WEEKDAY			AM PI	EAK HO	UR	PM PEAK HOUR			
GFA: 102,800 ft <sup>2</sup>	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribution	100%	50%	50%	100%	62%	38%	100%	51%	49%	
Rate (Trips/1000 ft <sup>2</sup> ) / Regression Equation	102.24	34.08	34.08	3.40	2.11	1.29	Ln(T)=0	.74Ln(X	)+3.25	
Total Trips	10510	5255	5255	350	217	133	795	405	390	

#### Table 4A. Trip Generation – Food Anchored Shopping Centre (Stage 1)

\*T=Vehicle Trips;  $X = 1000 \text{ ft}^2 \text{ GFA}$ .

#### Table 4B. Trip Generation – Highway Commercial (Stage 2)

GFA: 65,400 ft <sup>2</sup>	WEEKDAY			AM P	EAK HO	UR	PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Directional Distribution	100%	50%	50%	100%	62%	38%	100%	48%	52%
Rate (Trips/1000 ft <sup>2</sup> )	33.85	16.93	16.93	2.56	1.59	0.97	4.21	2.02	2.19
Total Trips	2214	1107	1107	167	104	64	275	132	143

#### Table 4C. Trip Generation – Row Housing (Stage 2)

UNITS: 36	WEEKDAY			AM PI	EAK HO	UR	PM PEAK HOUR			
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribution	100%	50%	50%	100%	17%	83%	100%	67%	33%	
Regression Equations	Ln(T)=0	.87Ln(X	)+2.46	Ln(T)=0.	80Ln(X)	+0.26	Ln(T)=0	Ln(T)=0.82Ln(X)+0		
Total Trips	264	132	132	23	4	19	26	17	9	

#### Table 4D. Trip Generation – Multi-Family Housing (Stage 2)

UNITS: 140	W	EEKDA	ſ	AM P	EAK HO	UR	PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Directional Distribution	100%	50%	50%	100%	31%	69%	100%	58%	42%
Rate (Trips / Unit)	3.90	1.95	1.95	0.30	0.09	0.21	0.39	0.23	0.16
Total Trips	546	273	273	42	13	29	55	32	23

#### 2.4.2 FULL BUIDL OUT

The proposed Blackfalds Crossing ASP is anticipated to be fully built out by 2025. The estimated traffic volumes generated by the proposed development in stage 3 and 4 are illustrated in Tables 4E to 4I. It is assumed that the land at the northeast corner of the NE 22-39-27-W4 would be developed by 2025. The anticipated trips that would be generated by this land are summarized in Tables 4J and 4K.

UNITS: 88	W	EEKDA	ſ	AM PI	ЕАК НО	UR	PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Directional Distribution	100%	100% 50% 50%			25%	75%	100%	63%	37%
Regression Equations	Ln(T)=0	.92Ln(X	)+2.72	T=0.7	70(X)+9.	74	Ln(T)=0	)+0.51	
Total Trips	934	467	467	71	18	54	94	59	35

#### Table 4E. Trip Generation – Single Family Housing (Stage 3)

\*T=Vehicle Trips; X = Dwelling Units.

#### Table 4F. Trip Generation – Single Family Housing (Stage 4)

UNITS: 80	W	EEKDA	Y	AM PI	EAK HO	UR	PM PEAK HOUR			
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribution	100%	50%	50%	100%	25%	75%	100%	63%	37%	
Regression Equations	Ln(T)=0	.92Ln(X	)+2.72	T=0.7	70(X)+9.	74	Ln(T)=0	Ln(T)=0.90Ln(X)+		
Total Trips	855	428	428	66	16	49	86	54	32	

\*T=Vehicle Trips; X = Dwelling Units.

#### Table 4G.Trip Generation – Row Housing (Stage 4)

UNITS: 25	W	EEKDA`	ſ	AM P	EAK HO	UR	PM PEAK HOUR			
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribution	100%	50%	50%	100%	17%	83%	100%	67%	33%	
Regression Equations	Ln(T)=0	.87Ln(X	)+2.46	Ln(T)=0.	80Ln(X)	+0.26	Ln(T)=0	Ln(T)=0.82Ln(X)+0		
Total Trips	193	96	96	17	3	14	19	13	6	

UNITS: 233	W	EEKDA	(	AM PI	AM PEAK HOUR			PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribution	100%	50%	50%	100%	31%	69%	100%	58%	42%	
Rate (Trips / Unit)	3.90	1.95	1.95	0.30	0.09	0.21	0.39	0.23	0.16	
Total Trips	909	454	454	70	22	48	91	53	38	

#### Table 4H. Trip Generation – Mixed Use Housing Residential (Stage 4)

T			
	Α	41	

#### Trip Generation – Mixed Use Housing Commercial (Stage 4)

GFA: 40,000 ft <sup>2</sup>	WEEKDAY			AM P	EAK HO	UR	PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Directional Distribution	100%	50%	50%	100%	62%	38%	100%	48%	52%
Rate (Trips/1000 ft <sup>2</sup> )	42.70	21.35	21.35	0.96	0.60	0.36	3.71	1.78	1.93
Total Trips	1708	854	854	38	24	15	148	71	77

#### Table 4J. Trip Generation – Single Family Housing (Future Development)

UNITS: 16		WEEKDAY			AM P	EAK HO	UR	PM PEAK HOUR			
		TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT	
Directional Distribut	on	100%	50%	50%	100%	25%	75%	100%	63%	37%	
Regression Equatio	ns	Ln(T)=0	.92Ln(X	)+2.72	T=0.7	70(X)+9.	74	Ln(T)=0	Ln(T)=0.90Ln(X)+		
Total Trips		195	97	97	21	5	16	20	13	7	

#### Table 4K. Trip Generation – Highway Commercial (Future Development)

GFA: 63,200 ft <sup>2</sup>	WEEKDAY			AM PI	EAK HO	UR	PM PEAK HOUR		
	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Directional Distribution	100%	50%	50%	100%	62%	38%	100%	48%	52%
Rate (Trips/1000 ft <sup>2</sup> )	33.85	16.93	16.93	2.56	1.59	0.97	4.21	2.02	2.19
Total Trips	2139	1070	1070	162	100	61	266	128	138

It is estimated that the proposed development would generate a total of approximately 20,470 daily trips, 1,027 AM peak hour trips, and 1,875 PM peak hour trips when the whole development area is fully built out.

#### 2.4.3 INTERNAL AND PASS-BY TRIPS

Internal trips should be considered for a multi-use development. According to the ITE *Trip Generation Handbook*, a multi-use development is typically a single real-estate project that consists of two or more ITE land use classifications between which trips can be made without using the off-site road system. The internal trips can be made either by walking or by vehicles using internal roadways. In this study, the proposed development is deemed to be a multi-use development (residential, shopping centre, and highway commercial), thus to estimate the trips made on the external streets, the internal trips that are not made on the major street system should be deducted from the total trips. To account for the internal trips, the following internal capture rates were used. It should be noted that vehicles travelling from / to the residential development may stop by the commercial development. These internal pass-by trips were considered as internal trips for commercial development.

- → Residential: 20%
- → Food Anchored Shopping Centre: 10%
- → Highway Commercial: 10%
- → Live/Work Housing Commercial development: 10%

According to the ITE *Trip Generation Handbook*, pass-by trips are defined as the trips that are made as intermediate stops on the way from an origin to a primary trip destination without a route diversion. Pass-by trips are attracted from traffic passing the site on an adjacent street or roadway that offers direct access to the generator. Pass-by trips will not add new traffic to the adjacent street system. In this study, the proposed shopper centre and highway commercial developments will attract pass-by trips. In accordance with the ITE *Trip Generation Handbook*, an average 36% of the trips generated by supermarket are pass-by trips. In this study, it is assumed that 35% of the total trips generated by the commercial development will be pass-by trips. Table 5 summarizes the estimated new trips that will be generated by the proposed development at full build out.

DEVELOPMENT	WEEKDAY			AM PEAK HOUR			PM PEAK HOUR		
DEVELOPMENT	TOTAL	IN	OUT	TOTAL	IN	OUT	TOTAL	IN	OUT
Residential (Blackfalds Crossing ASP)	3701	1850	1850	289	76	213	370	228	143
Commercial (Blackfalds Crossing ASP)	14432	7216	7216	555	344	211	1219	609	610
Total (Blackfalds Crossing ASP)	18133	9066	9066	844	420	424	1589	837	752
Residential (Future Development)	195	97	97	21	5	16	20	13	7
Commercial (Future Development)	2139	1070	1070	162	100	61	266	128	138
Total (Future Development)	2334	1167	1167	183	106	77	286	140	146
Total Trips	20467	10233	10233	1027	526	501	1875	977	898
Internal Trips	2436	1218	1218	134	61	73	227	122	105
External Trips	18030	9015	9015	893	465	428	1649	855	793
Pass-by Trips (35% of Commercial)	5220	2610	2610	226	140	86	468	232	236
Non-Pass-by Trips	12810	6405	6405	667	325	342	1181	623	558

#### Table 5.Trip Generation Summary

#### 2.5 TRIP DISTRIBUTION AND ASSIGNMENT

Trip distributions for the proposed development were estimated based on the traffic turning movement patterns at the existing intersections on Highway 2A and the road network in the vicinity of the proposed development.

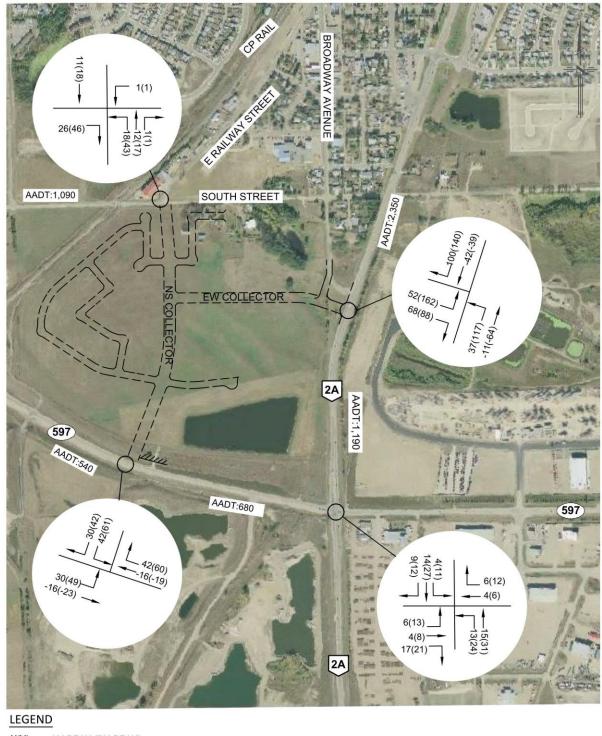
Figures 7A and 7B illustrate the estimated site generated trips at the 3 year horizon (Stages 1 and 2) and full build out, respectively. The detailed trip distribution and assignment for each land use are attached in Appendix B.

#### 2.6 COMBINED TRAFFIC

Combined traffic volumes (post-development traffic) include both background traffic and the traffic generated by the proposed development. Combined traffic volumes for the study intersections at the 3, 10 and 20 year horizons are shown in Figures 8 to 10.

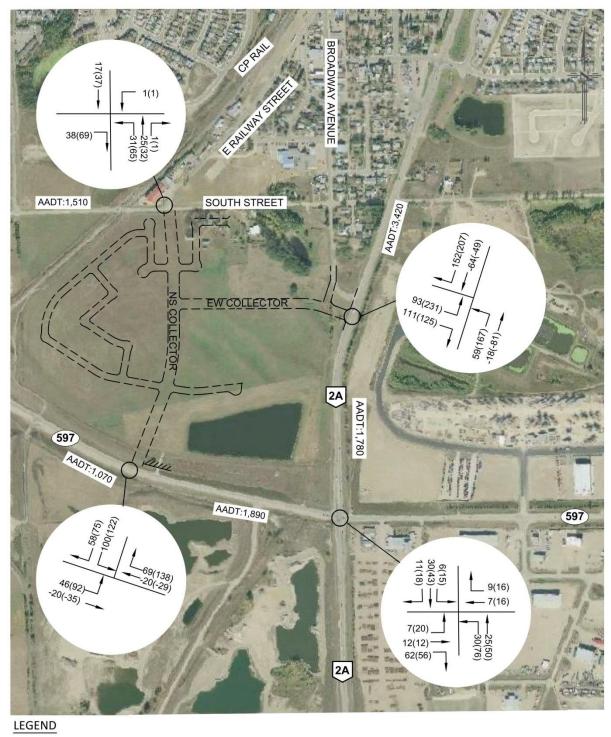
#### 2.7 SHORTCUTTING TRAFFIC

The proposed north-south collector road on site will provide a new connection between South Street and Highway 597. Some traffic travelling from the Town may use the proposed collector road as a shortcutting route to access onto Highway 597. However, based on the surrounding road network in the vicinity of the proposed development, it is anticipated that the volume of shortcutting traffic would be relatively small and would not significantly impact the Highway 597 / South Access intersection. Therefore, the shortcutting traffic was not included in this study.



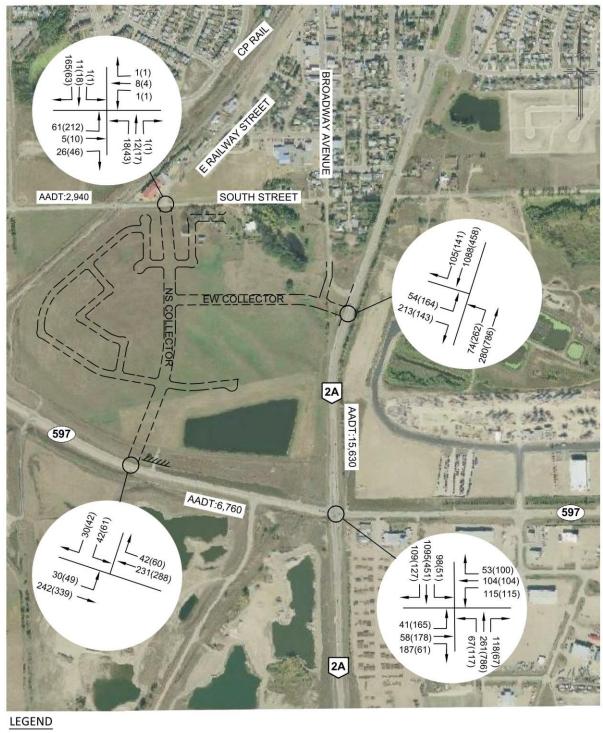




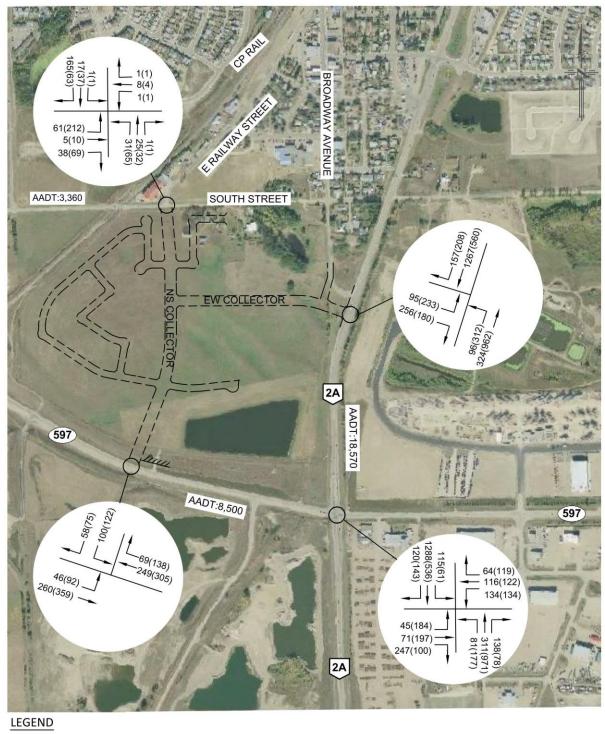




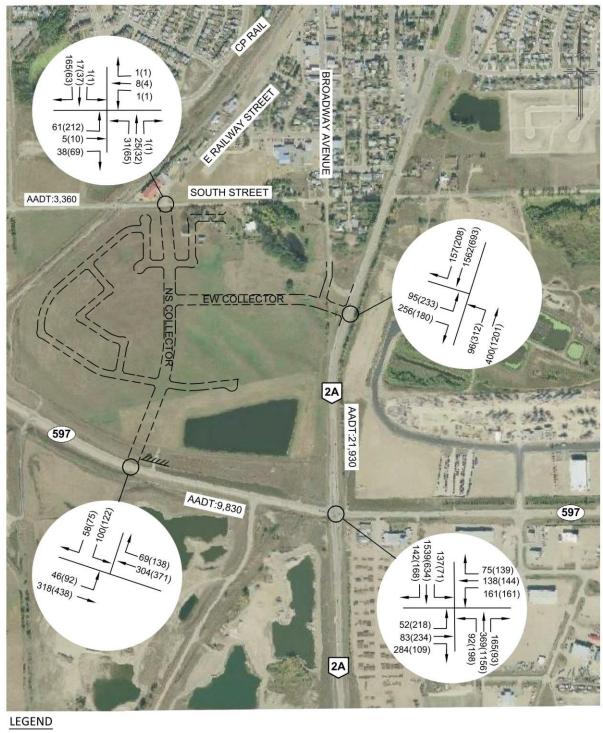














# 3 SIGNAL WARRANT ANALYSIS

Signal warrant analyses were conducted for the proposed Highway 2A / East Access, Highway 597 / South Access, and South Street / East Railway Street intersections based on the forecasted traffic volumes.

The signal warrant analysis followed the procedure recommended in the *Traffic Signal Warrant Handbook (2014)* published by the Transportation Association of Canada (TAC). A value of 100 cumulative warrant points is considered the minimum value required to warrant a traffic signal. The warrant analysis files are attached in Appendix C, and the analysis results are outlined in Table 6.

INTERSECTION	SCENARIO	WARRANT POINTS	SIGNALS?	
	Existing (2015)	73	Not Warranted	
	2018 Background	80	Not Warranted	
Highway 2A / Broadway Avenue / East-West Collector Road	2025 Background	94	Nearly Warranted	
	Stage 1 Combined	170	Warranted	
	2018 Combined	200	Warranted	
	2025 Combined	317	Warranted	
	2018 Combined	21	Not Warranted	
Highway 597 / South Access	2025 Combined	48	Not Warranted	
	2035 Combined	58	Not Warranted	
South Street / East Railway Street	2035 Combined	13	Not Warranted	

#### Table 6.Signal Warrant Analysis

Table 6 reveals that traffic signals will be warranted at the intersection of Highway 2A and the proposed East-West Collector Road under the 3 year horizon traffic conditions. It should be noted that traffic signals will be warranted in 2016 when Stage 1 is built out.

Traffic signals will not be warranted at the Highway 597 / South Access and South Street / East Railway Street intersection up to the 20 year horizon under the projected post-development traffic conditions.

It should be noted that Highway 2A is under Alberta Transportation's jurisdiction and in accordance with Design Bulletin #68/2010, Alberta Transportation may require that a roundabout feasibility assessment be conducted prior to installing traffic signals at the Highway 2A / East Access intersection.

The proposed East-West Collector Road intersection on Highway 2A will be located on a vertical sag curve with the gradient less than 4% in both northbound and southbound directions. In addition, there are no sight line constraints at this intersection. Therefore, a roundabout may be a feasible option for the proposed Highway 2A / East Access intersection. Based on the Technical Memo prepared by Stantec (Appendix A), traffic signals should be strongly considered as a more economical alternative

than a roundabout over the 20 year period and the Town of Blackfalds and Elkay / Spire wish to proceed with the construction of an upgraded signalized intersection.

Alberta Transportation indicated that they were prepared to consider the implementation of a signalized intersection at the Highway 2A / Broadway Avenue intersection on the condition that the Town of Blackfalds is responsible for constructing any future intersection improvements generated by developments, at the Town's cost and for addressing any operational concerns in a timely manner that may arise.

It is recommended that the right of way for a future roundabout at the Highway 2A / Broadway Avenue intersection should be protected as the surrounding lands are developed.

## 4 INTERSECTION ANALYSIS

This section presents the intersection analysis procedures that are specified in Alberta Transportation's *Highway Geometric Design Guide*, and covers the left and right turn lane criteria that were used in this study. The proposed Highway 597 / South Access intersection will not warrant traffic signals. Left and right turn lane warrant analyses were conducted for this intersection to determine if auxiliary lanes are required.

### 4.1 LEFT TURN LANE WARRANT ANALYSIS

Left turn warrants are based on the level of probability that a vehicle in the advancing traffic stream will not arrive at an intersection when another vehicle, traveling in the same direction, is stopped waiting to make a left turn. The interference caused by standing left turning vehicles in the through advancing traffic lane can reduce capacity and create a safety hazard. The amount of interference is dependent on opposing volumes, advancing volumes, and the number of left turning vehicles. The addition of a left turn lane with the required storage space will minimize this interference.

The analysis of left turn manoeuvres at the proposed Highway 597 / South Access intersection is based on the forecasted combined traffic volumes.

Table 7 summarizes the AM and PM peak hour turning information for the eastbound traffic on Highway 597 at the proposed South Access intersection under the 3, 10, and 20 year horizon combined traffic conditions. The left turn lane warrant analysis for the Highway 597 / South Access intersection was based on a design speed of 70 km/h.

EB <b>AM</b> PEAK	ADVANCING	OPPOSING	LEFT TURNS	% LEFT TURN	TRUCKS IN LT	WARRANTED?
2018 Combined	272	273	30	11%	10%	Yes, Type III
2025 Combined	306	318	46	15%	10%	Yes, Type IV
2035 Combined	364	373	46	13%	10%	Yes, Type IV
EB <b>PM</b> PEAK	ADVANCING	OPPOSING	LEFT TURNS	% LEFT TURN	TRUCKS IN LT	WARRANTED?
2018 Combined	388	348	49	13%	10%	Yes, Type IV
2025 Combined	451	433	92	20%	10%	Yes, Type IV
2035 Combined	530	509	92	17%	10%	Yes, Type IV

### Table 7. Left Turn Lane Warrant Analysis – Highway 597 / South Access

Table 7 reveals that a Type IV left turn lane will be warranted at the Highway 597 / South Access intersection for the eastbound traffic under the 3 year horizon post-development traffic conditions. An additional 10 m storage length (total parallel deceleration lane length 65 m) will be required to accommodate the forecasted 20 year horizon traffic. The existing raised median on Highway 597 will need to be removed to provide room for the proposed eastbound left turn lane.

### 4.2 RIGHT TURN LANE WARRANT ANALYSIS

According to Alberta Transportation's *Highway Geometric Design Guide*, the warrant for an exclusive right turn lane requires that all of the following conditions be met:

- → Main (or through) road AADT  $\geq$  1800,
- → Intersecting road AADT  $\geq$  900, and
- $\rightarrow$  Right turn daily traffic volume  $\geq$  360 for the movement in question.

Based on the forecasted traffic volumes, a westbound right turn lane will be warranted at the proposed Highway 597 / South Access intersection under the 3 year horizon post-development traffic conditions.

Based on the Highway 2A / 597 roundabout plan, the proposed right turn lane taper at the Highway 597 / South Access intersection will overlap the westbound two lanes to one lane merging taper located approximately 80 m east of the South Access on Highway 597. It is recommended that two through lanes be provided for the westbound traffic on Highway 597 between the Highway 2A / 597 roundabout and the existing two lanes approximately 200 m west of the proposed South Access.

The proposed Highway 597 / South Access intersection improvement concept plan is shown in Figure 11 and attached in Appendix C. The South Access intersection is located east and out of the two-lane to one-lane transition zone on Highway 597.

Alberta Transportation is requiring that two eastbound through lanes be provided at the South Access intersection up to the existing two lanes west of the Highway 2A / 597 roundabout to provide better safety and operational performance for the eastbound traffic. Alberta Transportation prefers the intersection improvement concept plan shown in Figure 12 and attached in Appendix C. Discussion on construction cost sharing with Alberta Transportation is anticipated to be required on the upgraded intersection improvement.

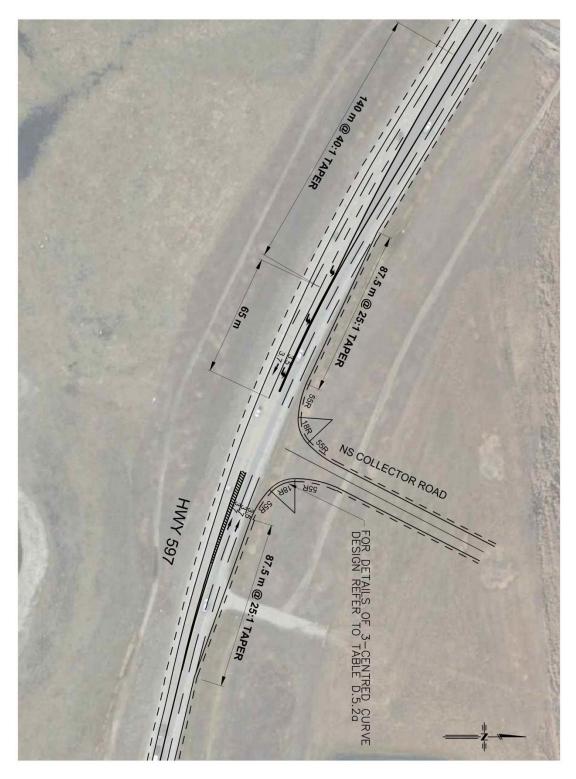


Figure 11. Proposed Intersection Improvement Concept Plan (South Access)

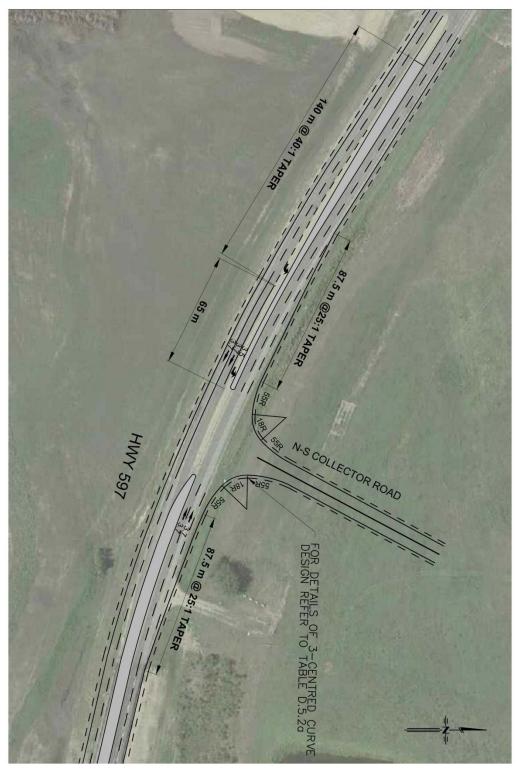


 Figure 12.
 AT Preferred Intersection Improvement Concept Plan (South Access)

# 5 CAPACITY ANALYSIS

This section describes the method used for the capacity analysis and evaluates the operating level of service of the study intersections under the 3, 10, and 20 year horizon traffic conditions.

### 5.1 METHODOLOGY

To determine the operating conditions of an intersection or roadway, the concept of level of service (LOS) is generally used. The LOS of an intersection is a qualitative measure of capacity and operating conditions and is directly related to vehicle delay. LOS is given a letter designation from A to F, with LOS A representing very short delays and LOS F representing very long delays.

For this study, WSP developed Synchro Studio 9 (Synchro) intersection simulation models for signal and stop controlled intersections. Synchro 9 implements the methods of the *Highway Capacity Manual, 2010* (HCM 2010) and follows the LOS criteria that is listed in Table 8. For two-way stop controlled intersections, the delay is typically calculated for the movements at the minor approaches only, since the major roads are considered to be operating at free flow conditions.

To evaluate the traffic operational performance for a roundabout, SIDRA Intersection 6.1 (SIDRA) was used. SIDRA employs a combined geometry and gap-acceptance modelling approach in order to take into account the effect of roundabout geometry on driver behaviour directly through gap-acceptance modelling. The LOS criteria for unsignalized intersections in Table 8 were used for assessing the traffic operational performance for a roundabout.

SIGNALIZED	UNSIGNALIZED	LOS BY VOLUME-TO	O-CAPACITY RATIO
CONTROL DELAY (s)	CONTROL DELAY (s)	<i>v/c</i> ≤ 1.0	<i>v/c</i> > 1.0
≤ 10	≤ 10	А	F
> 10 and ≤ 20	> 10 and ≤ 15	В	F
> 20 and ≤ 35	> 15 and ≤ 25	С	F
> 35 and ≤ 55	> 25 and ≤ 35	D	F
> 55 and ≤ 80	> 35 and ≤ 50	E	F
> 80	> 50	F	F

### Table 8. Level of Service Criteria for Intersections (HCM 2010)

### 5.2 CAPACITY ANALYSIS RESULTS

Traffic simulation models (Synchro and SIDRA) were created for the study intersections under the traffic conditions for each analysis horizon.

### 5.2.1 HIGHWAY 2A / HIGHWAY 597

The existing Highway 2A / 597 intersection is a four-legged intersection. A two-lane modern roundabout was recently constructed at this intersection.

Tables 9A to 9D summarize the anticipated traffic operational performance at the Highway 2A / 597 intersection under the analysis horizon traffic conditions when the two-lane modern roundabout is in operational. The detail SIDRA outputs are attached in Appendix D.

		AM PI	EAK HOU	IR	PM PEAK HOUR			
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
NBLT	4.7	А	0.17	6.8	7.9	А	0.42	17.3
NBTR	4.2	А	0.17	6.7	7.2	А	0.42	17.8
WBLT	4.5	А	0.12	3.8	8.2	А	0.20	7.0
WBTR	3.9	А	0.12	3.7	6.5	А	0.20	7.5
SBLT	9.4	А	0.54	25.2	5.7	А	0.25	9.3
SBTR	8.6	А	0.54	25.9	5.3	А	0.25	9.6
EBLT	9.0	А	0.16	5.4	5.8	А	0.18	6.0
EBTR	7.7	А	0.23	8.8	5.3	А	0.18	6.5
INT Summary	7.5	А	0.54	-	6.6	А	0.42	-

### Table 9A. Capacity Analysis: Existing (2015) Traffic – Highway 2A / 597 (Roundabout)

### Table 9B. Capacity Analysis: 2018 Combined Traffic – Highway 2A / 597 (Roundabout)

		AM PI	EAK HOU	R	PM PEAK HOUR				
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	
NBLT	5.2	А	0.21	8.7	9.6	А	0.49	22.5	
NBTR	4.7	А	0.21	8.6	8.5	А	0.49	22.6	
WBLT	5.0	А	0.14	4.6	9.9	А	0.26	9.4	
WBTR	4.3	А	0.14	4.6	7.7	А	0.26	10.1	
SBLT	11.5	В	0.62	35.2	6.6	А	0.31	12.0	
SBTR	10.5	В	0.62	35.3	6.1	А	0.31	12.5	
EBLT	11.2	В	0.23	8.1	6.9	А	0.25	8.7	
EBTR	9.8	А	0.32	13.2	6.3	А	0.25	9.6	
INT Summary	9.0	А	0.62	-	7.8	А	0.49	-	

		AM PI	EAK HOU	IR	PM PEAK HOUR				
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	
NBLT	5.8	А	0.25	10.8	13.8	В	0.65	39.9	
NBTR	5.2	А	0.25	10.7	12.1	В	0.65	40.6	
WBLT	5.5	А	0.17	5.6	15.1	В	0.38	15.3	
WBTR	4.7	А	0.17	5.5	11.2	В	0.38	16.9	
SBLT	15.5	С	0.73	53.6	8.3	А	0.40	16.0	
SBTR	14.0	В	0.73	54.4	7.5	А	0.40	16.8	
EBLT	15.5	С	0.33	12.2	8.6	А	0.33	12.1	
EBTR	15.3	С	0.49	24.3	7.9	А	0.33	13.8	
INT Summary	11.9	В	0.73	-	10.8	В	0.65	-	

### Table 9C.Capacity Analysis: 2025 Combined Traffic – Highway 2A / 597 (Roundabout)

Table 9D.Capacity Analysis: 2035 Combined Traffic – Highway 2A / 597 (Roundabout)

		AM PE	EAK HOU	IR	PM PEAK HOUR				
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	
NBLT	6.7	А	0.31	14.1	23.5	С	0.82	70.2	
NBTR	5.9	А	0.31	14.1	20.5	С	0.82	72.9	
WBLT	6.3	А	0.21	7.3	27.8	D	0.58	26.8	
WBTR	5.3	А	0.21	7.3	20.0	С	0.58	31.2	
SBLT	27.8	D	0.88	102.8	10.5	В	0.50	23.6	
SBTR	25.1	D	0.88	106.0	9.4	А	0.50	24.6	
EBLT	28.3	D	0.52	22.1	11.4	В	0.43	17.9	
EBTR	34.7	D	0.75	46.9	10.2	В	0.43	20.4	
INT Summary	20.8	С	0.88	-	17.0	С	0.82	-	

The capacity analysis results reveal that all traffic movements at the Highway 2A / 597 intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 10 year horizon and LOS D or better at the 20 year horizon under the post-development traffic conditions. The roundabout at the Highway 2A / 597 intersection will be capable of accommodating the forecasted post-development traffic.

### 5.2.2 HIGHWAY 2A / EAST-WEST COLLECTOR ROAD

Based on the signal warrant analysis results, the Highway 2A / East-west Collector Road intersection will warrant traffic signals at the 3 year horizon (2018) when Stage 1 and Stage 2 are fully built out.

Table 10A summarizes the current traffic operational performance at this intersection under the existing traffic conditions. Tables 10B to 10D summarize the traffic operational performance at the analysis horizons under the post-development traffic conditions when the intersection is under signal control. The detailed Synchro outputs are attached in Appendix D. The following intersection lane configurations are recommended when traffic signals are installed at this intersection:

- → Eastbound: two left turn lanes and one right turn lane;
- $\rightarrow$  Northbound: one left turn lane and two through lanes, and
- $\rightarrow$  Southbound: two through lanes and one right turn lane.

## Table 10A.Capacity Analysis: Existing Traffic – Highway 2A / Broadway Avenue<br/>(Stop Control)

TRAFFIC MOVEMENTS D		AM PI	EAK HOU	R	PM PEAK HOUR			
	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL	43.2	Е	0.65	43.5	13.3	В	0.13	3.5
NBL	11.2	В	007	1.6	9.0	А	0.15	4.0
INT Summary	4.6	А	0.65	-	1.9	А	0.15	-

## Table 10B. Capacity Analysis: 2018 Combined Traffic – Highway 2A / East-West Collector Road (Signal Control)

TRAFFIC		AM PI	EAK HOU	IR	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL,L	20.8	С	0.13	6.6	17.4	В	0.29	13.5
EBR	9.5	А	0.56	14.9	7.1	A	0.38	11.3
NBL	5.8	А	0.24	6.8	7.0	A	0.47	18.4
NBT,T	4.3	А	0.15	10.2	5.8	A	0.38	28.0
SBT,T	15.2	В	0.69	91.7	15.1	В	0.53	27.8
SBR	3.3	А	0.14	7.4	4.5	A	0.29	8.9
INT Summary	12.0	В	0.69	-	9.1	А	0.53	-

## Table 10C.Capacity Analysis: 2025 Combined Traffic – Highway 2A / East-West Collector<br/>Road (Signal Control)

TRAFFIC		AM PE	EAK HOU	R	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL,L	25.1	С	0.17	12.1	22.6	С	0.40	21.8
EBR	18.3	В	0.64	36.5	7.5	A	0.43	14.1
NBL	7.1	А	0.35	8.0	9.2	A	0.58	24.6
NBT,T	4.9	А	0.17	12.2	7.4	А	0.51	39.8
SBT,T	18.7	В	0.82	97.5	20.5	С	0.62	45.2
SBR	2.5	А	0.21	8.0	5.0	А	0.38	13.0
INT Summary	15.2	В	0.82	-	11.9	В	0.62	-

### Table 10D. Capacity Analysis: 2035 Combined Traffic – Highway 2A / East-West Collector Road (Signal Control)

TRAFFIC		AM PI	EAK HOU	R	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL,L	32.6	С	0.21	14.3	23.4	С	0.41	22.3
EBR	27.0	С	0.74	51.2	7.8	А	0.44	14.4
NBL	7.9	А	0.35	10.7	12.8	В	0.66	32.4
NBT,T	4.0	А	0.19	13.0	8.5	А	0.63	52.1
SBT,T	20.9	С	0.88	138.3	20.9	С	0.70	52.8
SBR	2.0	А	0.19	7.4	4.3	А	0.36	12.0
INT Summary	17.6	В	0.88	-	12.9	В	0.70	-

The above capacity analysis results reveal that the existing eastbound traffic movements on Broadway Avenue currently operate at LOS E during the AM peak hours. When the proposed Highway 2A / East-West Collector Road intersection is under signal control, all traffic movements at this intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods up to the 20 year horizon. The proposed intersection lane configurations will be capable of accommodating the forecasted post-development traffic.

As previously stated in Section 3, Alberta Transportation requires that a roundabout feasibility assessment be conducted prior to installing traffic signals at an intersection on provincial highways. A two-lane roundabout concept plan was developed for illustrative purposes and attached in Appendix C.

Tables 10E to 10G summarize the anticipated traffic operational performance at the Highway 2A / East Access intersection under the analysis horizon traffic conditions when the proposed roundabout is constructed.

Table 10E.	Capacity Analysis: 2018 Combined Traffic – Highway 2A / East-West Collector
	Road (Roundabout)

		AM PE	EAK HOU	R	PM PEAK HOUR				
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	
NBLT	3.8	А	0.14	5.6	7.7	А	0.46	23.2	
NBT	3.6	А	0.14	5.8	7.2	А	0.46	24.0	
SBT	7.1	А	0.46	22.1	6.1	А	0.29	11.9	
SBTR	6.6	А	0.46	22.2	5.6	А	0.29	12.2	
EBL	7.9	А	0.11	3.1	4.7	А	0.17	5.6	
EBR	6.9	А	0.27	9.0	5.4	А	0.17	5.5	
INT Summary	6.3	А	0.46	-	6.6	А	0.46	-	

## Table 10F. Capacity Analysis: 2025 Combined Traffic – Highway 2A / East-West Collector Road (Roundabout)

		AM PE	EAK HOU	R	PM PEAK HOUR			
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
NBLT	4.3	А	0.18	7.2	10.9	В	0.60	36.1
NBT	4.1	А	0.18	7.5	10.1	В	0.60	36.8
SBT	8.9	А	0.56	31.8	7.7	А	0.39	18.3
SBTR	8.2	А	0.56	32.1	7.1	А	0.39	19.0
EBL	9.4	А	0.20	6.0	6.0	А	0.25	9.3
EBR	9.0	А	0.36	13.9	6.7	А	0.24	8.1
INT Summary	7.8	А	0.56	-	8.8	А	0.60	-

		AM PI	EAK HOU	IR	PM PEAK HOUR			
LANE	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
NBLT	4.6	А	0.21	9.0	14.2	В	0.71	57.8
NBT	4.3	А	0.21	9.3	13.1	В	0.71	58.3
SBT	11.4	В	0.67	46.8	8.9	А	0.46	23.5
SBTR	10.4	В	0.67	47.0	8.1	А	0.46	24.5
EBL	11.6	В	0.23	7.6	6.7	А	0.28	10.3
EBR	11.6	В	0.43	18.3	7.7	А	0.26	9.1
INT Summary	9.7	А	0.67	-	11.0	В	0.71	-

## Table 10G. Capacity Analysis: 2035 Combined Traffic – Highway 2A / East-West Collector Road (Roundabout)

The roundabout capacity analysis results reveal that all traffic movements will operate at an acceptable LOS B or better during both the AM and PM peak periods up to the 20 year horizon if a roundabout is constructed at the Highway 2A / East-West Collector Road intersection. The proposed roundabout will be capable of accommodating the forecasted post-development traffic.

### 5.2.3 HIGHWAY 597 / SOUTH ACCESS

Tables 11A to 11C summarize the traffic operational performance at this intersection under the analysis horizon traffic conditions. The detailed Synchro outputs are attached in Appendix D.

TRAFFIC		AM PI	EAK HOU	R	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL	7.9	А	0.03	0.6	8.1	А	0.04	1.1
SBLR	11.6	В	0.20	3.3	13.9	В	0.22	6.2
INT Summary	1.8	А	0.20	-	2.2	А	0.22	-

Table 11A. Capacity Analysis: 2018 Combined Traffic – Highway 597 / South Access

Table 11B.	Capacity Analysis:	2025 Combined T	Fraffic – Highway 59	7 / South Access
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TRAFFIC		AM PI	EAK HOU	R	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL	8.0	А	0.04	1.0	8.3	А	0.08	2.4
SBLR	14.2	В	0.31	9.8	21.9	С	0.51	21.7
INT Summary	3.3	А	0.31	-	4.7	А	0.51	-

Table 11C.	Capacity Analysis: 2035 Combined Traffic – Highway 597 / South Access
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TRAFFIC		AM PI	EAK HOU	R	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBL	8.1	А	0.04	1.1	8.5	А	0.09	2.5
SBLR	15.9	С	0.34	11.5	28.2	D	0.59	28.3
INT Summary	3.2	А	0.34	-	5.1	А	0.59	-

The capacity analysis results reveal that all traffic movements at the Highway 597 / South Access intersection will operate at an acceptable LOS D or better during both the AM and PM peak periods at the 10 and 20 year horizons under the post-development traffic conditions. The proposed intersection treatment is expected to be capable of accommodating the forecasted future traffic volumes.

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### 5.2.4 SOUTH STREET / EAST RAILWAY STREET

The existing South Street / East Railway Street intersection is a three-legged intersection and is controlled by one stop sign on the east approach with free flow conditions in the north and west directions. This intersection is proposed to become a four-legged intersection with the proposed N-S Collector Road forming the south leg. It is recommended that an additional stop sign be installed on the west approach when the proposed N-S Collector Road is constructed. No auxiliary lane (i.e., left or right turn lane) is recommended for this intersection.

Tables 12A to 12C summarize the traffic operational performance at this intersection under the analysis horizon traffic conditions with the proposed intersection control type. The detailed Synchro outputs are attached in Appendix D.

### Table 12A. Capacity Analysis: 2018 Combined Traffic – South Street / East Railway Street

TRAFFIC		AM PI	EAK HOU	IR	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBLTR	10.1	В	0.12	3.1	12.1	В	0.37	12.7
WBLTR	10.4	В	0.02	0.4	10.1	В	0.01	0.2
NBL	7.6	А	0.01	0.3	7.5	А	0.03	0.7
SBL	7.2	А	0.00	0.0	7.3	A	0.00	0.0
INT Summary	3.7	А	0.12	-	8.7	А	0.37	-

### Table 12B. Capacity Analysis: 2025 Combined Traffic – South Street / East Railway Street

TRAFFIC		AM PI	EAK HOU	IR	PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)
EBLTR	10.3	В	0.14	3.8	13.9	С	0.44	17.1
WBLTR	10.8	В	0.02	0.4	10.7	В	0.01	0.2
NBL	7.7	А	0.03	0.6	7.5	A	0.05	1.1
SBL	7.3	А	0.00	0.0	7.3	А	0.00	0.0
INT Summary	4.0	А	0.14	-	9.3	А	0.44	-

TRAFFIC AM PEAK HOUR						PM PEAK HOUR			
MOVEMENTS	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	Delay (s)	LOS	V/C	95 <sup>th</sup> Queue Length (m)	
EBLTR	10.3	В	0.14	3.8	13.9	С	0.44	17.1	
WBLTR	10.8	В	0.02	0.4	10.7	В	0.01	0.2	
NBL	7.7	А	0.03	0.6	7.5	А	0.05	1.1	
SBL	7.3	А	0.00	0.0	7.3	А	0.00	0.0	
INT Summary	4.0	А	0.14	-	9.3	А	0.44	-	

### Table 12C. Capacity Analysis: 2035 Combined Traffic – South Street / East Railway Street

The above capacity analysis results reveal that all traffic movements at the South Street / East Railway Street intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 20 year horizon. The proposed intersection control type and lane configurations will be capable of accommodating the forecasted post-development traffic. South Street will operate at acceptable level of services with the existing two-lane cross section up to the 20 year horizon.

# 6 ADDITIONAL CONSIDERATIONS

This section is intended as a general overview of a number of site aspects. Some additional issues have been identified for consideration.

### 6.1 SIGHT DISTANCE

The intersection sight distances along Highway 2A and Highway 597 at the study intersections were checked utilizing Alberta Transportation's TIMS based on the sight distance requirements in Alberta Transportation's *Geometric Design Guide*. The sight distances are adequate at the study intersections.

### 6.2 OPERATIOANL ANALYSIS

The proposed realigned Broadway Avenue intersection on the East-West Collector Road will be located approximate 100 m (center line to center line) west of Highway 2A. The stacking distance between the Broadway Avenue / East-West Collector Road and Highway 2A / East-West Collector intersection is more than 50 m which is adequate to accommodate two 25 m long WB-23 vehicles.

The East-West Collector Road and Broadway Avenue intersection will be controlled by one stop sign on Broadway Avenue with free flow conditions on the East-West Collector Road. Therefore, no vehicle queue is expected to occur for the westbound traffic on the East-West Collector Road at the Broadway Avenue / East-West Collector Road intersection. As such, westbound traffic on the East-West Collector Road will not spill onto Highway 2A.

### 6.3 PEDESTRIANS AND ILLUMINATION

Currently there are no pedestrian facilities (e.g., sidewalks or trails) provided along Highway 2A or in the vicinity of the Broadway Avenue intersection. If the Town wants to provide pedestrian facilities in the future, pedestrian traffic will be accommodated by providing marked crosswalks and pedestrian signals at the proposed signalized intersection.

Lighting is currently provided at the Highway 2A / Highway 597, Highway 2A / Broadway Avenue, and South Street / East Railway Street intersections. The Highway 597 / South Access intersection was evaluated for illumination requirements based on the latest revision of the Transportation Association of Canada's (TAC) *Guide for the Design of Roadway Lighting*. The following factors were evaluated:

- Geometric geometric features of the intersection and associated roadways.
- Operational present and proposed AADT, roadway classification and operating speeds on all connecting legs.
- Environmental proximity to other lighted developments within the area.
- Collision night-time highway collision history in the area that may be attributed to lack of illumination.

Based on the TAC requirements, delineation lighting will be warranted at the Highway 597 / South Access intersection. The illumination warrant analysis can be found in Appendix C.

# 7 CONCLUSIONS AND RECOMMENDATIONS

This study has examined the traffic impacts associated with the proposed residential and commercial development located within the southern limits of the Town of Blackfalds. The conclusions and recommendations are summarized below:

### HIGHWAY 2A / HIGHWAY 597

→ All traffic movements at the Highway 2A / Highway 597 intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 10 year horizon and LOS D or better at the 20 year horizon under the post-development traffic conditions. The roundabout at the Highway 2A / Highway 597 intersection will be capable of accommodating the forecasted post-development traffic.

### HIGHWAY 2A / BROADWAY AVENUE / EAST-WEST COLLECTOR ROAD

- → The eastbound traffic movements on Broadway Avenue currently operate at LOS E during the AM peak hours at the existing Highway 2A / Broadway Avenue intersection.
- → Traffic signals will be warranted at the proposed Highway 2A / East-West Collector Road intersection in 2016 when Stage 1 is built out.
- → The following intersection lane configurations are recommended when traffic signals are installed at this intersection:
  - Eastbound: two left turn lanes and one right turn lane;
  - Northbound: one left turn lane and two through lanes, and
  - Southbound: two through lanes and one right turn lane.
- → When the proposed Highway 2A / East-West Collector Road intersection is under signal control, all traffic movements will operate at an acceptable LOS C or better during both the AM and PM peak periods up to the 20 year horizon. The proposed intersection lane configurations will be capable of accommodating the forecasted post-development traffic.
- → To improve the traffic operational performance at this intersection up to the 20-year horizon, traffic signals are proposed to be installed at the same time as the geometric improvements to an all-directional intersection. As the upgraded intersection nears capacity, the feasibility of a roundabout should be assessed at that time; however, the right of way for a future roundabout should be protected as the surrounding lands are developed. A roundabout concept plan was developed for this intersection and attached in Appendix C.

### HIGHWAY 597 / SOUTH ACCESS

- → A Type IV left turn lane will be warranted for eastbound traffic under the 3 year horizon postdevelopment traffic conditions. An additional 10 m storage length (total parallel deceleration lane length 65 m) will be required to accommodate the forecasted 20 year horizon traffic. The existing raised median on Highway 597 will need to be removed to provide room for the proposed eastbound left turn lane.
- → It is recommended that two through lanes be provided for the westbound traffic on Highway 597 between the Highway 2A / 597 roundabout and the existing two lanes approximately 200 m west of the proposed South Access. One eastbound through lane is expected to be capable of accommodating the forecasted post-development traffic. The proposed South

Access intersection is located east of and out of the eastbound two-lane to one-lane transition zone on Highway 597.

- → Alberta Transportation is requiring that two eastbound through lanes be provided at the South Access intersection up to the existing two lanes west of the Highway 2A / 597 roundabout to provide better safety and operational performance for the eastbound traffic. Alberta Transportation's requested intersection improvement concept plan is shown in Figure 12 and attached in Appendix C. Construction cost sharing with Alberta Transportation is anticipated to be required regarding these upgraded intersection improvements.
- → All traffic movements at the Highway 597 / South Access intersection will operate at an acceptable LOS D or better during both the AM and PM peak periods at the 10 and 20 year horizons under the post-development traffic conditions.
- → The intersection sight distances along Highway 597 at the South Access intersection appear to be adequate.
- $\rightarrow$  Signals will not be warranted at this intersection up to the 20 year horizon.
- → Delineation lighting will be warranted at the Highway 597 / South Access intersection.

### SOUTH STREET / EAST RAILWAY STREET

- → This intersection will become a four-legged intersection with the proposed N-S Collector Road forming the south leg. It is recommended that an additional stop sign be installed on the west approach when the proposed North-South Collector Road is constructed. No auxiliary lane (i.e., left or right turn lane) is recommended for this intersection.
- → All traffic movements at the South Street / East Railway Street intersection will operate at an acceptable LOS C or better during both the AM and PM peak periods at the 20 year horizon. The proposed intersection control type and lane configurations will be capable of accommodating the forecasted post-development traffic. South Street will operate at acceptable level of services with the existing two-lane cross section up to the 20 year horizon.

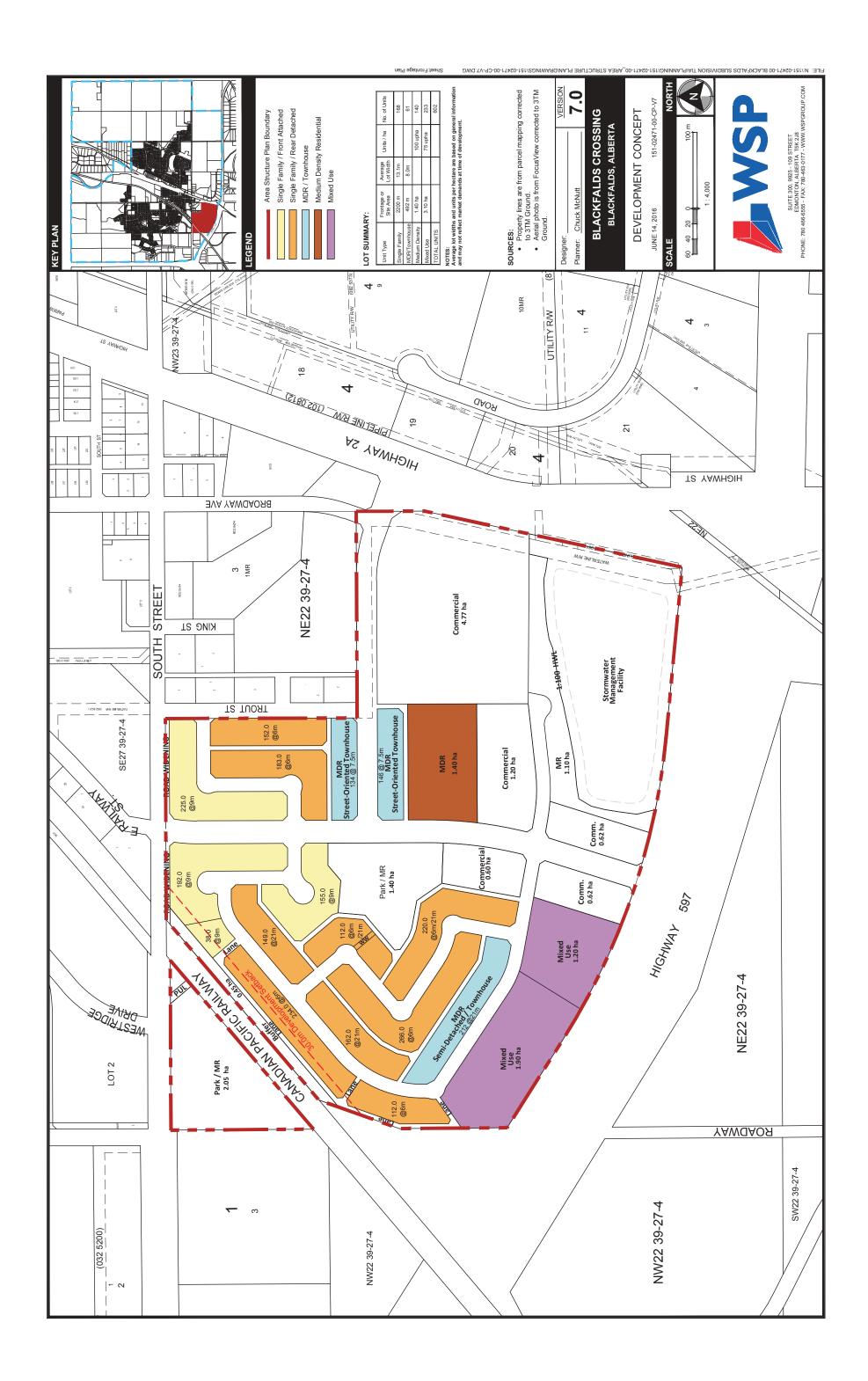


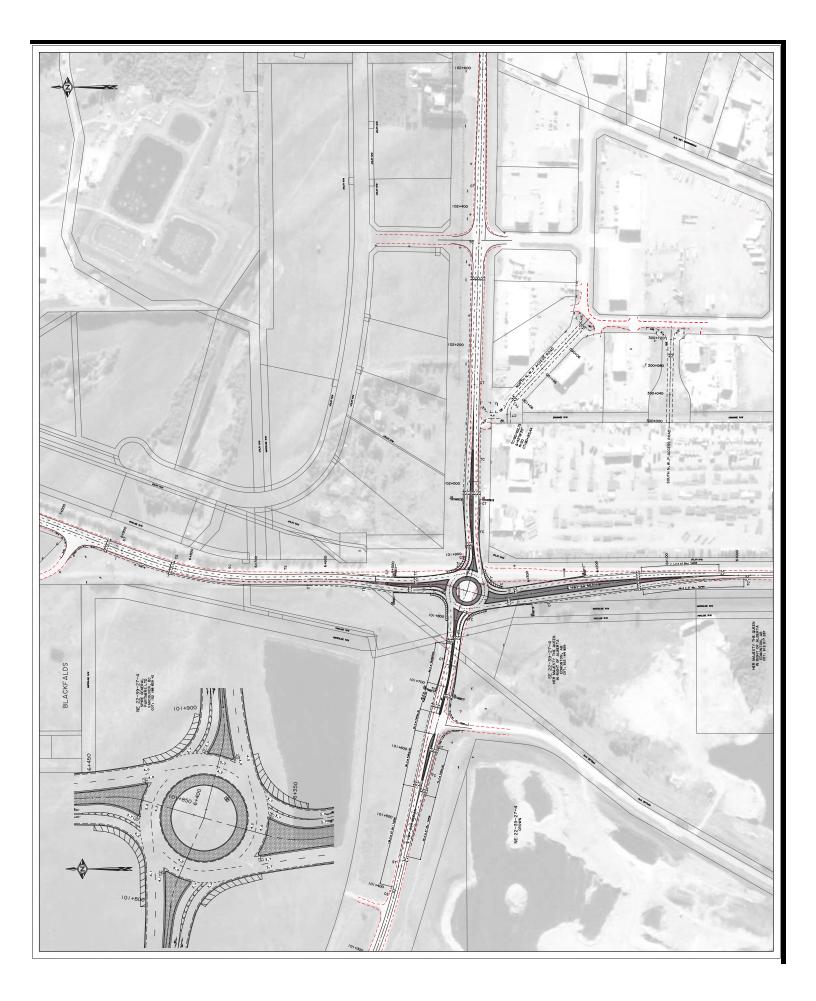
This report has been prepared by WSP based on the best information available at the time for the exclusive use of Elkay Developments Ltd. and Spire General Partner Ltd. Use by third parties, without the express written permission of WSP Canada Inc., is not permitted.

# Appendix A

## **PROJECT INFORMATION**

- Proposed Site Plan
- Highway 2A / 597 Roundabout Plan
- AT's Comments
- Stantec Roundabout & Traffic Signals Life Cost Analysis







Office of the Operations Manager Central Region #401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

September 27<sup>th</sup>, 2016

File: Blackfalds (ASP)

Town of Blackfalds Box 220, 5018 Waghorn St Blackfalds, AB TOM 0J0 Sent via email to: <u>MThompson@blackfalds.com</u>

Attention: Myron Thompson, Chief Administrative Officer

### RE: STANTEC TECHNICAL MEMO – REVIEW OF ROUNDABOUT & TRAFFIC SIGNALS NE 22-39-27-W4 (ELKAY DEVELOPMENTS) HIGHWAY 2A & BROADWAY AVENUE, BLACKFALDS CROSSING

Thank you for the technical memo and updated Life Cycle Cost Analysis (LCCA) comparing signalized intersection and roundabout treatment options at the Highway 2A & Broadway Avenue intersection.

We have reviewed the technical memo and in deciding between traditional traffic signals and a roundabout, we have considered the site-specific characteristics of this intersection, and given the life cycle costs of both are comparable, we prefer the roundabout option that offers lower collision costs, lower greenhouse gas cost, and better passenger and truck reliability (reduction in delays and improvements in traffic flow).

The LCCA clearly demonstrates the lower initial capital costs of traditional signals are offset by higher future collision costs. Within the context of similar overall life cycle costs, although our preference is to select the solution with the lower collision costs, we recognize the importance of the development to the Town of Blackfalds and we are prepared to consider the implementation of a signalized intersection at Highway 2A & Broadway Avenue on the condition that the Town of Blackfalds is responsible for constructing any future intersection improvements generated by developments, at the Town's cost and for addressing any operational concerns in a timely manner that may arise.

If the Town is amenable to accepting responsibility for all future Highway 2A and Broadway Avenue intersection improvements (which may include future twinning of Highway 2A to ensure adjacent intersections do not conflict) and operational issues, WSP is to incorporate the recommendation contained in Stantec's Technical Memo into a revised Traffic Impact Assessment for Alberta Transportation's acceptance.

If you have any questions, please contact me or Sandy Choi at 403-340-5166.

Sincerely,

N. Som

Mike Baik Operations Manager

SC/sc

cc: Stantec – <u>Brad.VanderHeyden@stantec.com</u> Preston Weran – <u>pweran@blackfalds.com</u> Russ Watts – Russell.Watts@gov.ab.ca



Office of the Operations Manager Central Region

#401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

Stuart Richardson - Stuart.Richardson@gov.ab.ca



To:	Stuart Richardson	From:	Brad Vander Heyden
	Alberta Transportation		Stantec Consulting Ltd.
File:	113928147-346	Date:	September 21, 2016

## Reference:Proposed Broadway Avenue Intersection Upgrades - Life Cycle Cost Analysis<br/>Review of Roundabout & Traffic Signals

### 1.0 INTRODUCTION AND BACKGROUND

On June 15, 2016, Elkay Developments, the Town of Blackfalds, WSP, and Stantec met with Alberta Transportation to discuss the options of upgrading the Highway 2A and Broadway Avenue intersection as two potential improvements - a signalized intersection as well as a roundabout. At that meeting, a preliminary copy of the Life Cycle Cost Analysis (LCCA) was provided for discussion purposes. At the conclusion of the meeting, Alberta Transportation was understanding of the subjectivity of the comparison and open-minded to resubmitting the LCCA with supporting information for their decision making process.

On behalf of the Town of Blackfalds and Elkay Developments, Stantec and WSP have collaborated on the preparation of this updated LCCA to serve our respective clients in a united manner and we are pleased to submit it to you accordingly. The LCCA, was developed using the National Cooperative Highway Research Program (NCHRP) Life Cycle Cost Estimation Tool. The NCHRP tool compares the long term costs of constructing an upgraded signalized intersection to the costs of a roundabout intersection.

In general, roundabouts have historically been demonstrated to typically function safer and more efficiently than traffic signals, but in most cases, roundabouts cost considerably more for this type of highway project. In completing our review, we have made effort to remain technically-neutral to the pros and cons of each alternative to ensure that a design alternative solution is chosen to meet the satisfactory requirements of all stakeholders involved.

The LCCA was completed to compare the 20 year life cycle costs of the two alternatives (traffic signals and roundabout improvements), to each other as well as the base alternative scenario of "do nothing". In addition to the costs of construction, the LCCA also factors in the costs of passenger time, truck time, and safety (i.e. cost of collisions). It should be noted that these costs are very subjective and as such, they should be well supported with supplementary information

The benefit-cost ratio, shown on the summary sheet, is relative to the base case only (no development and no improvements) and in our opinion, should not be taken into consideration in comparing the signals and the roundabout alternatives. The formulas that calculate the benefit-cost ratio also seems to be significantly skewed and don't compare the life cycle costs of the signals and the roundabout directly to each other.

### 2.0 LIFE CYCLE COST ANALYSIS – CRITERIA INPUT

The following items were reviewed in chronological order with WSP's draft document and updated in the spreadsheet for comparative discussion:



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### Reference: Proposed Broadway Avenue Intersection Upgrades

### 2.1 Cost Parameters

The Alberta Transportation Project Benefit Cost Model User Guide (April 8, 2015) has identified the following collision costs.

Accident Type	Stantec
Fatality	\$9,464,015
Injury	\$66,744
Property Damage Only	\$5,851

Table 3.1 – Accident	Costs, by Type
----------------------	----------------

It should be noted that Greenhouse Gas costs have not been included. Example case studies provided by the NCHRP that have included them have generally shown that the associated costs are very small relative to the overall cost and are not typically relevant in comparison.

Alberta Transportation uses as discount rate of 4%.

The demand and travel delays were based on the numbers provided by WSP are consistent with numbers used in the Alberta Transportation Project Benefit Cost Model User Guide (April 8, 2015).

### 2.2 Demand Parameters

The traffic demand parameters are based off of the Traffic Impact Assessment completed by WSP. As shown in the TIA, the signalized intersection will operate at an acceptable level of service beyond the standard 20 year design horizon.

### 2.3 Cost Base Inputs (Base Case, Alternative 1 – Signals, and Alternative 2 – Roundabout)

The Base Case is be a "do nothing" scenario, which is not an option to the Town and the Developer. Inherently, no development would mean no new upfront construction and design costs.

Direct Costs	Base Case	Alt 2 - Roundabout			
Planning and Design	\$O	\$200,000	\$300,000		
Construction (Total)	\$0	\$1,600,000	\$4,000,000		

### Table 3.2 – Costs of Construction and Professional Services



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### Reference: Proposed Broadway Avenue Intersection Upgrades

### 2.4 Collision Projections

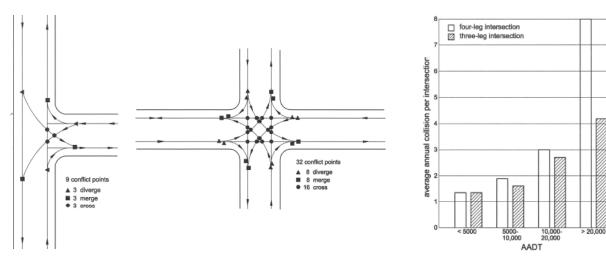
Perhaps the most challenging and subjective component of the analysis is the Safety costs, which are based on the number of fatal, injury only, and property damage only (PDO) collision types in the model. These are difficult to predict and they can vary substantially between model methodologies, Average Annual Daily Traffic (AADT) intersection types, posted speed limits, climate conditions, and unique site considerations. Rather than basing the estimated future collisions on models, we have taken a conservative approach of reviewing past collision history along the Highway 597 and Highway 2A corridors and inflating them quite conservatively to reflect future traffic growth. The data, which is discussed further below, was provided by the RCMP to the Town for information purposes. The projected collisions for the roundabout alternative were developed by WSP using the Collision Prediction Models for British Columbia in conjunction with the traffic volumes as per the TIA.

Collision Type	Base Case	Alt 1 - Signals	Alt 2 - Roundabout
Fatality	0.04	0.04	0.0
Injury	0.67	0.109	0.26
PDO	2.7	11	2.43

Table 3.3 – Projected Annual Collision Rates in Stantec Model

As shown in Table 3.4 below, there were 13 non-fatal collisions over a weighted 5 year period at the 5 intersections on Highways 2A and 597 in the Town limits, which averages 0.104 non-fatal collisions per year. Four of the five intersections used in the historical assessment are four legged intersections. The Broadway Avenue intersection is a tee intersection, which has less conflict points and lower collision rates than four legged intersections as illustrated in the TAC images below.





### Design with community in mind

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September 21, 2016 Stuart Richardson Page 4 of 6

### Reference: Proposed Broadway Avenue Intersection Upgrades

### \* Image from Transportation of Canada Design Guide for Canadian Roads

The current AADT for Highway 2A north of Highway 597 is approximately 12,910. At an annual increase of 2.5%, it will reach approximately 21,150 in 2035. On average over the 20 year timespan, it is reasonable to increase the collision rate by a factor of 1.5 for the traffic volume increase and multiply the collision rate per year by a factor of 0.70 for a three legged intersection. Stantec has modeled the collision rate as follows:

Collision rate = (0.104 collisions/year) x (0.70) x 1.5 = 0.109

Over the 6 year period (weighted to 5 years), there was one fatality among the five signalized intersections, which results in an average of 0.04 fatalities per year. The fatality was at the signalized intersection of Highway 2A and Highway 597, which at the time, had a posted speed limit of 80km/hr. The posted speed limit at the proposed signalized intersection locations would only be 60km/hr, which would have a much lower rate of fatality. For conservation reasons, the LCCA has maintained the 0.04 fatalities per intersection per year and has not reduced it for the reduction in conflict points of a tee intersection in comparison to a four-legged intersection.

Signalized	Year										
Intersections	2010	2011	2012	2013	2014	2015					
Highway 597 and Vista Trail			1								
Highway 597 and Highway 2A	1		2	2	2ª	<b>4</b> b					
Highway 2A and Park Street		1				1					
Highway 2A and Panorama Drive / Gregg Street		1		1	2						
Highway 2A and Cottonwood Drive		Not signalize									

Table 3.4 – Fatal & Non-Fatal Collision History at Signalized Intersections Since 2010

a) One of the two collisions in 2014 at the Highway 2A and Highway 597 intersection resulted in a fatality.

b) 2015 was the first full year that the roundabout was open

As shown in Table 3.5 below, there were zero fatal collisions and 4 non-fatal collisions among the 6 unsignalized intersections over the 6 year period. Two of them were at Broadway Avenue, and as such Stantec is proposing to use a collision rate of 0.67 (2 collisions / 6 years x 2.0 Conservation Factor) for the unsignalized intersection.



September 21, 2016 Stuart Richardson Page 5 of 6

### Reference: Proposed Broadway Avenue Intersection Upgrades

Unsignalized	Year										
Intersections	2010	2011	2012	2012 2013		2015					
Highway 2A and Broadway Avenue		1				1					
Highway 2A and South Street					1						
Highway 2A and Indiana Street (RIRO)											
Highway 2A and Cottonwood Drive					Signalized in 2013						
Highway 2A and TWP Rd 40-0		1									

### Table 3.5 – Collision History at Unsignalized Intersections (No fatalities)

The property damage only (PDO) projection developed by Stantec was based on the 2015 PDO data provided by the RCMP to the Town. To be conservative in the modeling, the rate was multiplied by a Factor of 2 based on the charts in the TAC collision rates and the projected AADT. The rate was developed as follows:

PDO Collision Rate = [(8 collisions) / (0.5 years) / 3 Intersections] x 2 = 10.6 (Rounded up to 11)

### 3.0 CONCLUSION AND OTHER ECONOMIC CONSIDERATIONS

Using the information entered above, which is highly conservative in the professional judgment of Stantec and WSP, the signalized intersections and the roundabout alternatives have 20 year life cycle costs of approximately \$6.0 Million and \$6.1 Million, respectively. Therefore, the traffic signals option should be strongly considered as a more economical alternative than a roundabout over the 20 year period. The additional \$2.5M construction value of the roundabout alternative over the signals is not considered economically viable to the Development, which is only approximately 90 acres in size, and development cannot proceed at this time if a roundabout will be required.

In addition, we would like Alberta Transportation to consider the additional economic benefits that will be realized by society if the development is able to proceed:

- 1. The construction of the servicing works for the first phase will provide jobs, income and additional tax revenue to the community and the province (approximately \$3.5 million for construction of the servicing works for phase 1).
- 2. The construction of commercial buildings for the first phase will provide jobs, income and additional tax revenue to the community and the province (approximately \$15 million for construction of approximately 80,000 sq. ft. of commercial/retail space).
- 3. Upon buildout the first phase commercial development will generate approximately \$180,000 to \$200,000 in tax revenue.



September 21, 2016 Stuart Richardson Page 6 of 6

### Reference: Proposed Broadway Avenue Intersection Upgrades

- 4. The completion of the first phase will be the catalyst to future phases (approximately 320 residential units and 10 additional acres of commercial land plus acres of Municipal Reserve).
- 5. Blackfalds requires additional retail services and conveniences which Blackfalds Crossing will provide.

It should also be noted that the "Do Nothing" scenario of no improvements to the Broadway Avenue intersection is the least favorable for public safety costs.

In summary, the Town of Blackfalds and Elkay Developments wish to proceed with the construction of an upgraded signalized intersection. We trust that this technical memo will meet your requirements, but if you have any questions or comments, we welcome the opportunity to discuss further to assist in moving this exciting project forward.

Sincerely,

### STANTEC CONSULTING LTD.

Markelle.

Brad Vander Heyden, P.Eng. Associate Phone: 403-341-3320 Fax: 403-342-0969 brad.vanderheyden@stantec.com

Attachment: Model Summary

c. Town of Blackfalds, Elkay Developments, WSP

### LIMITATIONS

The recommendations provided in this document are based strictly on the historical data that was provided to Stantec as well as the criteria shown in Alberta Transportation's Project Benefit Cost Model User Guide (April 8, 2015). The projected costs for safety are highly subjective and vary depending on the modeling techniques and other considerations that would need to be taken into account at the detailed design level.

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### Outputs

### This sheet compiles the data from summary tables in individual alternatives sheets.

#### Analysis Summary

Cost Categories	Net Present Value of Costs											
	Alternative 0 - Base Case	Alternative 1 - Signal	Alternative 2 - Multilane Roundabout									
Planning & Construction Costs	\$ -	\$ 1,800,000	\$ 4,300,000									
Post-Opening Costs	\$-	\$-	\$-									
Auto Passenger Time	\$ 211,360	\$ 1,572,767	\$ 1,027,413									
Auto Passenger Reliability												
Truck Time	\$ 17,471	\$ 130,004	\$ 84,925									
Truck Reliability												
Transit Passenger Time												
Transit Passenger Reliability												
Bicyclist Time												
Pedestrian Time												
Safety	\$ 3,951,717	\$ 2,498,629	\$ 718,739									
Greenhouse Gases												
Criteria Pollutants												
Total cost	\$4,180,548	\$6,001,400	\$6,131,078									

	Net Present Value of Benefits Relative to Base Case											
Benefit Categories			rnative 1 - Signal	Alternative Multilan Roundabo	e							
Auto Passenger Time		\$	(1,361,407)	\$ (81	L6,053)							
Auto Passenger Reliability												
Truck Time		\$	(112,533)	\$ (6	57,454)							
Truck Reliability												
Transit Passenger Time												
Transit Passenger Reliability												
Bicyclist Time												
Pedestrian Time												
Safety		\$	1,453,088	\$ 3,23	32,978							
Greenhouse Gases												
Criteria Pollutants												
Net Present Value of Benefits		\$	(20,852)	\$ 2,34	49,470							
Net Present Value of Costs		\$	1,800,000	\$ 4,30	00,000							
Present Value of Net Benefits		\$	(1,820,852)		6,530)							
Benefit-Cost Ratio			-0.01	0.55								

To exclude cost categories from the comparison clear all values in the row. Selecting the "Compile Analysis Summary" button will repopulate all values from the alternatives sheets.

THIS ASSESSMENT WAS COMPLETED WITH THE INTENT OF COMPARING THE SIGNALS AND ROUNDABOUT ALTERNATIVES TO EACHOTHER AND THEREFORE, A COMPARISON TO THE BASE CASE (NO DEVELOPMENT) SHOULD NOT BE CONSIDERED



Office of the Operations Manager Central Region

#401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

March 16<sup>th</sup>, 2016

File: Blackfalds (ASP)

Town of Blackfalds Box 220 5018 Waghorn St Blackfalds, AB T0M 0J0 Sent via email to: PWeran@blackfalds.com

Attention: Preston Weran, Director of Infrastructure and Property Services

### RE: PROPOSED BLACKFALDS CROSSING TRAFFIC IMPACT ASSESSMENT (TIA) NE 22-39-27-W4 (ELKAY DEVELOPMENTS) HIGHWAYS 2A & 597, BLACKFALDS CROSSING

Our department has reviewed the information that was provided in the TIA and notes the following:

- Page 3: The Town may wish to ensure that this TIA does not conflict with the Town's future Functional Design of Highway 2A from Highway 587 to the South Street. Please also ensure that the Functional Design is in accordance with Alberta Transportation's Highway 597 Functional Plan.
- Research for C-TEP by Bunt & Associates were used as trip generation for Highway Commercial. Please provide us with the background information on how the numbers were attained.
- For the other trip generation categories, the ITE 9th Edition were used as per Alberta Transportation TIA guidelines, however, during our review, we noticed inconsistencies between our numbers and the TIA. Appendix 1 contains a sample of numbers we derived from our review for comparison purposes.
- Page 20 and 21: Figure 7A and 7B site traffic show negative traffic. Clarification is required as to what negative traffic means.
- Page 27: Based on the left turn lane warrant analysis, a Type IV intersection is recommended. Please confirm the specific intersection treatment type recommended (i.e. Type IVa)
- Page 29: The geometry of this intersection's eastbound lanes needs to be looked at again as it does not appear to match any of Alberta Transportation's Type IV standards.
- We are unable to accommodate the proposed right-in and right-out (RI/RO) on Highway 2A. There does not appear to be a demonstrated need for the addition of a new RI/RI as southbound right turns from 2A operate at LOS A and eastbound rights out of the development at LOS C according to the analysis at the 2035 signalized horizon. Furthermore, the proposed RI/RO introduces a potential weaving issue for traffic originating from the highway commercial lot turning right onto Highway 2A requiring a quick transition for those needing to get into the left lane of the roundabout. Also, the RI/RO contributes to additional conflict points from non-conforming northbound Highway 2A left turns into the RI/RO. The proposed location of the RI/RO approximately 150 metres south of the realigned Broadway Avenue intersection would also not meet our access spacing requirements.
- We also require an operational analysis (showing design vehicle turning left into the development, left out of the development) at this intersection to determine if there will be any stacking distance issues between the first access from Highway 2A and the realigned Broadway Avenue, as well as a drawing that shows storage lengths.



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- There does not appear to developments east or south of the development where pedestrians require
  access, and accordingly, pedestrian warrants are not needed. Please confirm pedestrian requirements
  with the Town.
- In addition to the roundabout analysis, we also require a cost/benefit analysis (as per design bulletin #68/2010) since the TIA finds that a roundabout works at this location.
- The Town of Blackfalds is responsible for to submit a Roadside Development Application and a Traffic Accommodation Strategy (TAS) for the proposed Broadway Avenue realignment, and the new intersection on Highway 597.
- The Town of Blackfalds/Developer is responsible for arranging all the required intersectional improvements to accommodate the proposed development.

We look forward to receiving a revised copy with these amendments incorporated in the TIA for review prior to final endorsement. If you have any questions please contact me at 403-340-7179.

Sincerely,

Sandy Choi Development & Planning

SC/sc

cc. WSP (Craig Suchy – <u>Craig.Suchy@wspgroup.com</u>) Stuart Richardson, Alberta Transportation



Office of the Operations Manager Central Region #401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

This link includes access to the associated report and also a newly developed "Life-Cycle Cost Estimation Tool" that can be used to compare intersection designs such as roundabouts vs signals.

Prior to Alberta Transportation accepting the TIA, please provide the additional information requested. Should you have any questions regarding any of the points above or wish to schedule a meeting, please contact me at 403-340-7179.

Sincerely,

Sandy Choi Development & Planning

SC/sc

cc: WSP (Craig Suchy – <u>Craig.Suchy@wspgroup.com</u>) Town of Blackfalds (Prestan Weran – <u>PWeran@blackfalds.com</u>) Town of Blackfalds (Terry Topolnitsky – <u>Terry@blackfalds.com</u>)



62.0

360

27

32

DU

#401, 4920 - 51 Street Red Deer, Alberta

Telephone 403/340-5166 Fax 403/340-4876

### Appendix 1

230

			<u>Total Gen</u>	erated 1	Trips	Total Distribution of Generated Trips					
			AM PM Daily Hour Hour			AM In	AM Out	Pass-By	PM In	PM Out	Pass-By
						0			1		
Supermarket 850	KSF <sup>2</sup>	102.8	10,510	350	975	139	85	126	318	306	351
Single Family Homes 210	DU	40.0	381	30	40	8	23	0	25	15	0
Resd. Condo/Townhouse											

23

0

22

11

0

5



Office of the Operations Manager Central Region

May 11<sup>th</sup>, 2016

#401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

File: Blackfalds (ASP)

Town of Blackfalds c/o WSP 300, 9925 – 109 Street Edmonton, AB T5K 2J8 Sent via email to: <u>James.Sun@wspgroup.com</u>

Attention: James Sun, Transportation Engineer

### RE: PROPOSED BLACKFALDS CROSSING TRAFFIC IMPACT ASSESSMENT (TIA) NE 22-39-27-W4 (ELKAY DEVELOPMENTS) HIGHWAYS 2A & 597, BLACKFALDS CROSSING

Thank you for addressing our comments on the Blackfalds Crossing TIA. Alberta Transportation's (AT) response to your comments is below:

1. **AT's Original Comment**: Research for C-TEP by Bunt & Associates were used as trip generation for Highway Commercial. Please provide us with the background information on how the numbers were attained.

**WSP's Response**: We will provide a copy of C-TEP's report for the Department review. **AT's Response**: We have received a copy of C-TEP's report and advise if we have any feedback.

2. **AT's Original Comment**: For the other trip generation categories, the ITE 9<sup>th</sup> Edition were used as per Alberta Transportation TIA guidelines, however, during our review, we noticed inconsistencies between our numbers and the TIA. Appendix 1 contains a sample of number we derived from our review for comparison purposes.

**WSP's Response**: WSP also used the ITE 9<sup>th</sup> Edition Trip Generation Manual in the process of trip generation estimate. ITEP Trip General Manual provides Average Trip Generation Rates and Fitted Curve Equations for most land uses in the manual. The process for selecting Average Rate or Equation for the proposed development followed the step-by-step procedure recommended in the ITP Trip Generation Handbook, Third Edition. In this study, when the equations were selected to estimate the trips generated by the development. The estimated trips will be different from that were estimated based on the average rates (AT used in the sample).

AT's Response: Acknowledged.

- AT's Original Comment: Page 20 & 21: Figure 7A and 7B site traffic show negative traffic. Clarification is required as to what negative traffic means.
   WSP's Response: The negative traffic numbers are pass-by trips for commercial development. Pass-by trips are drawn from the passing traffic stream and do not add new traffic to the adjacent road system. The detailed pass-by trip analysis for each commercial development is attached in Appendix B in the TIA report.
   AT's Response: Acknowledged.
- AT's Original Response: Page 27: Based on the left turn lane warrant analysis, a Type IV intersection is recommended. Please confirm the specific intersection treatment type recommended (i.e. Type IVa).
   WSP's Response: The left turn lane warrant analysis indicated that a Type IV left turn lane (exclusive left turn lane) will be warranted for the eastbound traffic at the intersection. Highway

M:\DS\CR\RD OPS\JOINT.DEV\Town-City\Blackfalds\ASP\NE 22-39-27-4 Blackfalds Crossing Elkay Development\11May2016 Response to WSPs Letter.doc



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597 is not an Alberta Transportation's standard two-land highway (Raised median and fourlane cross-section to the west). It's hard and not necessary to apply a standard Type IV intersection treatment to this intersection. Since this is a three-legged intersection, Type IVa may be appropriate if we need to specify the intersection treatment type.

### AT's Response:

### a. Eastbound Hwy 597

The proposed intersection is located in a transition zone between a divided and undivided roadway. Merging of lanes at the intersection are potential operational and safety issues. It is undesirable to have a proposed intersection located within a transition zone. Issues include not meeting driver expectations, increase driver workload, high potential for confusion, sideswipe and rear end type collisions with the proposed two eastbound lane transitioning into a single lane through the intersection.

The warranted left turn lane EB to NB should be provided along with either a painted island or a preferred small raised island (1.5m minimum curb face to curb face width should be provided for hazard sign /keep right assembly) on the east leg. However, to reduce the potential operational/safety concerns, the two eastbound through lanes should be maintain past the proposed intersection. The two through lanes transition (or tie in) to the existing single lane should occur further east of the proposed intersection location or if possible, continue the two lanes east to the existing two lane (west of the roundabout).

### b. Westbound Hwy 597

The right side eastbound lane (shown as through/right arrow pavement markings) has not accommodated for slower vehicles (WB to NB) to decelerate and turn right from the eastbound through lane. **Deceleration and acceleration tapers should be provided** east and west of the proposed intersection treatment respectively.

- c. What is the radius of the horizontal curve and superelevation rate on Hwy 597? Intersections on horizontal curves are considered undesirable. As indicated in the AT HGDG (page B-29), Table B3.6a, for design speeds from 40km/h to 90 km/h, intersections are only permitted if e is less than or equal to 0.038. Highway 597 is posted at 50 km/h (design typical 60 km/h).
- d. The existing north intersection immediately east of proposed intersection should be closed.
- 5. **AT's Original Comment**: Page 29: The geometry of this intersection's eastbound lanes needs to be looked at again as it does not appear to match any of Alberta Transportation's Type IV standards).

**WSP's Response**: Similar reason as above, the proposed intersection treatment is not a standard Type IV intersection. The eastbound left turn lane will be provided by removing the raised median on the west leg. The eastbound through lane alignment will not change. An AT's Standard Type IV left turn lane on a two-lane highway is provided by shifting through lane to shoulder side by 3.5 m. A approaching tape and a departure taper (recovery taper) are required to accommodate the through traffic movement shifting. In our case, the eastbound through movement will not need to shift to the shoulder side and will stay in the existing through lane since the left turn lane will be provided by removing the raised median. As such, no tapers for the EB through lane will be required. That's why the proposed intersection treatment does not match AT's Type IV standard.

AT's Response: See AT's response to Section #4.



Office of the Operations Manager Central Region

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6. AT's Original Comment: We are unable to accommodate the proposed right-in and right-out (RI/RO) on Highway 2A. There does not appear to be a demonstrated need for the addition of a new RI/RO as the southbound right turns from 2A operate at LOS A and eastbound rights out of the development at LOS C according to the analysis at the 2035 signalized horizon. WSP's Response: The right-in/right-out access was determined to be removed from the proposed site plan.

AT's response: Thank you and acknowledged.

7. **AT's Original Comment**: We also require an operational analysis (showing design vehicle turning left into the development, left out of the development) At this intersection to determine if there will be any stacking distance issues between the first access from Highway 2A and the realigned Broadway Avenue, as well as a drawing that shows storage lengths.

**WSP's Response**: The proposed realigned Broadway Avenue intersection on the East-West Collector Road will be located approximately 100m (center line to center line) west of Highway 2A. The stacking distance is adequate for two 25 m long WB-23 vehicles. The capacity analysis results show that the eastbound vehicle queue at the Highway 2A intersection will not reach the Broadway Avenue intersection. The design vehicle operational analysis will be conducted in preliminary and detail design stages.

**AT's Response:** The capacity analysis results showing eastbound vehicle queue at the Highway 2A intersection will not reach the Broadway Avenue intersection addresses local road concerns. We would like to see the design vehicle operational analysis done at the TIA stage to look at whether traffic spills onto Highway 2A and reaffirm the appropriate location of the local road intersection from Highway 2A.

8. **AT's Original Comment**: There does not appear to be developments east or south of the development where pedestrians require access, and accordingly, pedestrian warrants are not needed. Please confirm pedestrian requirements with the Town.

WSP's Response: Pedestrians are not anticipated crossing Highway 2A and Highway 597.

**AT's response**: How do you envision the potential for pedestrian traffic wanting to access the commercial destination at Blackfalds Crossing from the east side of Highway 2A?

9. **AT's Original Comment**: In addition to the roundabout analysis, we also require a cost/benefit analysis (as per design bulletin #68/2010) since the TIA finds that a roundabout works at this location.

**WSP's Response**: The purpose of the roundabout analysis in the TIA is to preliminarily identify if a roundabout is physically feasible for the geometrics of the roadway location and if a roundabout is able to accommodate the forecasted future traffic volumes. A cost/benefit analysis should be conducted in a detailed Roundabout Feasibility Study which is out of the scope of work of the TIA.

**AT's Response**: Section 1.0 Economic Analysis of the design bulletin requires that "an economic analysis shall be undertaken to assist in evaluating the preferred type of intersection control as per the current version of the Department's Benefit Cost Guide, that accounts for all cost and benefits over the design period". Alberta Transportation has consulted with the Town of Blackfalds and we would like to see an economic analysis as part of this TIA to establish the feasibility of a roundabout at this location.

Here is a link to a Transportation Research Board project on "Estimating the Life-Cycle Cost of Intersection Designs." <u>http://www.trb.org/Main/Blurbs/173928.aspx</u>



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This link includes access to the associated report and also a newly developed "Life-Cycle Cost Estimation Tool" that can be used to compare intersection designs such as roundabouts vs signals.

Prior to Alberta Transportation accepting the TIA, please provide the additional information requested. Should you have any questions regarding any of the points above or wish to schedule a meeting, please contact me at 403-340-7179.

Sincerely,

Sandy Choi Development & Planning

SC/sc

cc: WSP (Craig Suchy – <u>Craig.Suchy@wspgroup.com</u>) Town of Blackfalds (Prestan Weran – <u>PWeran@blackfalds.com</u>) Town of Blackfalds (Terry Topolnitsky – <u>Terry@blackfalds.com</u>)



May 30, 2016

Alberta Transportation - Central Region #401, 4920 – 51 Street Red Deer, AB T4N 6K8

Attention: Sandy Choi, Development and Planning Technologist

### Re: PROPOSED BLACKFALDS CROSSING TRAFFIC IMPACT ASSESSMENT (TIA) NE 22-39-27-W4 (ELKAY DEVELOPMENTS) HIGHWAYS 2A & 597, BLACKFALDS CROSSING

0/Ref: 151-02471-00

Thank you for your comments on the Blackfalds Crossing TIA Report. The following details our responses to your comments dated May 11, 2016:

- 1. **(Comment #4)** Page 27: Based on the left turn lane warrant analysis, a Type IV intersection is recommended. Please confirm the specific intersection treatment type recommended (i.e. Type IVa).
  - a. Eastbound Hwy 597

The proposed intersection (Highway 597 / South Access) is located in a transition zone between a divided and undivided roadway. Merging of lanes at the intersection are potential operational and safety issues. It is undesirable to have a proposed intersection located within a transition zone. Issues include not meeting driver expectations, increase driver workload, high potential for confusion, sideswipe and rear end type collisions with the proposed two eastbound lane transitioning into a single lane through the intersection.

**Response:** We have developed a new concept plan and the proposed two eastbound through lanes continue to the existing two through lanes to the east.

b. Westbound Hwy 597

The right side eastbound lane (shown as through/right arrow pavement markings) has not accommodated for slower vehicles (WB to NB) to decelerate and turn right from the eastbound through lane. Deceleration and acceleration tapers should be provided east and west of the proposed intersection treatment respectively.

## **Response:** We have developed a new concept plan with the proposed deceleration and acceleration tapers for the westbound traffic.

*c*. What is the radius of the horizontal curve and superelevation rate on Hwy 597? Intersections on horizontal curves are considered undesirable. As indicated in the AT HGDG (page B-29), Table B3.6a, for design speeds from 40km/h to 90 km/h, intersections are only permitted if e is less than or equal to 0.038. Highway 597 is posted at 50 km/h (design typical 60 km/h).

**Response:** The radius of the horizontal curve is approximately 840 m and the super-elevation is approximately 0.046. The superelevation will be adjusted to



meet the department requirements during the detail design stage. The existing horizon curve radius (840 m) is capable of accommodating a design speed of 80 km/h with a superelevation of 0.035.

d. The existing north intersection immediately east of proposed intersection should be closed.

**Response:** Yes, the existing access will be closed.

2. **(Comment #7)** We also require an operational analysis (showing design vehicle turning left into the development, left out of the development) at this intersection to determine if there will be any stacking distance issues between the first access from Highway 2A and the realigned Broadway Avenue, as well as a drawing that shows storage lengths.

The capacity analysis results showing eastbound vehicle queue at the Highway 2A intersection will not reach the Broadway Avenue intersection addresses local road concerns. We would like to see the design vehicle operational analysis done at the TIA stage to look at whether traffic spills onto Highway 2A and reaffirm the appropriate location of the local road intersection from Highway 2A.

**Response:** The East-West Collector Road and Broadway Avenue intersection will be controlled by one stop sign on Broadway Avenue with free flow conditions on the Collector Road. Therefore, no vehicle queue will occur for the westbound traffic on the Collector Road at the Broadway Avenue intersection. As such, traffic will not spill onto Highway 2A.

3. (Comment #8) There does not appear to be developments east or south of the development where pedestrians require access, and accordingly, pedestrian warrants are not needed. Please confirm pedestrian requirements with the Town.

How do you envision the potential for pedestrian traffic wanting to access the commercial destination at Blackfalds Crossing from the east side of Highway 2A?

**Response:** Currently there are no pedestrian facilities (e.g., sidewalks or trails) provided along Highway 2A or in the vicinity of the Broadway Avenue intersection. If the Town wants to provide pedestrian facilities in the future, pedestrian traffic will be accommodated by providing marked crosswalks and pedestrian signals at the signalized intersection; or marked pedestrian crosswalks with associated signing, with the crossings safely located in accordance with NCHRP 672 - Roundabouts: An Information Guide if a roundabout is constructed.

4. **(Comment #9)** In addition to the roundabout analysis, we also require a cost/benefit analysis (as per design bulletin #68/2010) since the TIA finds that a roundabout works at this location.

Section 1.0 Economic Analysis of the design bulletin requires that "an economic analysis shall be undertaken to assist in evaluating the preferred type of intersection control as per the current version of the Department's Benefit Cost Guide, that accounts for all cost and benefits over the design period". Alberta



Transportation has consulted with the Town of Blackfalds and we would like to see an economic analysis as part of this TIA to establish the feasibility of a roundabout at this location.

**Response:** WSP performed an economic analysis based on TRB's "Estimating the Life-Cycle Cost of Intersection Designs". The results reveal that the roundabout option will have a lower life-cycle cost than signals. However, the initial construction costs of the roundabout are much higher than the proposed signalized intersection. The stacking distance between Highway 2A and Broadway Avenue for the roundabout will be shorter than that for signals since a roundabout will occupy more land area than a signalized intersection. WSP recommends installing traffic signals and protecting the right-of-way for a potential future roundabout.

Thank you for your comments. Should you have any questions, please do not hesitate to contact me at james.sun@wspgroup.com or 780.233.0757.

Yours truly,

3

WSP Canada Inc.

James Sun, MSc., P. Eng. Transportation Engineer

Cc: Craig Suchy, P. Eng., Branch Manager – Red Deer Janis Fong, P. Eng., Urban Transportation Manager – Northern Alberta



Office of the Operations Manager Central Region

June 9<sup>th</sup>, 2016

#401, 4920 - 51 Street Red Deer, Alberta Telephone 403/340-5166 Fax 403/340-4876

File: Blackfalds (ASP) WSP File: O/Ref 151-02471-00

WSP 300, 9925 – 109 Street Edmonton, AB T5K 2J8 Sent via email to: James.Sun@wspgroup.com

Attention: James Sun, Transportation Engineer

### RE: PROPOSED BLACKFALDS CROSSING TRAFFIC IMPACT ASSESSMENT (TIA) NE 22-39-27-W4 (ELKAY DEVELOPMENTS), HIGHWAYS 2A & 597

Thank you for the opportunity to provide input on the Blackfalds Crossing TIA review. I would advise that Alberta Transportation has reviewed your comments provided on May 30<sup>th</sup>, 2016 and offer the following comments:

- As you are aware, Design Bulletin #68/2010 is a new policy requiring TIAs to review and assess roundabout as the first option for improvements to existing intersections or when constructing new intersections on the provincial highway network. Since the cost benefit analysis clearly demonstrates the economic, social and environmental benefits of a roundabout compared to a conventional signalized intersection at this location, a roundabout option is to be implemented at the Developer's/Town's cost.
- 2. Please revise the TIA to reflect the implementation of a roundabout at Highway 2A and the realigned Broadway Avenue intersection.
- 3. The Area Structure Plan (ASP) may need to be revised as well, and the roundabout is to be protected for at the subdivision stage.
- 4. I would confirm that the Town of Blackfalds would be responsible for arranging all required intersectional improvements to accommodate the proposed development. A Roadside Development Permit Application is required for Highway 2A & Broadway Avenue and Highway 597 & the North-South Collector Access.

We look forward to receiving a revised copy with these amendments incorporated in the TIA and if required, the ASP, for review prior to final endorsement.

Should you wish to schedule a meeting to clarify or discuss any of these points, please contact me at 403-340-5166.

Sincerely,

Sandy Choi Development & Planning

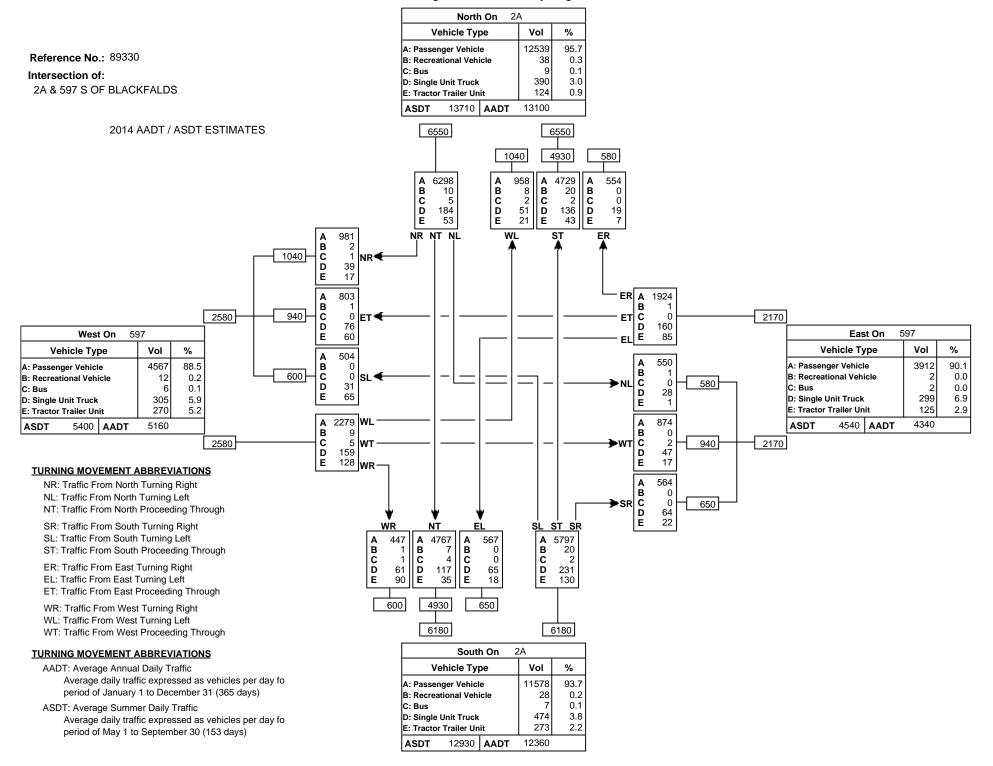
SC/sc

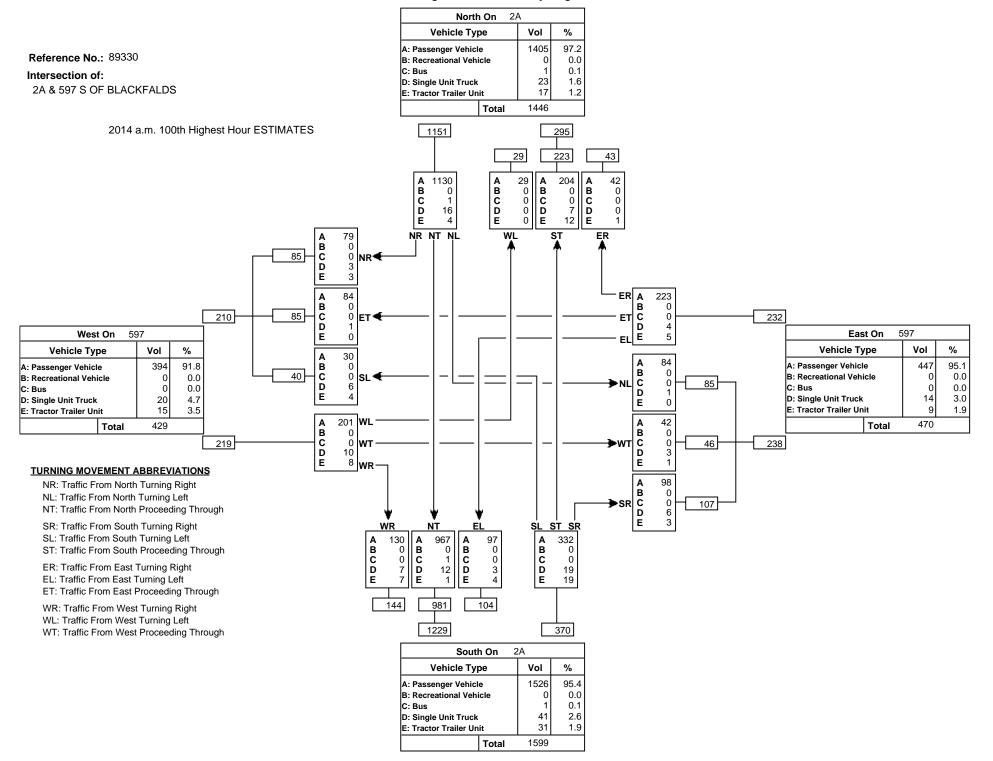
cc: Preston Weran - <u>PWeran@blackfalds.com</u> Terry Topolnitsky – <u>Terry@blackfalds.com</u> Stuart Richardson, Infrastructure

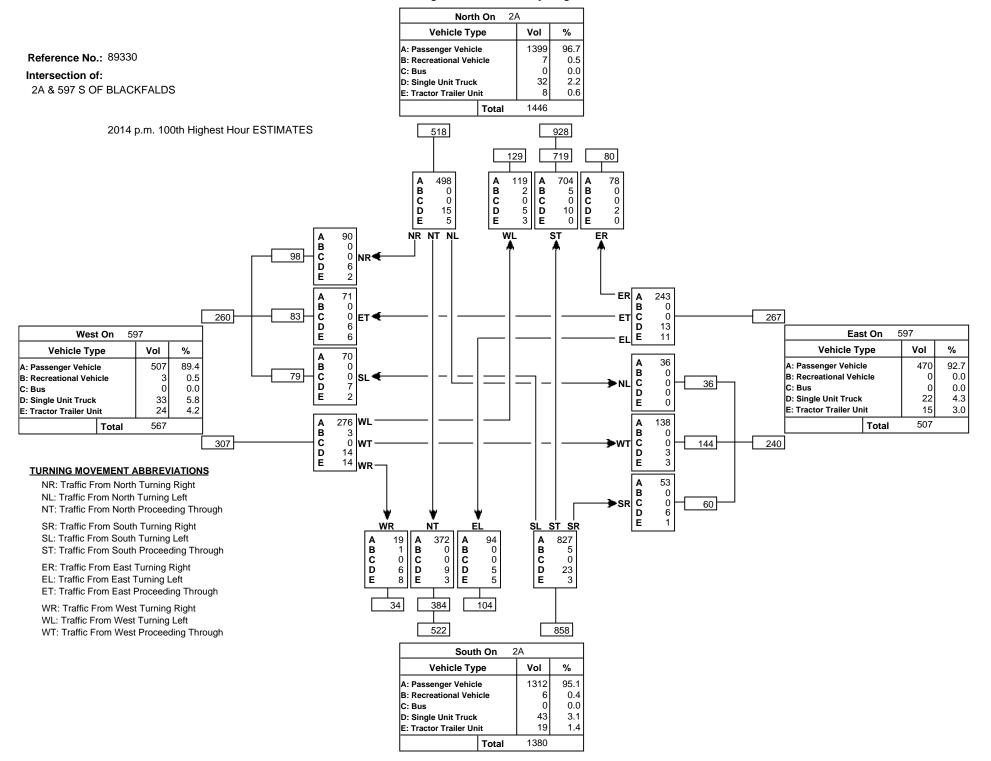
## Appendix B

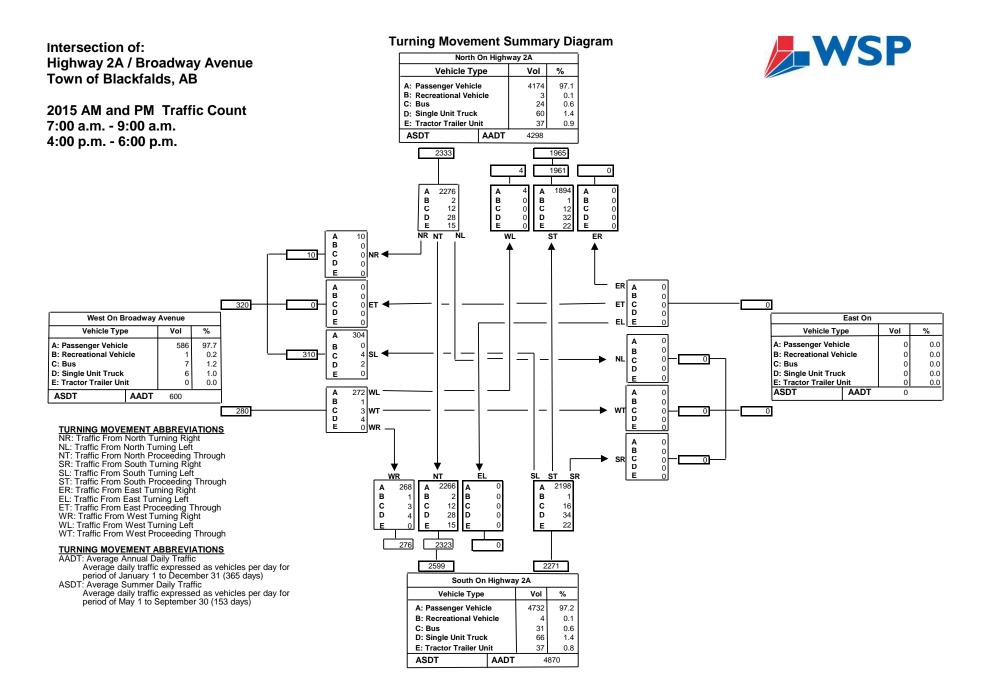
## TRAFFIC ANALYSIS

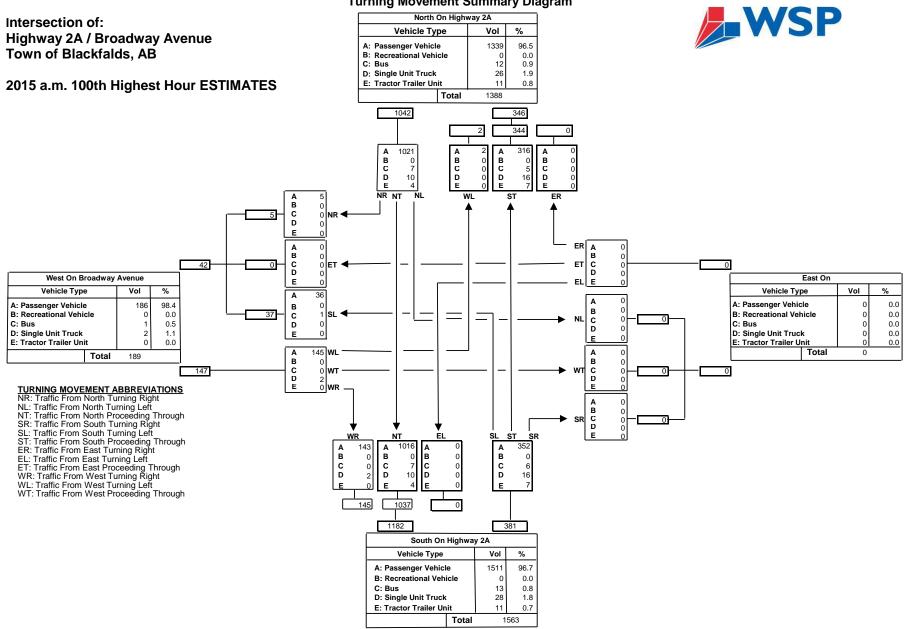
- Traffic Turning Movements
- Traffic Volume History on Highway 2A and Highway 597
- Trip Distribution and Assignment for Each Land Use
- C-TEP Trip Generation Rates for Highway Commercial

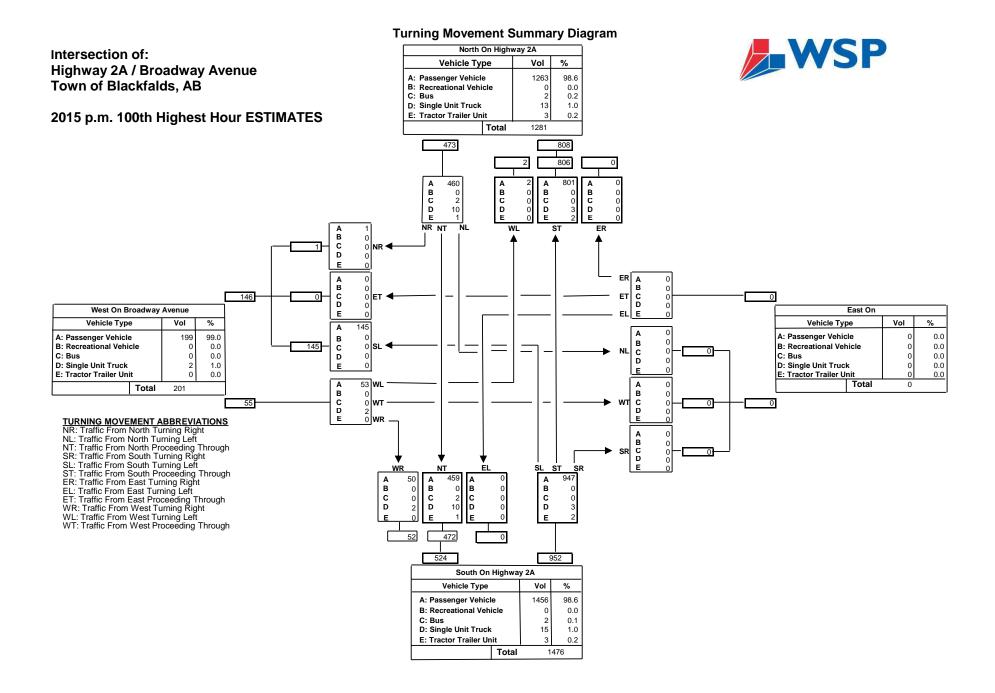












### Intersection of: South Street / East Railway Street Town of Blackfalds, AB

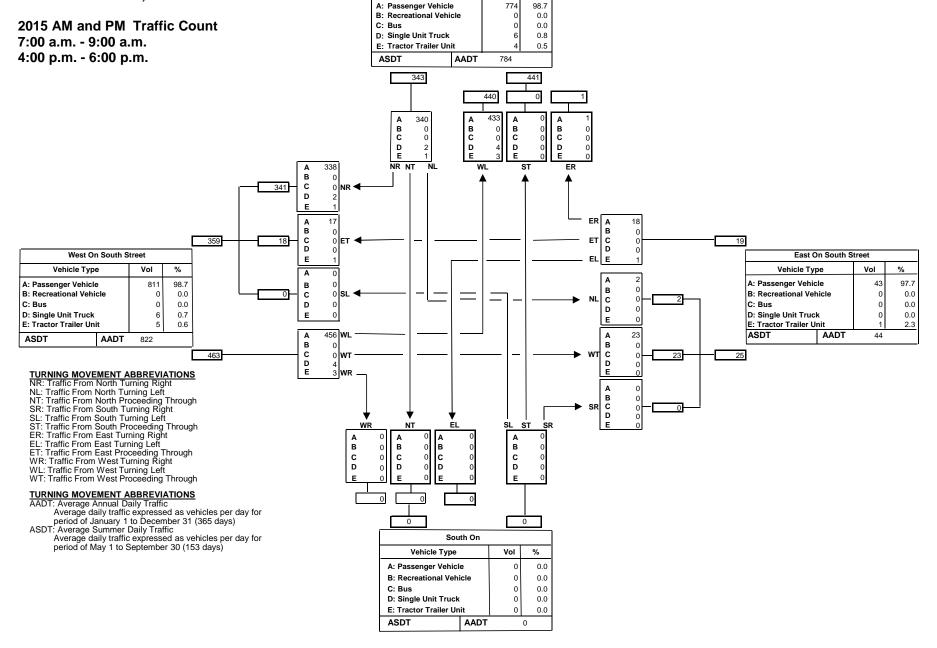
## Turning Movement Summary Diagram

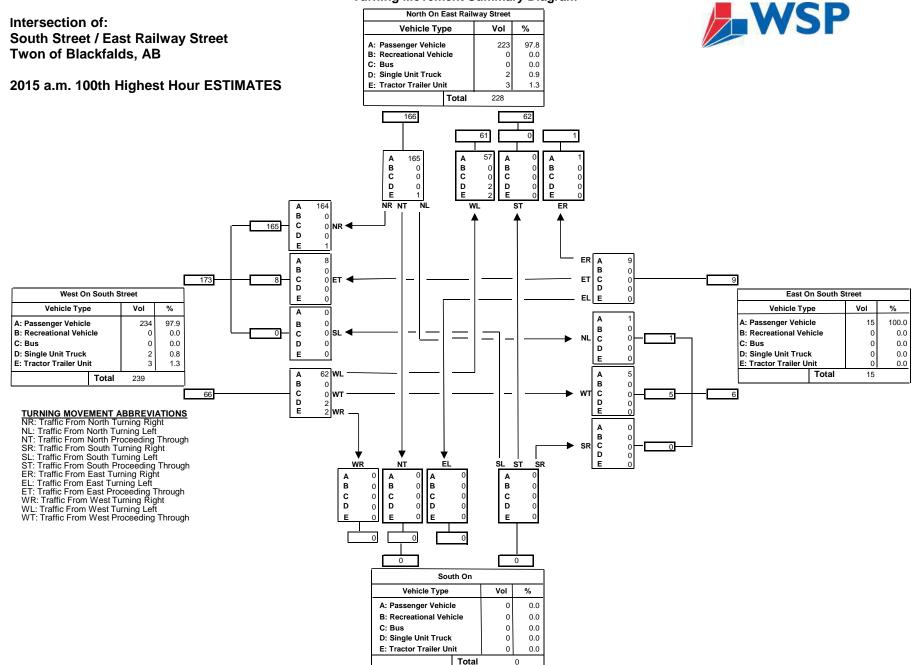
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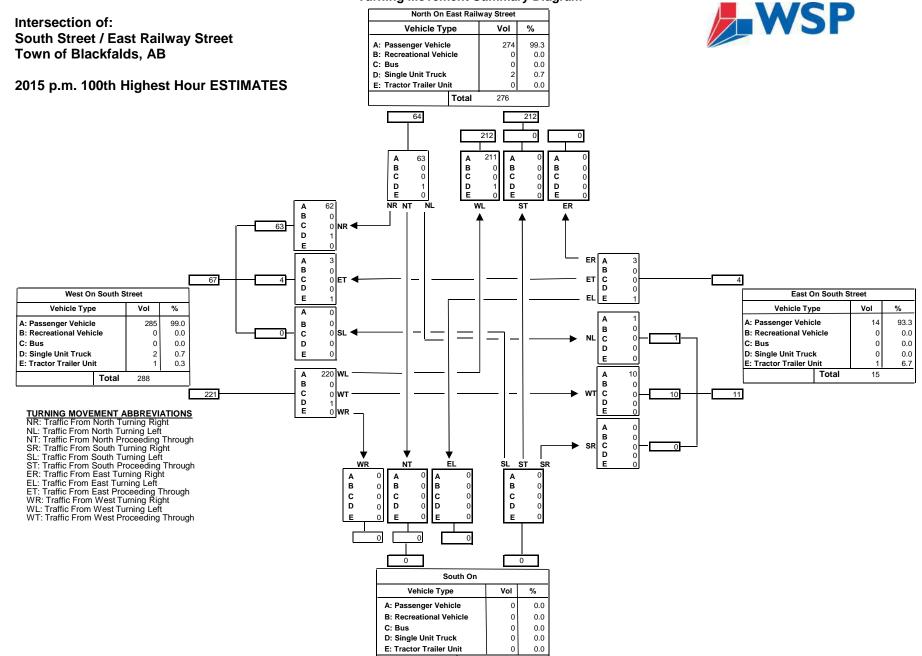
%

Vehicle Type









Total

0

# Alberta Transportation Modeling and Analysis

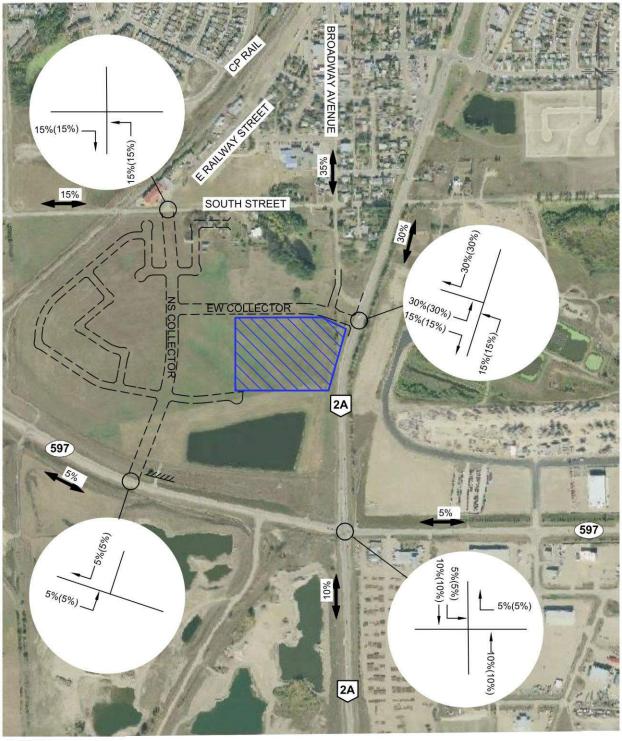
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Produced: 18-Feb	Produced: 18-Feb-2015 By CornerStone Solutions Inc.										
Hwy CS TCS	Muni Location Description	2005 AADT	2006 AADT	2007 AADT	2008 AADT	2009 AADT	2010 AADT	2011 AADT	2012 AADT	2013 AADT	2014 AADT
A 16		-	-			-		2920	3100	3280	3360
2 A 16 08	RdDr S OF 42 & 592 N OF PENHOLD	3960	4140	4580	4130	5320	5440	5580	5970	6330	6600
2 A 16 08	RdDr 0.8 KM N OF 2A & 42 PENHOLD	4690	5000	5400	4800	5940	6100	6170	6570	6950	7200
2 A 16 12	RdDr N OF 42 & 592 N OF PENHOLD	4580	4760	5260	4660	5710	5830	6140	6550	6930	7140
2 A 16 12	RdDr S OF TWP RD 372 12-37-28-40200000	4450					6070	6140	6550	6930	7140
2 A 16 12	RdDr N OF TWP RD 372 12-37-28-40200000	5320					8100	2066	8520	9040	9510
2 A 16 12	RdDr S OF MCKENZIE RD 19-37-27-406500000	5960	6200	6840	6780	7940	8100	2066	8520	9040	9510
2 A 16 12	RdDr N OF MCKENZIE RD 19-37-27-406500000	6740	7010	7730	6250	7320	7480	7010	7480	2000	8290
2 A 16 12	RdDr S OF LANTERN ST, RED DEER 32-37-27-415501560				6250	7320	7480	7010	7480	2000	8290
2 A 16 12	RdDr N OF LANTERN ST, RED DEER 32-37-27-415501560				10650	11810	11560	11900	12700	13360	14050
2 A 16 99	CoRD W OF 2 & TAYLOR DR IN RED DEER	8000	8450	9610	10650	11810	12070	13020	13890	14610	15350
	RdDr N OF 11A AT RED DEER	13920	14900	15020	14140	13870	14130	14530	14850	15170	15420
A 18	RdDr S OF CENTRAL PARK RD 3-39-27-406000000	13490	14440	14560	13710	12990	13230	13550	14500	14800	15050
2 A 18 16	RdDr N OF CENTRAL PARK RD 3-39-27-406000000	12880	13790	13910	13600	12900	13140	13470	14130	14430	14680
18	RdDr 1.6 KM N OF 2A & 11A RED DEER	12880	13940	13830	13640	12810	13220	13510	14110	14450	14770
A 18	RdDr S OF NORTHLAND IND ACC 14-39-27-414251400	11450	12250	12350	12070	11440	11210	11490	11830	12090	12310
A 18	RdDr N OF NORTHLAND IND ACC 14-39-27-414251400	11610	12430	12550	12270	11640	11300	11580	11920	12180	12400
A 18	Laco S OF 597 S OF BLACKFALDS	11050	11860	11960	11700	11020	11220	11500	11900	12160	12360
	Laco N OF 597 S OF BLACKFALDS	10610	11250	11290	11070	10800	10990	11270	12620	12880	13100
∢	Laco S OF INDIANA ST IN BLACKFALDS 26-39-27-413401350	10440	11080	11120	10900	10140	10340	10600	11560	11800	12660
18	Laco N OF INDIANA ST IN BLACKFALDS 26-39-27-413401350	8680	9220	9240	0906	9080	9260	9500	10360	10580	11600
∢	Laco S OF PARK ST IN BLACKFALDS 26-39-27-413101230	8680	9220	9240	0906	9080	9260	9500	10360	10580	11600
A 18	Laco N OF PARK ST IN BLACKFALDS 26-39-27-413101230	7130	7570	7350	7210	7240	7370	7550	7520	7660	8260
A 18	Laco S OF GREGG ST IN BLACKFALDS 26-39-27-411750805	7130	7570	7350	7210	7240	7370	7550	7520	7660	8260
	Laco N OF GREGG ST IN BLACKFALDS 26-39-27-411750805	7310	7770	7720	7600	7640	7790	7990	7010	7150	7590
A 18	Laco S OF C&E TRAIL 26-39-27-409500325 SJ	7320	7780	7730	7610	7650	7800	8000	7010	7150	7590
A 18	Laco N OF C&E TRAIL 26-39-27-409500325 SJ	6680	7100	7050	6810	6870	7000	7180	6250	6370	6750
	Laco S OF TWP RD 400 35-39-27-408050000	6680	7100	7050	6810	6870	7000	7180	6250	6370	6750
A 18		6800	7220	7200	7020	7170	7300	7480	6590	6630	7040
	OF C & E TRAIL S OF LACOMBE 13-40-27-40400030	6930	7350	7350	7240	7310	7450	7400	6520	6560	6980
A 18	Z	5730	6070	6070	6100	6070	6190	5900	5220	5260	5600
A 20	Laco S OF LACOMBE AIRPORT ACC 32-40-26-402000000	5300	5500	5760	5980	5940	6060	6000	5660	6480	6890
A 20	Laco N OF LACOMBE AIRPORT ACC 32-40-26-40200000	4360	4520	4740	4500	4480	4560	4520	4430	5080	5410
A 20		4030	4200	4370	4440	4390	4530	4460	4450	5090	5470
A 20	Laco S OF C&E TRAIL 4-41-26-408050000	4030	4180	4370	4440	4410	4500	4460	4430	5080	5410
20		4310	4480	4650	4720	4690	4780	4770	4970	5710	6080
A 20	Laco S OF MILTON RD 9-41-26-407501300	4310	4480	4650	4720	4690	4780	4770	4970	5710	6080
20	Laco N OF MILTON RD 9-41-26-407501300	3510	3640	4030	4080	4050	4120	4210	4380	5030	5360
		4160	4360	4400	4390	4300	4440	4360	4400	4800	5100
	Phka S OF 604 N OF MORNINGSIDE	4170	4370	4400	4390	4300	4440	4600	4640	4850	5150
	24.400										
	01 108	MH GZ:ZI GL0Z/81/Z	M							71 V M 2005-2014. NS	

# Alberta Transportation Modeling and Analysis

Produced: 18-Feb-2015 By CornerStone Solutions Inc.

Froduce	20. 10-L C											
Hwy	CS TCS	Muni Location Description	2005 AADT	2006 AADT	2007 AADT	2008 AADT	2009 AADT	2010 AADT	2011 AADT	2012 AADT	2013 AADT	2014 AADT
590	02 16	RdDr W OF 21 S OF DELBURNE	600	910	880	880	880	880	880	870	870	870
590	04 04	RdDr E OF 21 S OF DELBURNE	530	940	870	870	850	850	850	940	940	940
590	04 04	Stet W OF RGE RD 212 22-35-21-40000000	460	550		780	760	760	760	760	660	660
590	04 04	Stet E OF RGE RD 212 22-35-21-400000000	460	550		780	760	760	760	760	660	660
590	04 04	Stet W OF 835 W OF BIG VALLEY	620	630	630	770	760	760	760	760	660	660
590	04 08	Stet E OF 835 W OF BIG VALLEY	600	610	610	760	760	760	760	760	650	650
590	04 08	Stet W OF 56 NE OF BIG VALLEY	460	550	540	540	540	540	540	520	520	520
591	02 04	CIrw E OF 734 SW OF RICINUS	80	80	80	80	80	80	80	80	120	120
591	02 04	CIrw W OF SWAN LAKE ACC 25-35-9-503501550	80	80	80	80	80	80	80	80	160	160
591	02 06	CIrw E OF SWAN ALKE ACC 25-35-9-503501550	180	180	180	160	160	160	160	160	220	220
591	02 06	CIrw W OF 22 & 54 W OF CAROLINE WJ	800	820	820	820	800	820	930	930	930	930
592	02 08	RdDr E OF 781 NW OF PENHOLD	1040	1060	1060	1100	1170	1170	1170	1170	1260	1260
592	02 08	RdDr W OF RGE RD 10 36-36-1-500000000	1090	1120		1230	1300	1300	1300	1300	1290	1290
592	02 08	RdDr E OF RGE RD 10 36-36-1-50000000	1310	1340		1430	1500	1500	1500	1500	1540	1540
592	02 08	RdDr W OF C & E TRAIL 283A 33-36-28-401000000	1550	1580	1650	1620	1780	1780	1780	1780	1780	1800
592	02 08	RdDr E OF C & E TRAIL 283A 33-36-28-401000000	1370	1420	1470	1440	1540	1540	1540	1540	1540	1630
592	02 08	RdDr W OF 2A & 42 N OF PENHOLD	1700	1780	1850	1820	1870	1870	1880	1920	1940	2430
593	02 04		140	140	140	140	200	200	200	200	200	120
593	02 04	Stet W OF 853 N OF BYEMOOR	60	60	60	60	100	100	100	100	100	60
594	02 04	Stet E OF 835 SW OF ERSKINE	80	80	80	80	80	80	80	80	80	80
594	02 04	Stet W OF 56 S OF WARDEN	110	180	180	180	180	180	140	140	140	140
595	02 04	RdDr W OF 808 SE OF RED DEER	2600	2620	2420	2920	3200	3080	3080	3140	3280	3780
595	02 08	RdDr E OF 808 SE OF RED DEER	2490	2510	2310	2810	2760	2640	2640	2680	2800	2880
595	-	RdDr W OF 816 NW OF PINE LAKE	2440	2460	2260	2760	2620	2530	2520	2560	2660	2730
595	02 12	RdDr E OF 816 NW OF PINE LAKE	1780	1800	1660	2030	2060	1980	1970	2010	2090	2190
595	02 12	RdDr 4.8 KM E OF 595 & 816 NW DELBURNE	1700	1590	1610	1940	1980	1930	1890	1930	2000	2100
595	02 12	RdDr W OF 21 NW OF DELBURNE	1520	1540	1430	1610	1700	1650	1650	1680	1730	1780
597	02 04	Laco E OF 2 W OF BLACKFALDS	4100	4390	4480	4480	6700	6780	6780	7280	9720	0686
597	02 04	Laco W OF RGE RD 273 BLACKFALDS 22-39-27-412400245								7280	9720	9890
597	02 04	Laco E OF RGE RD 273 BLACKFALDS 22-39-27-412400245								4820	5420	5500
597	02 04	Laco W OF 2A S OF BLACKFALDS	2720	2900	2940	2940	3660	3730	3730	4620	5060	5160
597	02 08	Laco E OF 2A S OF BLACKFALDS	3440	3590	3610	3610	2680	2720	2720	4020	4260	4340
597	02 08	Laco W OF PRENTISS RD (RGE RD 260) 12-39-26-400000000	860	1140	1140	1140	1140	1270	1270	1270	1270	1270
597	02 08	Laco E OF PRENTISS RD (RGE RD 260) 12-39-26-400000000	870	1180	1180	1180	1180	1220	1220	1220	1220	1220
597	02 08	Laco W OF 815 N OF JOFFRE	720	810	810	810	810	810	810	810	810	720
598	-	CIrw E OF 11 & 11A ROCKY MOUNTAIN HOUSE	7640	7890	7890	6150	5850	5970	6280	6410	6640	6710
598						2790	2650	2710	3050	3110	3140	3180
598		Cirw E OF RGE RD 71 SJ 26-39-7-50000940				2710	2570	2630	2970	3030	3080	3120
598						2710	2570	2630	2970	3030	3080	3120
598	02 04	Clrw E OF RGE RD 71 EJ 25-39-7-514900815				2720	2580	2640	2980	3040	3080	3120
			1 30.01 310001010									
	гаде	Page 117 of 168	MH 62:21 6102/81/2	N							HI VHZ005-Z014.XIS	



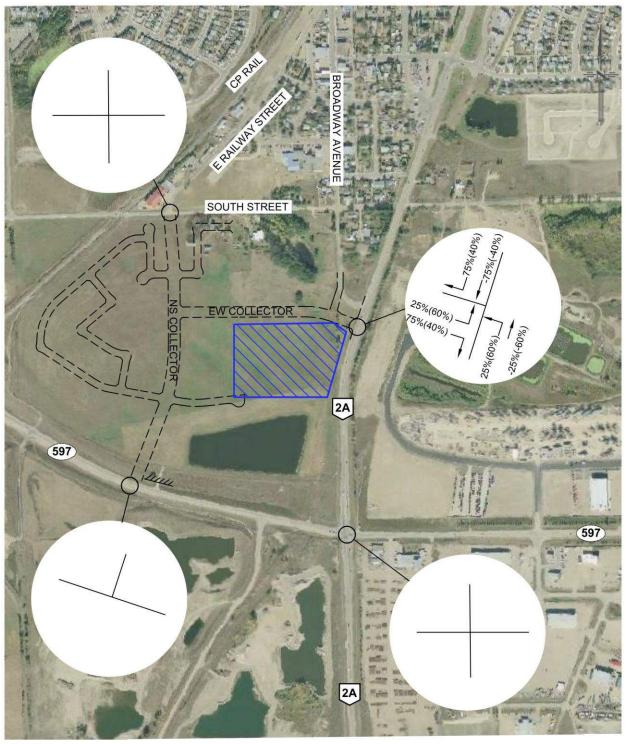
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NOT TO SCALE

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PROPOSED COMMERCIAL DEVELOPMENT

Trip Distribution (Shopping Center - Stage 1) - Non-Pass-By Trips

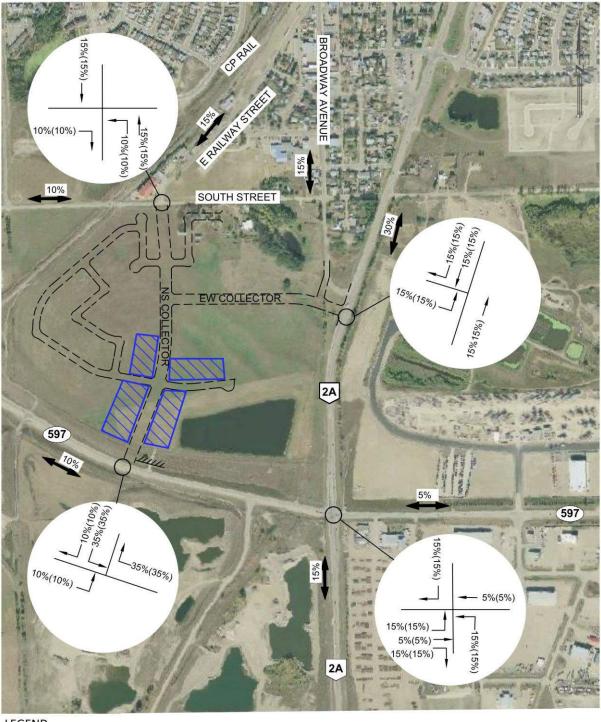


X(Y) AM PEAK (PM PEAK)

PROPOSED COMMERCIAL DEVELOPMENT

NOT TO SCALE

Trip Distribution (Shopping Center – Stage 1) - Pass-By Trips



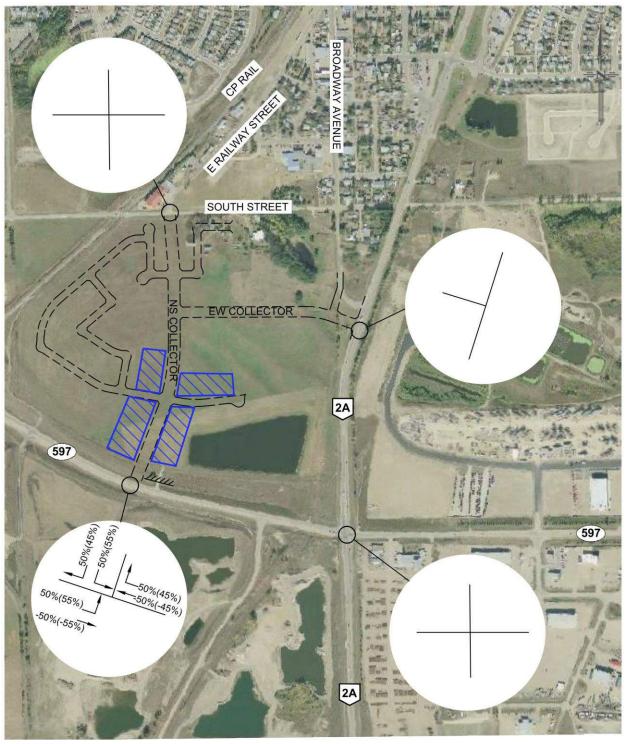
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PROPOSED COMMERCIAL DEVELOPMENT

Trip Distribution (Highway Commercial – Stage 2) – Non-Pass-By Trips



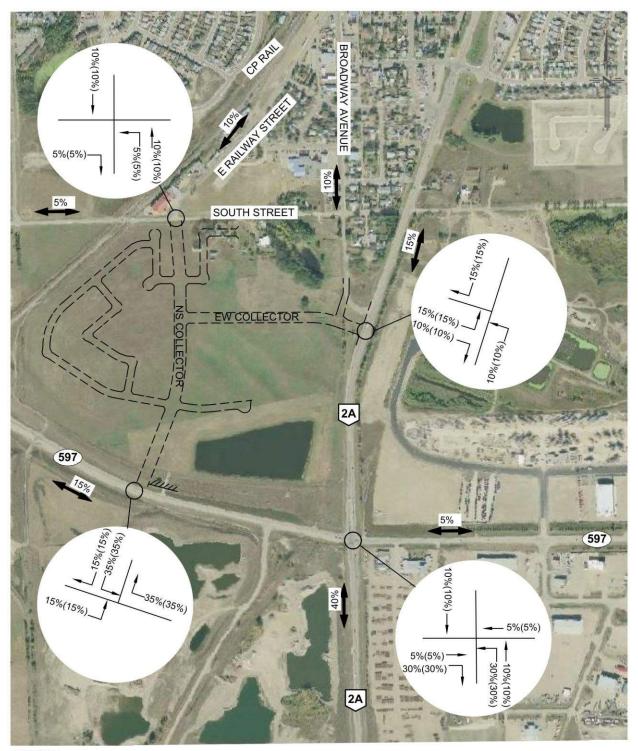
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PROPOSED COMMERCIAL DEVELOPMENT

Trip Distribution (Highway Commercial – Phase 2) - Pass-By Trips

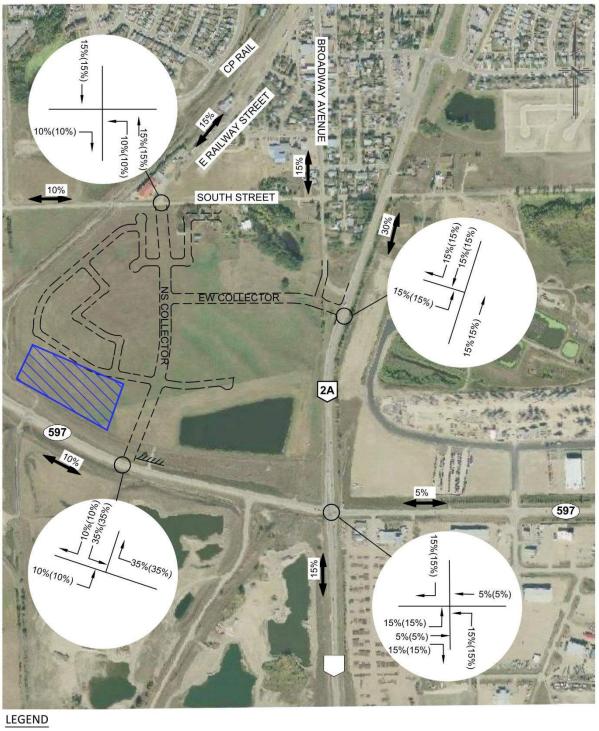


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 AM PEAK (PM PEAK)

NOT TO SCALE

Trip Distribution (Residential)



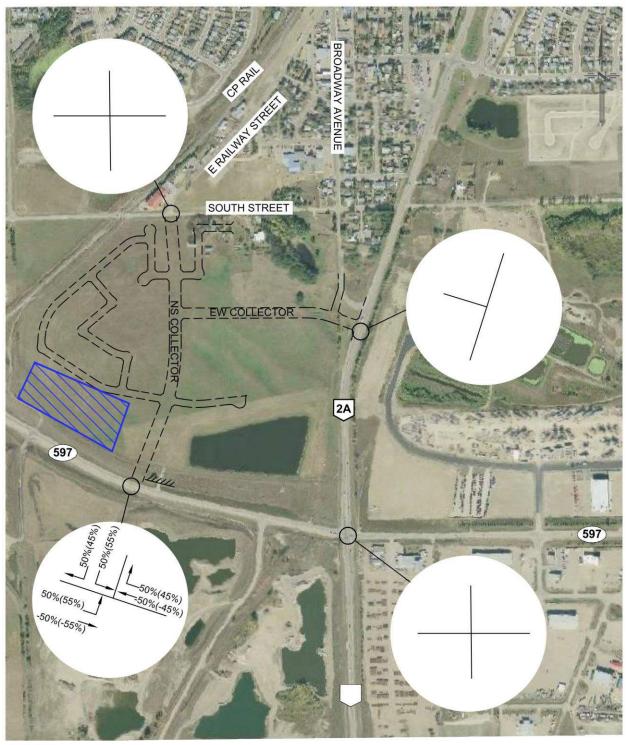
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PROPOSED MIXED USE COMMERCIAL DEVELOPMENT

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Trip Distribution (Mixed Use Housing - Commercial) - Non-Pass-by Trips



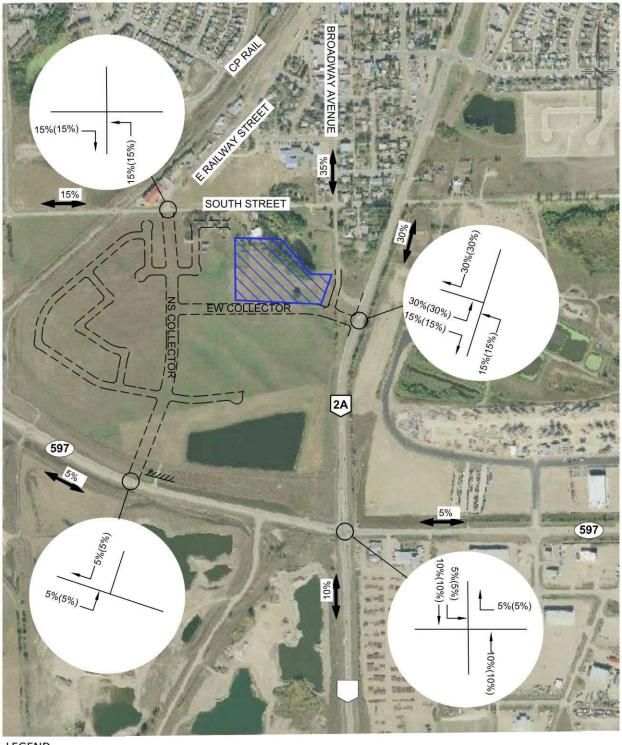
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PROPOSED MIXED USE COMMERCIAL DEVELOPMENT

Trip Distribution (Mixed Use Housing - Commercial) – Pass-by Trips



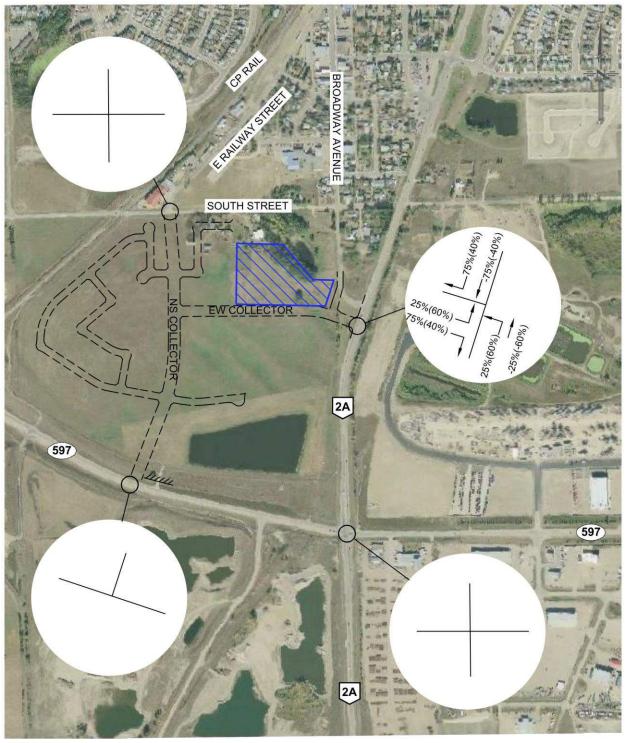
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X(Y) AM PEAK (PM PEAK)

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PROPOSED COMMERCIAL DEVELOPMENT

Trip Distribution (Highway Commercial – Future Development) – Non-Pass-By Trips



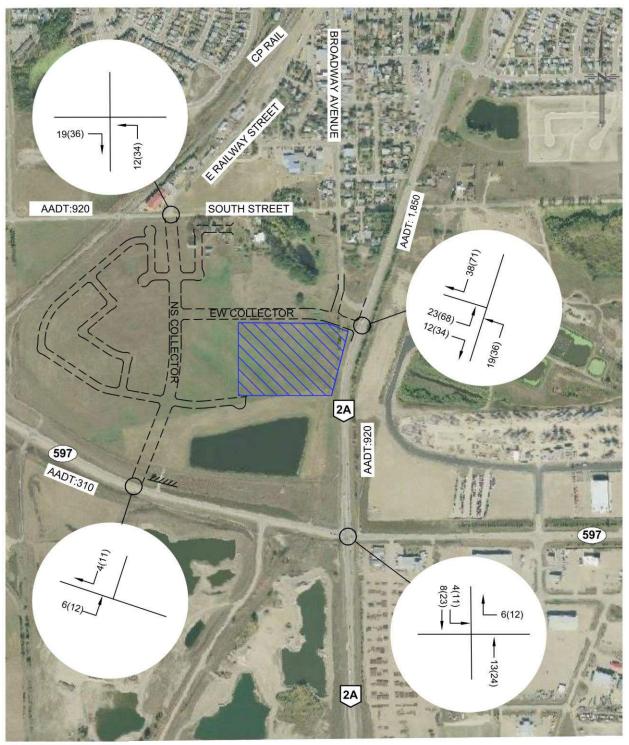
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PROPOSED COMMERCIAL DEVELOPMENT

NOT TO SCALE

Trip Distribution (Highway Commercial – Future Development) – Pass-By Trips



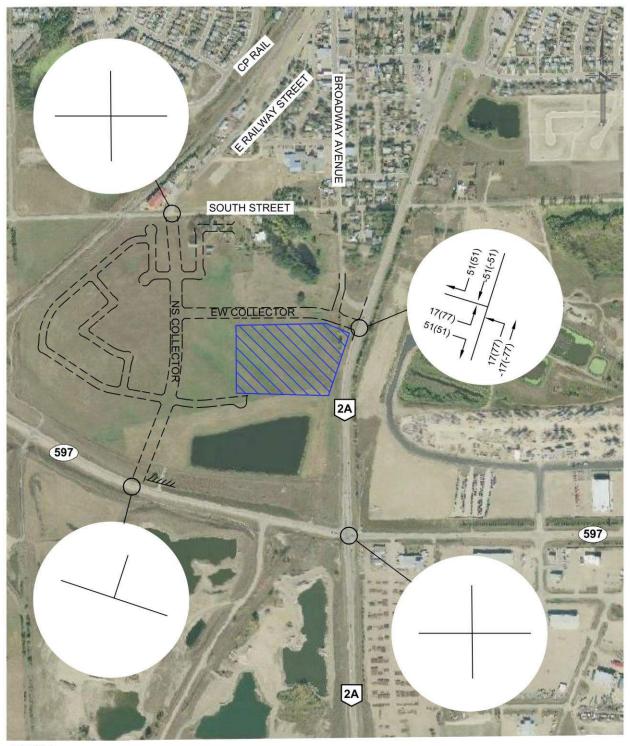


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PROPOSED COMMERCIAL DEVELOPMENT

Trip Assignment (Shopping Center) – Non-Pass-By Trips

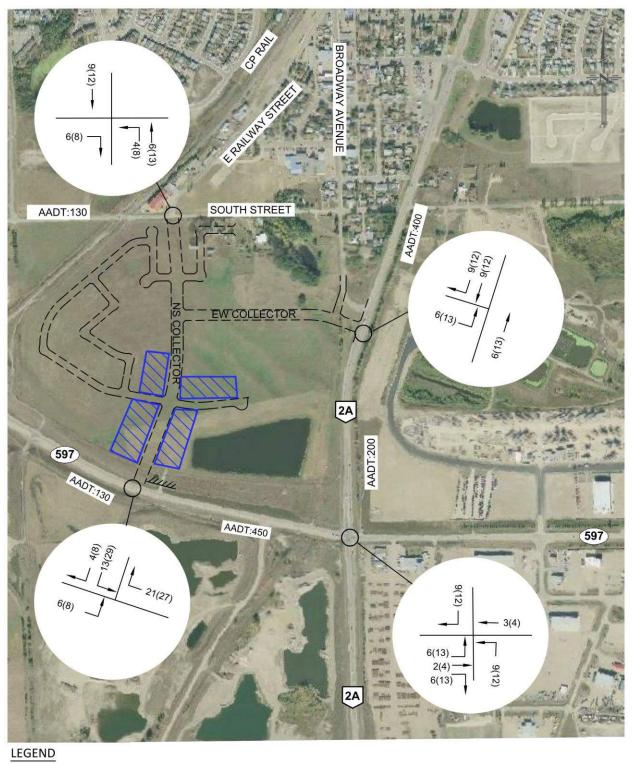


X(Y) AM PEAK (PM PEAK)

PROPOSED COMMERCIAL DEVELOPMENT

NOT TO SCALE

Trip Assignment (Shopping Center) – Pass-By Trips

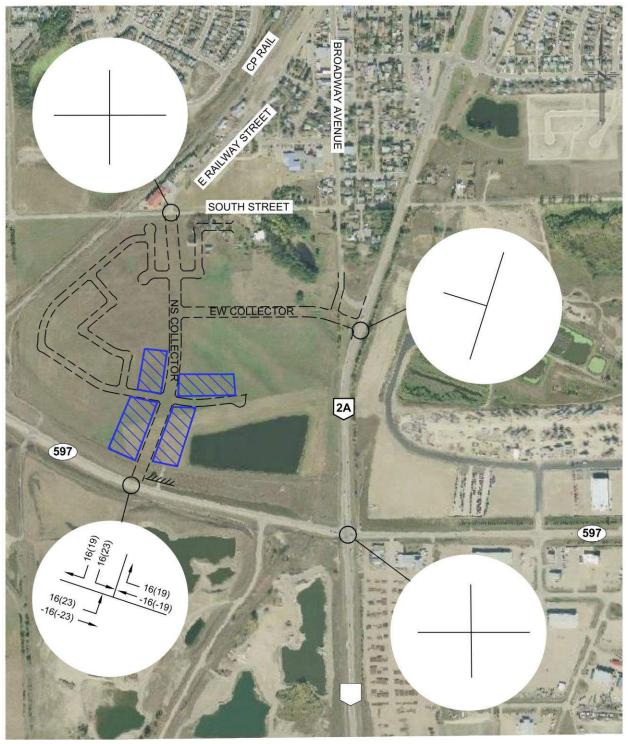


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NOT TO SCALE

PROPOSED COMMERCIAL DEVELOPMENT

Trip Assignment (Highway Commercial – Stage 2) – Non-Pass-By Trips



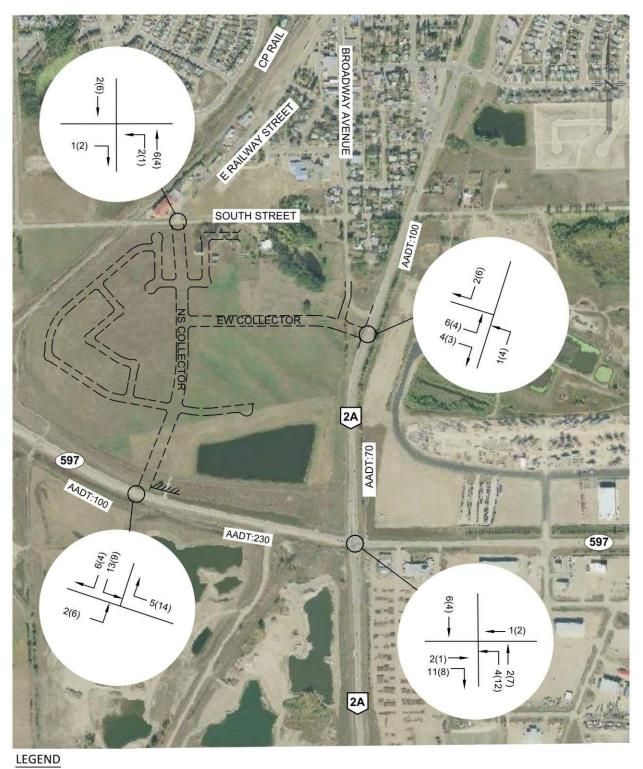
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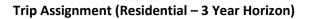
PROPOSED COMMERCIAL DEVELOPMENT

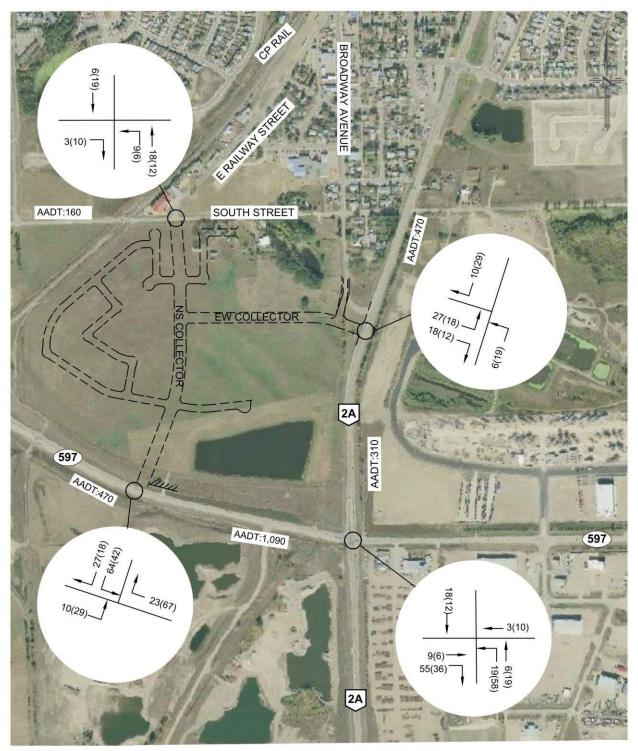
Trip Assignment (Highway Commercial – Stage 2) – Pass-By Trips





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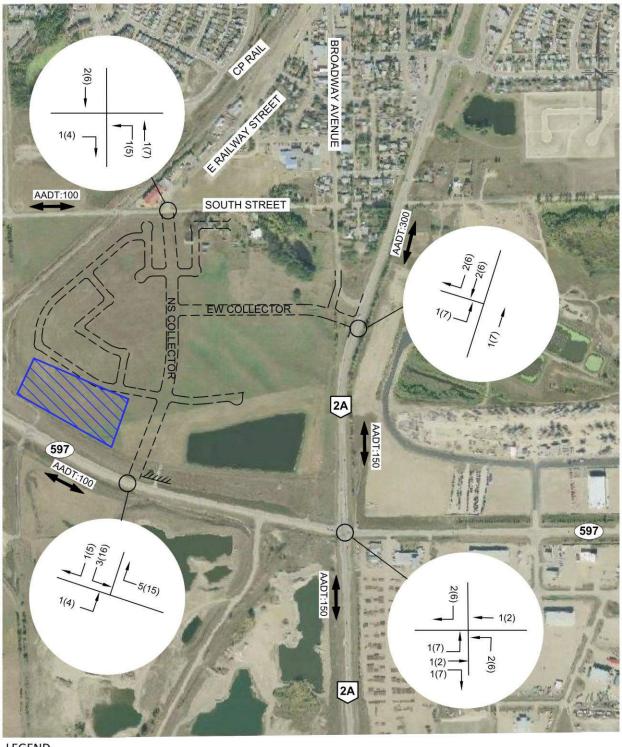






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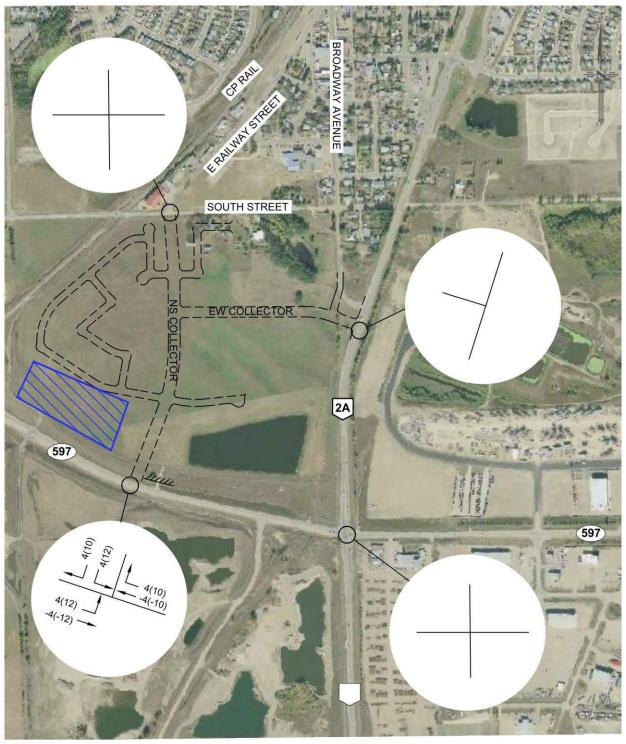
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PROPOSED MIXED USE COMMERCIAL DEVELOPMENT

Trip Assignment (Mixed Use Housing Commercial) – Non-Pass-by Trips



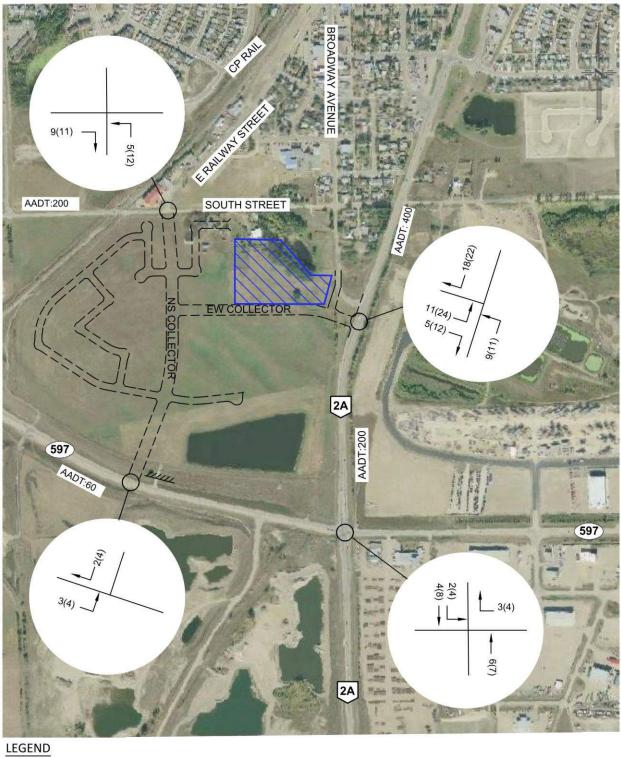
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PROPOSED MIXED USE COMMERCIAL DEVELOPMENT

Trip Assignment (Mixed Use Housing Commercial) – Pass-by Trips



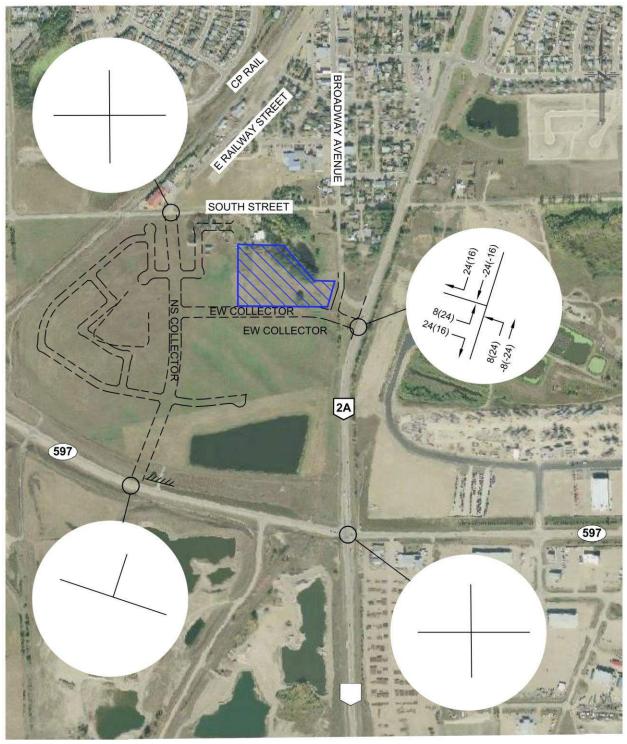
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X(Y) AM PEAK (PM PEAK)

NOT TO SCALE

PROPOSED COMMERCIAL DEVELOPMENT

Trip Assignment (Highway Commercial – Future Development) – Non-Pass-By Trips



## LEGEND

X(Y) AM PEAK (PM PEAK)

PROPOSED COMMERCIAL DEVELOPMENT

NOT TO SCALE

Trip Assignment (Highway Commercial – Future Development) – Pass-By Trips

Land Use	Recommendation	Time Period	Industry (ITE)	Empirical Average
Hotel	Use ITE Further study	АМ	0.56/room 0.69/emp	0.36/room 2.64/emp
Hotel	Further study Further study	РМ	0.59/room 0.80/emp	0.33/room 2.61/emp
Residential	Use ITE	AM	0.78/unit	0.62/unit
Dwellings	Use ITE	РМ	1.01/unit	0.76/unit
High Cale al	Use ITE Use local data	АМ	0.41/stu 4.63/emp	0.45/stu 5.75/emp
High School	Further study Use local data	РМ	0.41/stu 1.55/emp	0.26/stu 3.43/emp
Highway	Use local data	AM	N/A	2.56/93 m <sup>2</sup> GFA
Commercial	Use local data	РМ	N/A	4.21/93 m <sup>2</sup> GFA
Multi-Family	Use ITE	AM	0.30-0.67 per unit	0.34/unit
Dwellings	Use ITE	PM	0.8-0.78 per unit	0.51/unit
	Use ITE Use ITE	АМ	1.55/93 m2 GFA 0.48/emp	1.82/93 m <sup>2</sup> GFA 0.86/emp
General Office	Use ITE Further study	РМ	1.49/93 m2 GFA 0.46/emp	2.23/ 93 m <sup>2</sup> GFA 1.01/emp
Medical/Dental	Further study Further study	АМ	2.48/93 m2 GFA 0.53/emp	9.19/93 m <sup>2</sup> GFA 2.87/emp
Office	Use local data	РМ	3.72/93 m2 GFA 1.06/emp	8.42/93 m <sup>2</sup> GFA 2.64/emp
	Further study	AM	1.03/93 m2 GLA	2.83/93 m <sup>2</sup> GFA
Strip Mall	Further study Use ITE	РМ	3.76 per 93 m2 GLA	4.03/93 m <sup>2</sup> GFA
D'. D. Classica	Use local dada	AM	N/A	1.99/93 m <sup>2</sup> GFA
Big Box Shopping	Use local data	РМ	N/A	2.52/93 m <sup>2</sup> GFA
Sit-Down	Use ITE Use ITE	АМ	0.47/seat 11.52/93 m2 GFA	0.30/seat 7.36/93 m <sup>2</sup> GFA
Restaurant	Further study Use local data	РМ	0.41/ seat 10.92/ 93 m2 GFA	0.25/seat 5.63/93 m <sup>2</sup> GFA
Fast Food	Further study Further Study	АМ	1.32/seat 53.11/93 m2 GFA	0.93/seat 26.58/93m <sup>2</sup> GFA
Restaurant	Use ITE Further Study	РМ	0.94/seat 34.64/93 m2 GFA	0.83/seat 21.15/93m <sup>2</sup> GFA
	Use ITE Use ITE	АМ	0.42/stu 5.19/emp	0.42/stu 4.74/emp
Elementary School	Use ITE Further Study	РМ	0.28/stu 3.45/emp	0.25/stu 2.75/emp

Table 1.2: Recommended Site Traffic Generation Rate

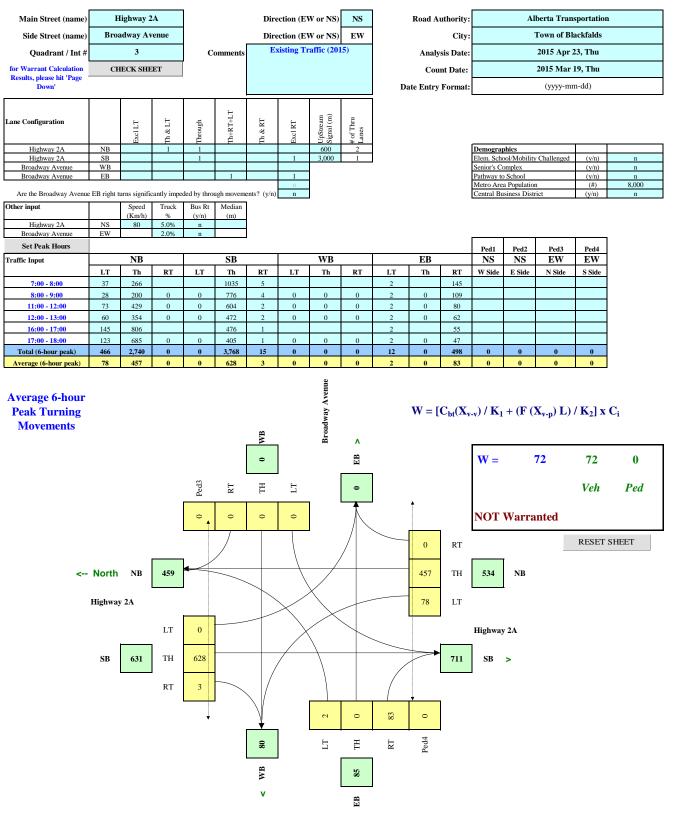
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# Appendix C

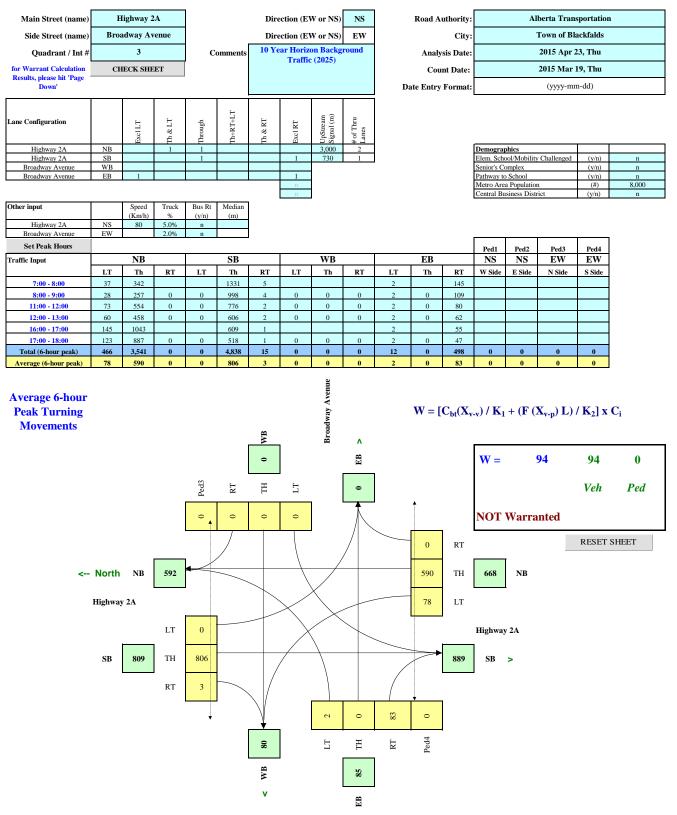
## **INTERSECTION ANALYSIS**

- Signal Warrant Analysis
- Left Turn Lane Warrant Analysis
- Illumination Warrant Analysis
- Proposed Intersection Improvement Concept plan for Highway 597 / South Access

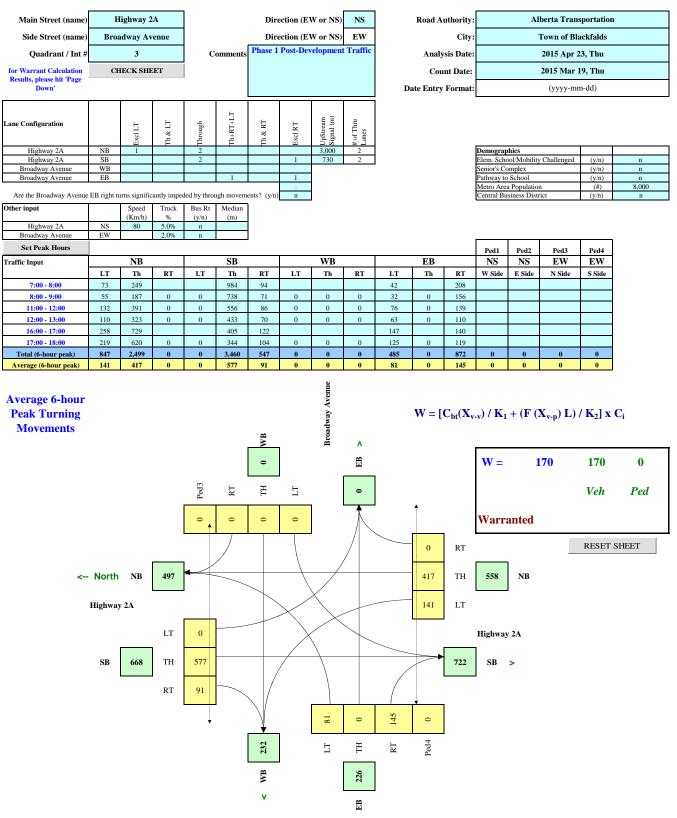




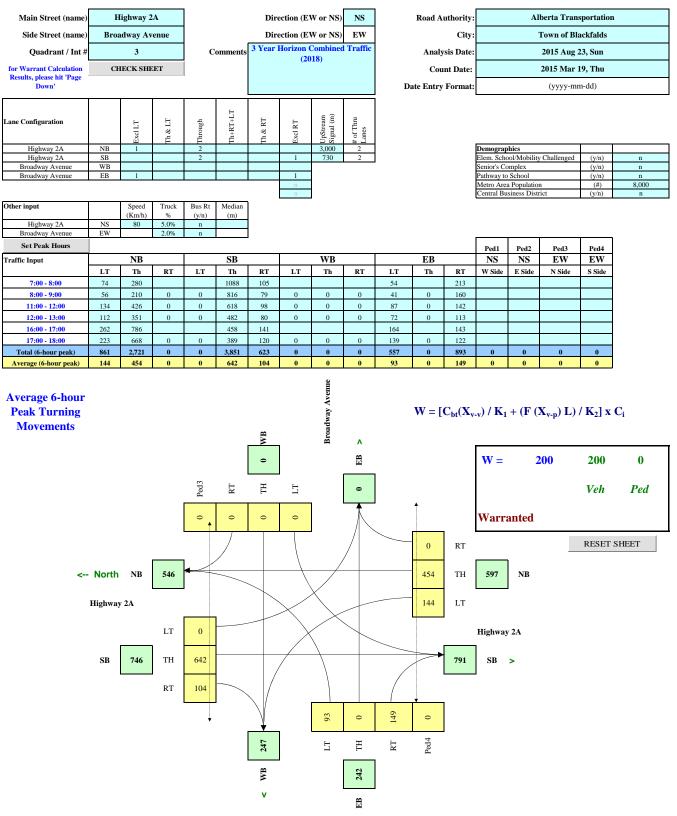




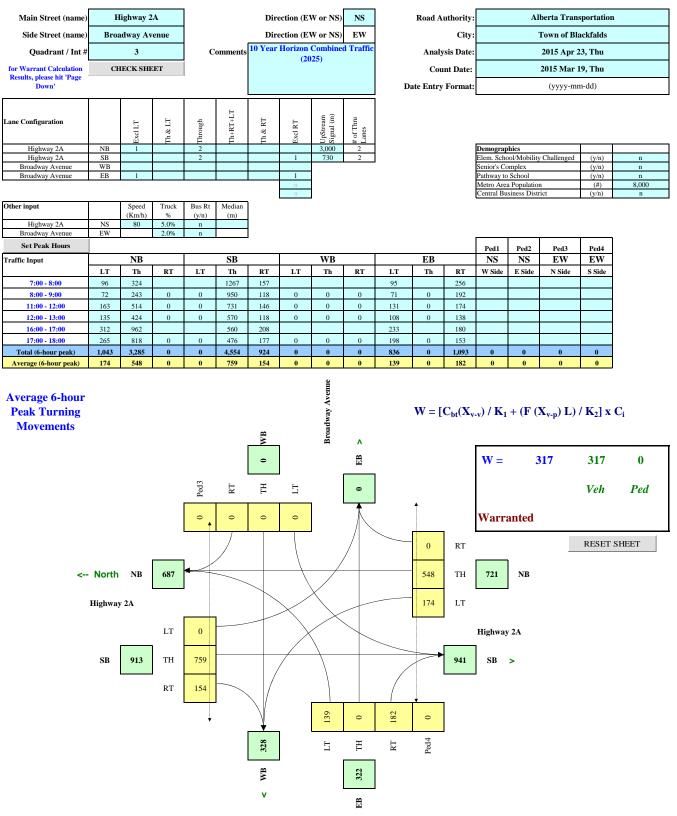




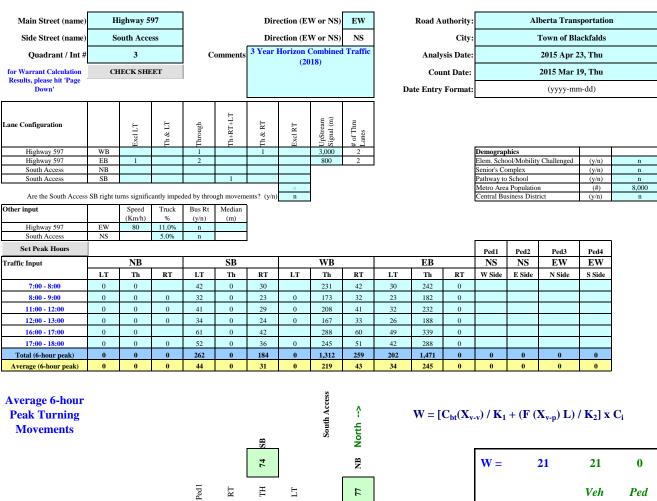


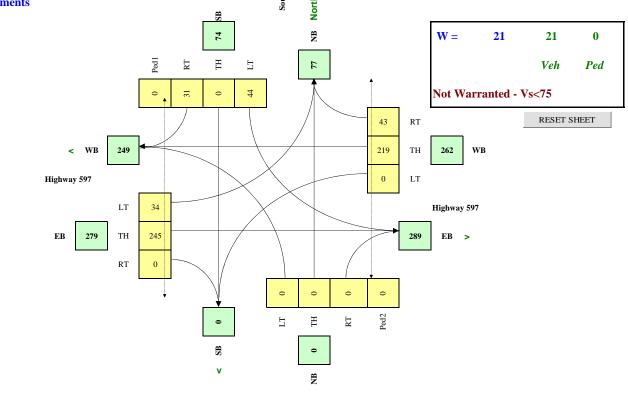




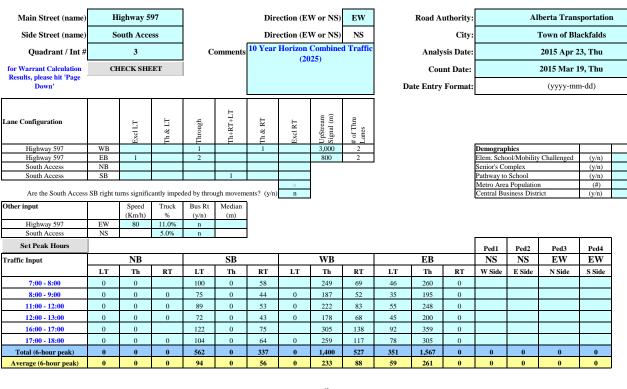






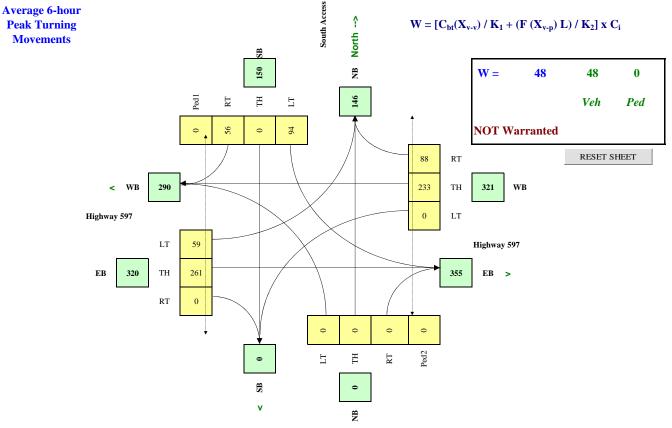




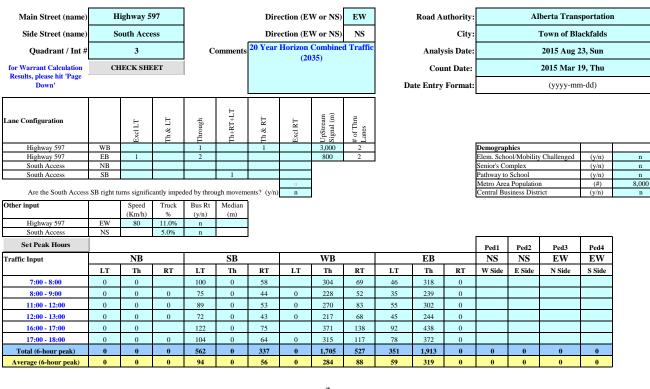


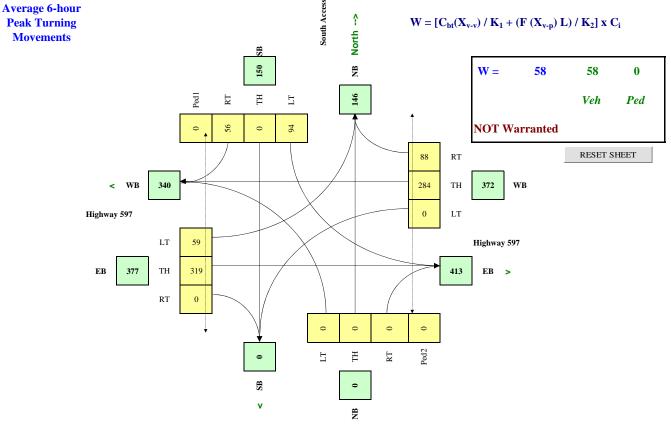
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Road Name	Highway 597 / South Access
From	То
Warrant Undertaken by	James Sun
Company Name	WSP Canada Inc.
Date	22-Jun-15

#### Warrant for Intersection Lighting (See Note 2)

1         Dominism         Implified with marking of the marking of the marking of the mark has a with a mark	Item No.	Classification Factor		Weight 'W'	Enter 'R' Here	Score 'R' x 'W'						
			0	1			4					
			1	1	Geon	letric Factors (G)	[					
			$\frown$	Right and/or Left Turn				than 70 km/h on at Least One	15			Only ONE 'R' Value is To Be
1         Impact of protection of protec	1	Channelization	None	Lanes on Minor				km/h or More on at Least One	20			Entered for These Three Rows!
1         Impact of protection of protec									5	0	0	
	2	Most Constrained Approach (Relative to Recommended Minimum Intersection Sight	100% or More	75% to 99%	50% to 74%	25% to 49%	<25%		10			
		Immediately Before Intersection on	1									
	3	110 km/hr:	Tangent	>1800 m	1150 to 1800 m	750 to 1150 m	<750 m				-	
								ł				
		70 or 80 km/h			550 to 950 m	340 to 550 m	<340 m	İ	5	1	5	
		60 km/h:	: Tangent	>575 m	320 to 575 m	190 to 320 m	<190 m					
a)       a) <td< td=""><td>4</td><td></td><td>90 Degree Angle</td><td>80 or 100 Degree Angle</td><td>-</td><td>70 or 110 Degree Angle</td><td></td><td></td><td>5</td><td>0</td><td>0</td><td></td></td<>	4		90 Degree Angle	80 or 100 Degree Angle	-	70 or 110 Degree Angle			5	0	0	
1         1 <th1< th="">         1         <th1< th=""> <th1< th=""></th1<></th1<></th1<>	5	Immdediately Before Intersection	<3.0%	Design Guidelines for Type and Speed of	Design Guidelines for Type and Speed of	Design Guidelines for Type and Speed of	Maximum Gradient for Type and Speed of		3	0	0	
	6	Number of Legs	· ·						3	1	3	
Pile Descriptions Subjected Absende un beneficient and of the BL Description and provide and the BL Description and the BL Descri						•	•		Subtotal Ge	eometric Factor	8	G
Pile Descriptions Subjected Absende un beneficient and of the BL Description and provide and the BL Description and the BL Descri					Opera	tional Eactors (O)					-	
APT 02. Weig (See Note)       APT 02. Weig (See Note) <td></td> <td></td> <td>ild be Calculated on the E</td> <td>lasis of EITHER the AADT</td> <td>Factor or the Signalization</td> <td>on Warrant Factor.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			ild be Calculated on the E	lasis of EITHER the AADT	Factor or the Signalization	on Warrant Factor.						
$ \left[ \begin{array}{c c c c c c c c c c c c c c c c c c c $												
2         3         4			i <1000	1000 to 2000	2000 to 3000	3000 to 5000	>5000		10	4	40	
i       issues do not set interaction in a function in the set interaction interactinteraction interaction inter		On Minor Road	\$ <500	500 to 1000	1000 to 1500	1500 to 2000	>2000		20	4	80	
8         Pedestram volume         No Pedestriam         Up to 10         10 to 30         30 to 50         Over 50         10         00         0           9         Intersection floadway         No Primary Read         Primary/Read Million, Primary/Secondary         Primary/Primary         Intersection floadway         5         11         5         11         5           10         Operating Speed or Posted Speed         50 km/h         70 km/h         80 km/h         50 km/h or Over         5         11         5           11         Operating Speed or Posted Speed         50 km/h         70 km/h         80 km/h         51 km/h         70         70           12         Upfort Road (See Note 3)         50 km/h         70 km/h         80 km/h         91 km/h or Over         5         0         0            50 km/h or Los         60 km/h         70 km/h         80 km/h         91 km/h or Over         5         0         0         0            5         5         10         0 km/h         70 km/h         80 km/h         91 km/h or Over         5         2         100         0         0         0         0         0         0         0         0         0	7		r Signalized and Volume- Based Signal Warrant is	Signalized and Volume- Based Warrant is 20%	Signalized and Volume- Based Warrant is 40%	Signalized and Volume- Based Warrant is Over			30			
9       Intersection Roadway Displayed or Primary Road Primary/Beam Displayed or Primary/Beam 	8	Pedestrian Volume	No Pedestrians	Up to 10	10 to 30	30 to 50	Over 50		10	0	0	
10       Limit on Major Road (See Note 3)       50 km/h or Less       60 km/h       70 km/h       80 km/h       91 km/h or Over       5       1       5         11       Operating Speed or Posted Speed Limit on Minor Road (See Note 3)       60 km/h       70 km/h       80 km/h       91 km/h or Over       5       0       0         Subtoal Operations Speed or Posted Speed Limit on Minor Road (See Note 3)       60 km/h       70 km/h       80 km/h       91 km/h or Over       5       0       0         Subtoal Operational Factors (S)         Subtoal Operational Factors (C)         Collision Factors (A)         Subtoal Environmental Factors (A)         Collision Factors (A)         Average Annual Nightime Collision Prequency (See Note 4) of Rate of Inadequate Lighting)       1 or 2 collisions per Year       15       0       0       Viria Entred Tentered Tentered Tentered Viria Collisions per Year       15       0       0       0       Viria Entred Tentered Tentered Tentered Viria Collisions per Year       15       0       0       0       Viria Entred Tentered Tentered Tentered Viria Collisions per Year       15       0       0       0       Viria Entred Tentered Tentered Tentered Viria Collision ger Year       15       0       0       0       0       0	9			Primary Rural Minor, r Primary/Designate	Primary/Secondary	Primary/Primary			5	1	5	
11       Limit on Minor Road (See Note 3)       St Min/in of Less       Bol Kin/in       Juit Kin/in of Uver       S       0       0         Subtotal Operational Factors       130       0         Subtotal Operational Factors       0       0         Subtotal Operational Factors       0       0         Subtotal Operational Factors       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0	10		50 km/h or Less	60 km/h	70 km/h	80 km/h	90 km/h or Over		5	1	5	
Environmental Factors (E)         12       Lighted Development Within 150 m       n       n One Quadrant       in Two Quadrants       in Four Quadrants       in Four Quadrants       5       2       10         Subtotal Environmental Factors (A)         Collision Factors (A)       E         Collision Factors (A)       0       0       0       0       0       Only ON         Subtotal Environmental Factors (A)       0 <td< td=""><td>11</td><td></td><td>50 km/h or Less</td><td>60 km/h</td><td>70 km/h</td><td>80 km/h</td><td>91 km/h or Over</td><td></td><td>5</td><td>0</td><td>0</td><td></td></td<>	11		50 km/h or Less	60 km/h	70 km/h	80 km/h	91 km/h or Over		5	0	0	
12       Lighted Development Within 150 m Radius of Intersection       In One Quadrant       In Three Quadrants       In Four Quadrants       In Four Quadrants       In Four Quadrants       5       2       10         Subtotal Environmental Factors       100       E         Collision Factors (A         Average Annual Nighttime Collision Frequency (See Note 4) or Rate 0       0       Collision per Year       1 or 2 Collisions per Year       15       0       0       Value 5       Collisions per Year       1       Collisions per Year       1       0       Value 5       0       Value 5       Collisions per Year       1       0       Value 5       0       Value 5       Value 5       0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Subtotal Ope</td><td>erational Factor</td><td>130</td><td>0</td></t<>									Subtotal Ope	erational Factor	130	0
12       Radius of Intersection       In One Quadratitie       In Hyde Quadratities       In Hyde Quadratit					Enviror	mental Factors (E)						
Collision Factors (A)         Average Annual Nightime Collision         13       Average Annual Nightime Collision       Collision per Year       1 or 2 Collisions per Year       15       0       Value is 1         13       Frequency (See Note 4) or Rate of Last Three Year (Only Collisions per Year       1 collision per Year       1 or 2 Collisions per Year       15       0       0       Value is 1         13       Detentially Attributable to Inadequate Lighting)       Collision per Year       1 collision per Year       1 or 2 Collisions per Year       30       0       0       0       Value is 1         Subtor A for Rate of Year and an Average Ratio of All Night-to- Day Collisions of at Least 1.5       3 or More Collisions per Year       30       30       0       0       0       Now         Subtor A Collision Per Year       1 collision of at Least 1.5       3 or More Collisions per Year       30       30       0       0       0       0       Now       Now         Subtor A Collision Per Year       1 collision Per Year       1 collision Factors (A)         Subtor A Collision Per Year       30       1       1       1       1       0       A         Subtor A Collision Per Year       1 collision Factors       0       A	12			In One Quadrant	In Two Quadrants	In Three Quadrants	In Four Quadrants					
Average Annual Nighttime Collision Frequency (See Note 4) or Rate of Last Three Yaer (Onk) Collisions per Year       1 collision per Year       1 collision per Year       1 or 2 collisions per Year       0 or 4 collision       1 or 2 collisions per Year       3 or More Collision Factors       4 or Factors       4									Subtotal Enviro	nmental Factor	s 10	E
Average Annual Nightime Collision Frequency (See Note 4) or Rate of Dependent Varies Preser       1 or 2 Collisions per Year       15       0       0       Null value is T         133       Last There Year (ON) Collisions Potentially Attributable to Inadequate Lighting)       0 Collision per Year       1 collision per Year       1 or 2 Collisions per Year       15       0       0       Value is T         133       Last There Year (ON) Collisions Potentially Attributable to Inadequate Lighting)       0 Collision per Year       1 collision per Year       3 or More Collisions per Year       4       4       6					Colli	sion Factors (A)	-					
Day Collisions of at Least 1.5     Rate 2.1.5 Collisions/MEV     30     A       Subtotal Collision Factors     0     A       G+O+E+A = Total Warranting Points     148       Warranting Condition     120	13	Frequency (See Note 4) or Rate of Last Three Year (Only Collisions Potentially Attributable to		1 Collision per Year	-	Year OR At Least 1.5 Collisions per Million Entering Vehicles per Year and an Average Ratio of All Night-to-				0	0	Only ONE 'R' Value is To Be Entered for These Two Bows!
G+O+E+A = Total Warranting Points 148 Warranting Condition 120		moocquice Lighting)								Collision Factors	s ()	
												للت
									Warr			D

Notes:

1 If the intersection is not signalized, the user should choose EITHER the AADT OR the signalization factor. The points from either factor, but not both factors, may be used for the warrant point calculations. 2 The number of certain types of vulnerable pedestrians should be factored to reflect their increased need for visibility. The number of child pedestrians (ages 12 and under) should be multiplied by two, and the number of senior pedestrians (age 65 and over) should be multiplied by 1.5. 3 85th percentile nightime speed should be used, if available. Otherwise the posted speed may be used.

4 Reported collisions, rounded to the nearest whole number.



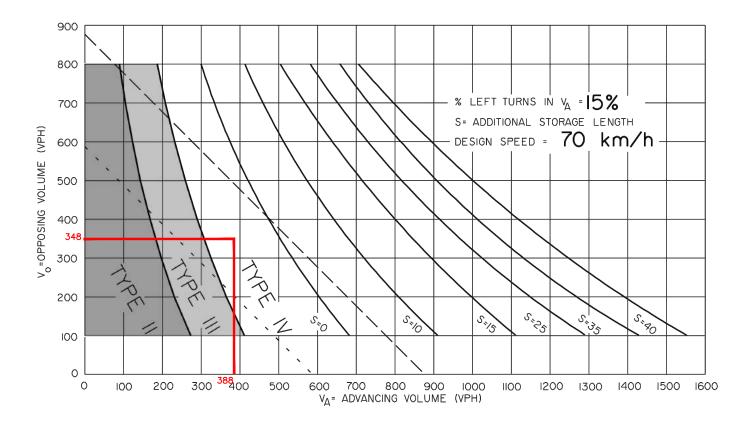
## Alberta Transportation Intersection Left Turn Lane Warrant Analysis For Two-Lane Highways

Project Number:	151-02471-00
Project Name:	Blackfalds Crossing ASP TIA
Intersection:	Highway 597 / South Accesws
Roadway:	Highway 597
Direction:	EB
Time Period:	PM Peak Hour
Scenario:	2018 Combined Traffic
Design Speed:	70 km/h

### **Traffic Information:**

a. Number of Left Turning Vehicles per Hour	Vℓ = 49 vph
b. Advancing Volume:	Va =388 vph
c. Proportion of Left Turns in Va	L = Vℓ / Va =49 / 388 =13%
d. Opposing Volume	Vo = 348 vph
	·

## ↔ A Left Turn Lane is Warranted (Type IV)





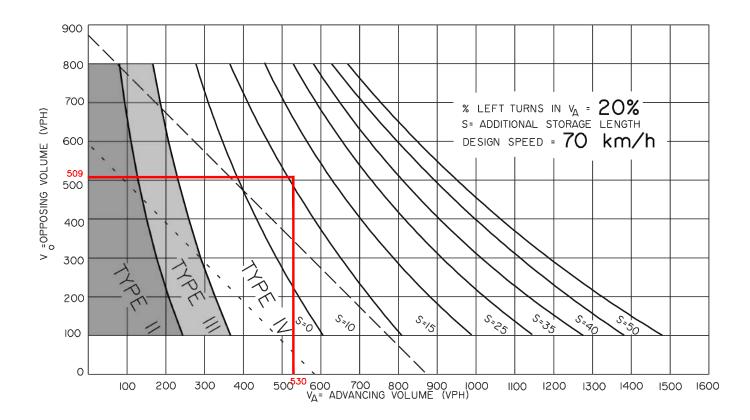
## Alberta Transportation Intersection Left Turn Lane Warrant Analysis For Two-Lane Highways

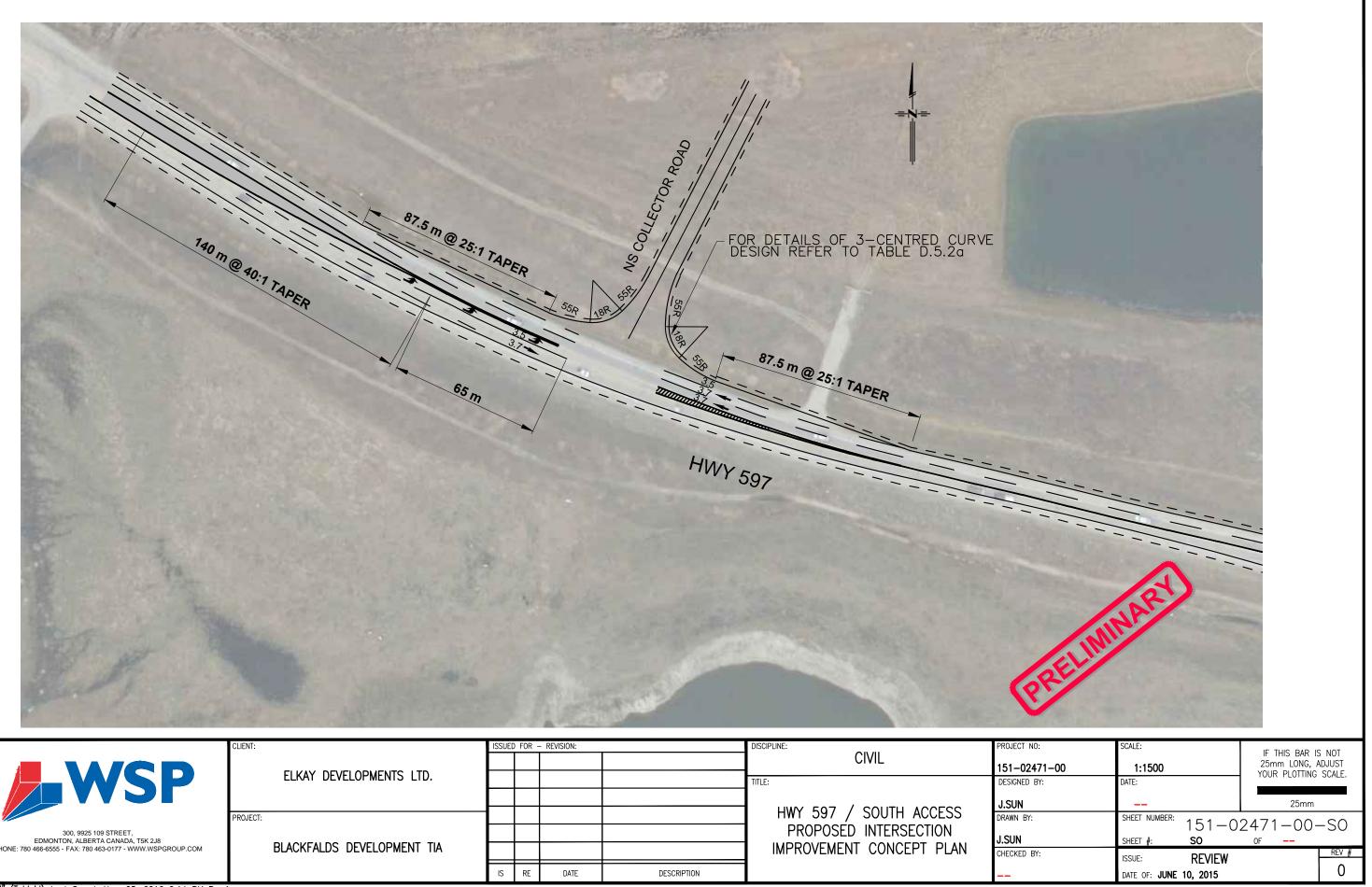
Project Number:	151-02471-00
Project Name:	Blackfalds Crossing ASP TIA
Intersection:	Highway 597 / South Accesws
Roadway:	Highway 597
Direction:	EB
Time Period:	PM Peak Hour
Scenario:	2035 Combined Traffic
Design Speed:	70 km/h

### **Traffic Information:**

a. Number of Left Turning Vehicles per Hour	Vℓ = 92 vph
b. Advancing Volume:	Va <b>=530 vph</b>
c. Proportion of Left Turns in Va	L = Vℓ / Va =92 / 530 =17%
d. Opposing Volume	Vo =509 vph

## ↔ A Left Turn Lane is Warranted (Type IV)





	CLIENT:	ISSUEE	) FOR -	REVISION:		DISCIPLINE:	PROJECT N
						CIVIL	151-02
	ELKAY DEVELOPMENTS LTD.					TITLE:	DESIGNED
							J.SUN
	PROJECT:					HWY 597 / SOUTH ACCESS	DRAWN BY:
300, 9925 109 STREET, EDMONTON, ALBERTA CANADA, T5K 2J8 IONE: 780 466-6555 - FAX: 780 463-0177 - WWW.WSPGROUP.COM						PROPOSED INTERSECTION	J.SUN
	BLACKFALDS DEVELOPMENT TIA					IMPROVEMENT CONCEPT PLAN	CHECKED E
			RE	DATE	DESCRIPTION	1	

James

Sun,

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23, 2016 2:41

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DATE OF: MAY 16, 2016

	CLIENT:		ISSUED	FOR -	- REVISION:		DISCIPLINE:	PROJECT N
						CIVIL	151-02	
	ELKAY DEVELOPMENTS LTD.						TITLE:	DESIGNED
								J.SUN
	PROJECT:						HWY 597 / SOUTH ACCESS	DRAWN BY
300, 9925 109 STREET, EDMONTON, ALBERTA CANADA, T5K 2J8	BLACKFALDS DEVELOPMENT TIA						AT REQUESTED INTERSECTION	J.SUN
PHONE: 780 466-6555 - FAX: 780 463-0177 - WWW.WSPGROUP.COM						IMPROVEMENT CONCEPT PLAN	CHECKED	
				RE	DATE	DESCRIPTION	1	

## Appendix D

## CAPACITY ANALYSIS

- Synchro Outputs
- SIDRA Outputs

4.6

#### Intersection

Int Delay, s/veh

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Vol, veh/h	2	145	37	266	1035	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	500
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	6	2	2
Mvmt Flow	2	158	40	289	1125	5

Major/Minor	Minor2		Major1		Major2		
Conflicting Flow All	1350	1125	1125	0	-	0	
Stage 1	1125	-	-	-	-	-	
Stage 2	225	-	-	-	-	-	
Critical Hdwy	6.63	6.23	4.12	-	-	-	
Critical Hdwy Stg 1	5.43	-	-	-	-	-	
Critical Hdwy Stg 2	5.83	-	-	-	-	-	
Follow-up Hdwy	3.519	3.319	2.218	-	-	-	
Pot Cap-1 Maneuver	153	249	621	-	-	-	
Stage 1	309	-	-	-	-	-	
Stage 2	792	-	-	-	-	-	
Platoon blocked, %				-	-	-	
Mov Cap-1 Maneuver	141	249	621	-	-	-	
Mov Cap-2 Maneuver	141	-	-	-	-	-	
Stage 1	309	-	-	-	-	-	
Stage 2	731	-	-	-	-	-	
Approach	EB		NB		SB		
HCM Control Delay, s	43.2		1.6		0		
HCM LOS	E						

Minor Lane/Major Mvmt	NBL	NBT EE	3Ln1	SBT	SBR	
Capacity (veh/h)	621	-	246	-	-	
HCM Lane V/C Ratio	0.065	-	0.65	-	-	
HCM Control Delay (s)	11.2	0.3	43.2	-	-	
HCM Lane LOS	В	Α	Е	-	-	
HCM 95th %tile Q(veh)	0.2	-	4	-	-	

1.9

#### Intersection

Int Delay, s/veh

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Vol, veh/h	2	55	145	806	476	1
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	500
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	3	2
Mvmt Flow	2	60	158	876	517	1

Major/Minor	Minor2		Major1		Major2		
Conflicting Flow All	1270	517	517	0	-	0	
Stage 1	517	-	-	-	-	-	
Stage 2	753	-	-	-	-	-	
Critical Hdwy	6.63	6.23	4.12	-	-	-	
Critical Hdwy Stg 1	5.43	-	-	-	-	-	
Critical Hdwy Stg 2	5.83	-	-	-	-	-	
Follow-up Hdwy	3.519	3.319	2.218	-	-	-	
Pot Cap-1 Maneuver	172	557	1049	-	-	-	
Stage 1	598	-	-	-	-	-	
Stage 2	427	-	-	-	-	-	
Platoon blocked, %				-	-	-	
Mov Cap-1 Maneuver	122	557	1049	-	-	-	
Mov Cap-2 Maneuver	122	-	-	-	-	-	
Stage 1	598	-	-	-	-	-	
Stage 2	302	-	-	-	-	-	
Approach	EB		NB		SB		
HCM Control Delay, s	13.3		2.2		0		
HCM LOS	В						

Minor Lane/Major Mvmt	NBL	NBT EBLn1	SBT	SBR	
Capacity (veh/h)	1049	- 495	-	-	
HCM Lane V/C Ratio	0.15	- 0.125	-	-	
HCM Control Delay (s)	9	1 13.3	-	-	
HCM Lane LOS	А	A B	-	-	
HCM 95th %tile Q(veh)	0.5	- 0.4	-	-	

## Lanes, Volumes, Timings 2: Highway 2A & Broadway Avenue

	٦	$\mathbf{r}$	1	1	ţ	~
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	ካካ	1	<u>102</u>	<b>1</b>	<u> </u>	
Traffic Volume (vph)	54	213	74	280	1088	105
Future Volume (vph)	54 54	213	74	280	1088	105
	1850	1850	1850	1850	1850	1850
Ideal Flow (vphpl)						
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
Storage Length (m)	50.0	0.0	60.0			60.0
Storage Lanes	2	1	1			1
Taper Length (m)	30.0		30.0			
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	1.00
Frt		0.850				0.850
Flt Protected	0.950		0.950			
Satd. Flow (prot)	3380	1559	1742	3322	3484	1525
Flt Permitted	0.950		0.129			
Satd. Flow (perm)	3380	1559	237	3322	3484	1525
Right Turn on Red	0000	Yes	201	UULL	1010	Yes
Satd. Flow (RTOR)		232				114
	50	232		60	60	114
Link Speed (k/h)	50			60	60	
Link Distance (m)	336.5			588.3	280.9	
Travel Time (s)	24.2			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	2%	2%	7%	2%	2%
Adj. Flow (vph)	59	232	80	304	1183	114
Shared Lane Traffic (%)						
Lane Group Flow (vph)	59	232	80	304	1183	114
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4		5	2	6	
Permitted Phases		4	2	-	Ū	6
Detector Phase	4	4	5	2	6	6
Switch Phase	4	4	J	2	0	0
	6.0	6.0	6.0	6.0	6.0	6.0
Minimum Initial (s)	6.0	6.0	6.0	6.0	6.0	6.0
Minimum Split (s)	24.0	24.0	12.0	24.0	24.0	24.0
Total Split (s)	24.0	24.0	12.0	41.0	29.0	29.0
Total Split (%)	36.9%	36.9%	18.5%	63.1%	44.6%	44.6%
Maximum Green (s)	18.0	18.0	6.0	35.0	23.0	23.0
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lead/Lag	0.0	0.0	Lead	0.0	Lag	Lag
Lead-Lag Optimize?			Yes		-	Yes
	0.0	0.0		0.0	Yes	
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0
Recall Mode	None	None	None	Min	Min	Min
Walk Time (s)	7.0	7.0		7.0	7.0	7.0
Flash Dont Walk (s)	11.0	11.0		11.0	11.0	11.0
Pedestrian Calls (#/hr)	0	0		0	0	0
Act Effct Green (s)	7.0	7.0	31.7	31.7	25.0	25.0
Actuated g/C Ratio	0.14	0.14	0.62	0.62	0.49	0.49
v/c Ratio	0.13	0.56	0.24	0.15	0.69	0.14
Control Delay	20.8	9.5	5.8	4.3	15.2	3.3
	20.0	9.0	<b>U.O</b>	4.3	10.Z	ა.ა

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## Lanes, Volumes, Timings 2: Highway 2A & Broadway Avenue

	≯	$\mathbf{r}$	1	Ť	ŧ	∢
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	20.8	9.5	5.8	4.3	15.2	3.3
LOS	С	А	А	А	В	А
Approach Delay	11.8			4.6	14.2	
Approach LOS	В			А	В	
Queue Length 50th (m)	2.6	0.0	2.1	4.4	47.8	0.0
Queue Length 95th (m)	6.6	14.9	6.8	10.2	#91.7	7.4
Internal Link Dist (m)	312.5			564.3	256.9	
Turn Bay Length (m)	50.0		60.0			60.0
Base Capacity (vph)	1212	707	327	2414	1710	806
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.05	0.33	0.24	0.13	0.69	0.14
Intersection Summary						
Area Type:	Other					
Cycle Length: 65						
Actuated Cycle Length: 50	.9					
Natural Cycle: 65						
Control Type: Actuated-Ur	ncoordinated					
Maximum v/c Ratio: 0.69						
Intersection Signal Delay:					tersection	
Intersection Capacity Utiliz	ation 55.9%			IC	CU Level c	of Service E
Analysis Period (min) 15						
# 95th percentile volume			eue may	be longer		
Queue shown is maxim	um after two	cycles.				

Splits and Phases: 2: Highway 2A & Broadway Avenue

1 ø2		🕹 ø4			
41 s			24 s		
<b>▲</b> ø5	Ø6				
12 s	29 s				

Intersection										
Int Delay, s/veh	1.8									
Movement	EBL	EBT			WE	ST \	WBR	SBL	SBR	
Lane Configurations	۲	<b>†</b> †			1	♠	1	Y		
Traffic Vol, veh/h	30	242			23		42	42	30	
Future Vol, veh/h	30	242			23	31	42	42	30	
Conflicting Peds, #/hr	0	0				0	0	0	0	
Sign Control	Free	Free			Fre	e	Free	Stop	Stop	
RT Channelized	-	None				- 1	None	-	None	
Storage Length	650	-				-	300	0	-	
Veh in Median Storage, #	-	0				0	-	0	-	
Grade, %	-	0				0	-	0	-	
Peak Hour Factor	92	92			ç	92	92	92	92	
Heavy Vehicles, %	5	8				8	5	5	5	
Mvmt Flow	33	263			25	51	46	46	33	
Major/Minor	Major1				Majo	r2		Minor2		
Conflicting Flow All	251	0				-	0	448	126	
Stage 1	-	-				-	-	251	_	
Stage 2	-	-				-	-	197	-	
Critical Hdwy	4.2	-				-	-	6.9	7	
Critical Hdwy Stg 1	-	-				-	-	5.9	-	
Critical Hdwy Stg 2	-	-				-	-	5.9	-	
Follow-up Hdwy	2.25	-				-	-	3.55	3.35	
Pot Cap-1 Maneuver	1290	-				-	-	532	891	
Stage 1	-	-				-	-	759	-	
Stage 2	-	-				-	-	808	-	
Platoon blocked, %		-				-	-			
Mov Cap-1 Maneuver	1290	-				-	-	518	891	
Mov Cap-2 Maneuver	-	-				-	-	518	-	
Stage 1	-	-				-	-	759	-	
Stage 2	-	-				-	-	787	-	
,										
Approach	EB				W	'B		SB		
HCM Control Delay, s	0.9					0		11.6		
HCM LOS								В		
								_		
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR SE	3Ln1					
Capacity (veh/h)	1290	-	_	-	627					
HCM Lane V/C Ratio	0.025	-	-	- 0	.125					
HCM Control Delay (s)	7.9	-	-		11.6					
HCM Lane LOS	A	-	-	-	В					
HCM 95th %tile Q(veh)	0.1	-	-	-	0.4					
	<b>.</b>									

Intersection												
Int Delay, s/veh	3.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- <del>4</del> >			- <del>4</del> >			- 42			- 🗘	
Traffic Vol, veh/h	61	5	26	1	-	1	18	12	1	1	11	165
Future Vol, veh/h	61	5	26	1	8	1	18	12	1	1	11	165
Conflicting Peds, #/hr	0	0	0	0		0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	•	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92		92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	66	5	28	1	9	1	20	13	1	1	12	179
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	162	157	102	174	246	14	191	0	0	14	0	0
Stage 1	102	104	102	53		-	-	-	-	-	-	0
Stage 2	58	53	_	121	193		_		_	_		
Critical Hdwy	7.12	6.52	6.22	7.12		6.22	4.12	_	_	4.12	_	_
Critical Hdwy Stg 1	6.12	5.52	0.22	6.12	5.52	- 0.22	-	_	-	-	_	_
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	_
Follow-up Hdwy	3.518	4.018	3.318	3.518		3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	803	735	953	789		1066	1383	-	-	1604	-	-
Stage 1	902	809	-	960		-	-	-	-	-	-	-
Stage 2	954	851	-	883		-	-	-	-	-	-	-
Platoon blocked, %		•••						-	-		-	-
Mov Cap-1 Maneuver	784	723	953	752	646	1066	1383	-	-	1604	-	-
Mov Cap-2 Maneuver	784	723	-	752		-	-	-	-	-	-	-
Stage 1	888	808	_	946	838	-	-	-	-	-	-	-
Stage 2	929	838	-	850		-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	10			10.4			4.4			0		
HCM LOS	В			В								
Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn1	SBL	SBT	SBR					
Capacity (veh/h)	1383	-	-	821 683			-					
HCM Lane V/C Ratio	0.014	_	_	0.122 0.016		_	-					
HCM Control Delay (s)	7.6	0		10 10.4		0	-					
HCM Lane LOS	A	A		B B		A	-					
HCM 95th %tile Q(veh)	0	-	_	0.4 0		-	-					
	0			0.1 0	0							

## Lanes, Volumes, Timings 8: Highway 2A & East Access

	٦	$\mathbf{i}$	•	1	ţ	~
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	<u>ነ</u> ካ	<u></u>	<u>NDL</u>		<u> </u>	<u> </u>
Traffic Volume (vph)	164	143	262	786	458	141
Future Volume (vph)	164	143	262	786	458	141
Ideal Flow (vphpl)	1850	145	1850	1850	450 1850	1850
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
. ,			60.0	J.1	3.1	
Storage Length (m)	50.0	0.0				60.0
Storage Lanes	2	1	1			1
Taper Length (m)	30.0		30.0			
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	1.00
Frt		0.850				0.850
Flt Protected	0.950		0.950			
Satd. Flow (prot)	3380	1559	1742	3484	3417	1525
Flt Permitted	0.950		0.335			
Satd. Flow (perm)	3380	1559	614	3484	3417	1525
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		155				153
Link Speed (k/h)	50	100		60	60	100
Link Distance (m)	336.5			588.3	280.9	
Travel Time (s)	24.2			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
					0.92 4%	0.92
Heavy Vehicles (%)	2%	2%	2%	2%		
Adj. Flow (vph)	178	155	285	854	498	153
Shared Lane Traffic (%)						
Lane Group Flow (vph)	178	155	285	854	498	153
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4		5	2	6	
Permitted Phases		4	2			6
Detector Phase	4	4	5	2	6	6
Switch Phase						
Minimum Initial (s)	6.0	6.0	6.0	6.0	6.0	6.0
Minimum Split (s)	24.0	24.0	12.0	24.0	24.0	24.0
Total Split (s)	24.0	24.0	12.0	36.0	24.0	24.0
Total Split (%)	40.0%	40.0%	20.0%	60.0%	40.0%	40.0%
Maximum Green (s)	18.0	18.0	7.5	30.0	18.0	
						18.0
Yellow Time (s)	4.0	4.0	3.5	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	1.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	4.5	6.0	6.0	6.0
Lead/Lag			Lead		Lag	Lag
Lead-Lag Optimize?			Yes		Yes	Yes
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0
Recall Mode	None	None	None	Min	Min	Min
Walk Time (s)	7.0	7.0		7.0	7.0	7.0
Flash Dont Walk (s)	11.0	11.0		11.0	11.0	11.0
Pedestrian Calls (#/hr)	0	0		0	0	0
Act Effct Green (s)	7.2	7.2	24.9	25.2	10.9	10.9
Actuated g/C Ratio	0.18	0.18	0.63	0.64	0.28	0.28
v/c Ratio	0.29	0.38	0.47	0.38	0.53	0.29
Control Delay	17.4	7.1	7.0	5.8	15.1	4.5

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	17.4	7.1	7.0	5.8	15.1	4.5
LOS	В	А	А	А	В	А
Approach Delay	12.6			6.1	12.6	
Approach LOS	В			А	В	
Queue Length 50th (m)	5.7	0.0	8.0	15.8	15.9	0.0
Queue Length 95th (m)	13.5	11.3	18.4	28.0	27.8	8.9
Internal Link Dist (m)	312.5			564.3	256.9	
Turn Bay Length (m)	50.0		60.0			60.0
Base Capacity (vph)	1641	836	616	2650	1660	819
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.11	0.19	0.46	0.32	0.30	0.19
Intersection Summary						
Area Type:	Other					
Cycle Length: 60						
Actuated Cycle Length: 39	9.3					
Natural Cycle: 60						
Control Type: Actuated-Ur	ncoordinated					
Maximum v/c Ratio: 0.53						
Intersection Signal Delay:					itersection	
Intersection Capacity Utiliz	zation 46.7%			IC	CU Level c	of Service A
Analysis Period (min) 15						
Splits and Phases: 8: H	ighway 2A &	East Acce	ess			



Intersection							
Int Delay, s/veh	2.2						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	٦	<b>^</b>	<u>^</u>	1	Y		
Traffic Vol, veh/h	49	339	288	60	61	42	
Future Vol, veh/h	49	339	288	60	61	42	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	650	-	-	300	0	-	
Veh in Median Storage, #	-	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	5	9	11	5	5	5	
Mvmt Flow	53	368	313	65	66	46	
Major/Minor	Major1		Major2		Minor2		
	0.4.0	<u> </u>		•	604	457	
Conflicting Flow All	313	0	-	0	604	157	
Stage 1	313	-	-	-	604 313	- 157	
•	313 -		- - -				
Stage 1 Stage 2	313 - - 4.2				313	157 - - 7	
Stage 1 Stage 2 Critical Hdwy	-	-			313 291	-	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1	-	-			313 291 6.9	- - 7	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2	- - 4.2	-	- - - - - -		313 291 6.9 5.9	- - 7	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy	- - 4.2 -		- - - - - - - -		313 291 6.9 5.9 5.9	- - 7 -	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver	- 4.2 - 2.25		- - - - - - - - - - -		313 291 6.9 5.9 5.9 3.55	- 7 - 3.35	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1	- 4.2 - 2.25		- - - - - - - - - - -		313 291 6.9 5.9 5.9 3.55 423	- 7 - 3.35	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1 Stage 2	- 4.2 - 2.25		- - - - - - - - - - - -		313 291 6.9 5.9 5.9 3.55 423 706	- 7 - 3.35	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1 Stage 2 Platoon blocked, %	- 4.2 - 2.25		- - - - - - - - - - - - - - - - - -		313 291 6.9 5.9 5.9 3.55 423 706	- 7 - 3.35	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1 Stage 2 Platoon blocked, % Mov Cap-1 Maneuver	- 4.2 - 2.25 1223 -		- - - - - - - - - - - - - - - - - - -		313 291 6.9 5.9 3.55 423 706 724 405	- 7 - 3.35 851 -	
Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1 Stage 2 Platoon blocked, % Mov Cap-1 Maneuver Mov Cap-2 Maneuver	- 4.2 - 2.25 1223 -	- - - - - - - - - - - - - - -	- - - - - - - - - - - -	· · · · · · · · · · · · · · · · · · ·	313 291 6.9 5.9 3.55 423 706 724	- 7 - 3.35 851 -	
Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Follow-up Hdwy Pot Cap-1 Maneuver Stage 1	- 4.2 - 2.25 1223 - - - 1223 -	- - - - - - - - - - - - - - -	- - - - - - - - - - - -	· · · · · · · · · · · · · · · · · ·	313 291 6.9 5.9 3.55 423 706 724 405 405	- 7 - 3.35 851 -	

Approach	EB	WB	SB	
HCM Control Delay, s	1	0	13.9	
HCM LOS			В	

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR SBLn1
Capacity (veh/h)	1223	-	-	- 515
HCM Lane V/C Ratio	0.044	-	-	- 0.217
HCM Control Delay (s)	8.1	-	-	- 13.9
HCM Lane LOS	А	-	-	- B
HCM 95th %tile Q(veh)	0.1	-	-	- 0.8

Intersection												
Int Delay, s/veh	8.7											
Movement	EBL	EBT	EBR	WB	_ WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- <b>4</b> >			- <b>4</b> >			- 44			- 44	
Traffic Vol, veh/h	212	10	46		1 4	1	43	17	1	1	18	63
Future Vol, veh/h	212	10	46		1 4	1	43	17	1	1	18	63
Conflicting Peds, #/hr	0	0	0		) 0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Sto	o Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None			None	-	-	None	-	-	None
Storage Length	-	-	-			-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-		- 0	-	-	0	-	-	0	-
Grade, %	-	0	-		- 0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	9	2 92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2		2 2	2	2	2	2	2	2	2
Mvmt Flow	230	11	50		1 4	1	47	18	1	1	20	68
Major/Minor	Minor2			Minor	1		Major1			Major2		
Conflicting Flow All	171	169	54	19	203	19	88	0	0	20	0	0
Stage 1	56	56	-	11	3 113	-	-	-	-	-	-	-
Stage 2	115	113	-	8	5 90	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.1	2 6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.1	2 5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.1		-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.51		3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	792	724	1013	76	) 693	1059	1508	-	-	1596	-	-
Stage 1	956	848	-	89	2 802	-	-	-	-	-	-	-
Stage 2	890	802	-	92	2 820	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	767	700	1013	69	670	1059	1508	-	-	1596	-	-
Mov Cap-2 Maneuver	767	700	-	69	670	-	-	-	-	-	-	-
Stage 1	925	847	-	86	3 776	-	-	-	-	-	-	-
Stage 2	856	776	-	86		-	-	-	-	-	-	-
Approach	EB			W	3		NB			SB		
HCM Control Delay, s	12.1			10.			5.3			0.1		
HCM LOS	В				3							
	_			-	-							
Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn	I SBL	SBT	SBR					
Capacity (veh/h)	1508	-	-	797 71			-					
HCM Lane V/C Ratio	0.031	-	-	0.366 0.00		-	-					
HCM Control Delay (s)	7.5	0	-	12.1 10.			-					
HCM Lane LOS	A	A	_		B A		-					
HCM 95th %tile Q(veh)	0.1	-	-		) 0		-					
	0.1		_	1.7	, 0							

## Lanes, Volumes, Timings 2: Highway 2A & Broadway Avenue

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	<u>1</u> 1	<u></u>	<u> </u>	<b>†</b>	<u>^</u>	<u> </u>
Traffic Volume (vph)	95	256	96	<b>TT</b> 324	<b>TT</b> 1267	157
Future Volume (vph)	95 95	256	96 96	324 324	1267	157
	95 1850	256 1850	96 1850	324 1850	1267	1850
Ideal Flow (vphpl)						
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
Storage Length (m)	50.0	0.0	60.0			60.0
Storage Lanes	2	1	1			1
Taper Length (m)	30.0		30.0			
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	1.00
Frt		0.850				0.850
Flt Protected	0.950		0.950			
Satd. Flow (prot)	3380	1559	1742	3322	3484	1525
Flt Permitted	0.950		0.119			'
Satd. Flow (perm)	3380	1559	218	3322	3484	1525
Right Turn on Red	0000	Yes	210	UULL	1010	Yes
		181				171
Satd. Flow (RTOR)	50	IÕI		00	00	1/1
Link Speed (k/h)	50			60	60	
Link Distance (m)	336.5			588.3	280.9	
Travel Time (s)	24.2			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	2%	2%	7%	2%	2%
Adj. Flow (vph)	103	278	104	352	1377	171
Shared Lane Traffic (%)						
Lane Group Flow (vph)	103	278	104	352	1377	171
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4		5	2	6	
Permitted Phases	т	4	2	2	Ū	6
Detector Phase	4	4	5	2	6	6
Switch Phase	4	4	5	2	0	0
	10.0	10.0	<u> </u>	45.0	45.0	45.0
Minimum Initial (s)	10.0	10.0	6.0	15.0	15.0	15.0
Minimum Split (s)	16.0	16.0	10.5	21.0	21.0	21.0
Total Split (s)	18.0	18.0	10.5	52.0	41.5	41.5
Total Split (%)	25.7%	25.7%	15.0%	74.3%	59.3%	59.3%
Maximum Green (s)	12.0	12.0	6.0	46.0	35.5	35.5
Yellow Time (s)	4.0	4.0	3.5	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	1.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	4.5	6.0	6.0	6.0
Lead/Lag	0.0	0.0	Lead	0.0		
0					Lag	Lag
Lead-Lag Optimize?	0.0	0.0	Yes	0.0	Yes	Yes
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0
Recall Mode	None	None	None	Min	Min	Min
Act Effct Green (s)	11.2	11.2	38.6	37.0	29.3	29.3
Actuated g/C Ratio	0.18	0.18	0.63	0.61	0.48	0.48
v/c Ratio	0.17	0.64	0.35	0.17	0.82	0.21
Control Delay	25.1	18.3	7.1	4.9	18.7	2.5
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	25.1	18.3	7.1	4.9	18.7	2.5
LOS	23.1 C					
103	U	В	A	A	В	A

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## Lanes, Volumes, Timings 2: Highway 2A & Broadway Avenue

	٦	$\mathbf{\hat{z}}$	•	Ť	ţ	∢				
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR				
Approach Delay	20.2			5.4	16.9					
Approach LOS	С			А	В					
Queue Length 50th (m)	5.6	10.7	3.4	7.0	67.1	0.0				
Queue Length 95th (m)	12.1	#36.5	8.0	12.2	97.5	8.0				
Internal Link Dist (m)	312.5			564.3	256.9					
Turn Bay Length (m)	50.0		60.0			60.0				
Base Capacity (vph)	700	466	296	2517	2136	1001				
Starvation Cap Reductn	0	0	0	0	0	0				
Spillback Cap Reductn	0	0	0	0	0	0				
Storage Cap Reductn	0	0	0	0	0	0				
Reduced v/c Ratio	0.15	0.60	0.35	0.14	0.64	0.17				
Intersection Summary										
Area Type:	Other									
Cycle Length: 70										
Actuated Cycle Length: 60	.8									
Natural Cycle: 60										
Control Type: Actuated-Un	coordinated									
Maximum v/c Ratio: 0.82										
Intersection Signal Delay: 7				In	tersectior	n LOS: B				
Intersection Capacity Utiliz	ation 63.5%			IC	CU Level o	of Service B				
Analysis Period (min) 15										
# 95th percentile volume			eue may	be longer						
Queue shown is maxim	um after two	cycles.								
Splits and Phases: 2: Hi	ghway 2A &	Broadway	/ Avenue							
1 m							A 04			
52 s							18 s			

1 Ø2		-\+ Ø4	
52 s		18 s	
<b>↑</b> ø5	<ul> <li>✓ Ø6</li> </ul>		
10.5 s	41.5 s		

Intersection											
Int Delay, s/veh	3.3										
Movement	EBL	EBT				WBT	WBR	S	SBL	SBR	
Lane Configurations	۲	<b>^</b>				- 11	1		Y		
Traffic Vol, veh/h	46	260				249	69		100	58	
Future Vol, veh/h	46	260				249	69		100	58	
Conflicting Peds, #/hr	0	0				0	0		0	0	
Sign Control	Free	Free				Free	Free	S	Stop	Stop	
RT Channelized	-	None				-	None		-	None	
Storage Length	650	-				-	300		0	-	
Veh in Median Storage, #	-	0				0	-		0	-	
Grade, %	-	0				0	-		0	-	
Peak Hour Factor	92	92				92	92		92	92	
Heavy Vehicles, %	5	8				8	5		5	5	
Mvmt Flow	50	283				271	75		109	63	
Major/Minor	Major1				Ν	/lajor2		Min	or2		
Conflicting Flow All	271	0				-	0		512	135	
Stage 1	-	-				-	-		271	-	
Stage 2	-	-				-	-		241	-	
Critical Hdwy	4.2	-				-	-		6.9	7	
Critical Hdwy Stg 1	-	-				-	-		5.9	-	
Critical Hdwy Stg 2	-	-				-	-		5.9	-	
Follow-up Hdwy	2.25	-				-	-	3	8.55	3.35	
Pot Cap-1 Maneuver	1268	-				-	-	4	484	880	
Stage 1	-	-				-	-	7	741	-	
Stage 2	-	-				-	-	1	768	-	
Platoon blocked, %		-				-	-				
Mov Cap-1 Maneuver	1268	-				-	-	4	465	880	
Mov Cap-2 Maneuver	-	-				-	-	4	465	-	
Stage 1	-	-				-	-	7	741	-	
Stage 2	-	-				-	-	1	738	-	
-											
Approach	EB					WB			SB		
HCM Control Delay, s	1.2					0			4.2		
HCM LOS									В		
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR S	BLn1						
Capacity (veh/h)	1268	-	-	-	562						
HCM Lane V/C Ratio	0.039	-	-	-	0.306						
HCM Control Delay (s)	8	-	-	-	14.2						
HCM Lane LOS	Â	-	-	-	В						
HCM 95th %tile Q(veh)	0.1	-			1.3						

Intersection												
Int Delay, s/veh	4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			\$	
Traffic Vol, veh/h	61	5	38	1	8	1	31	25	1	1	17	165
Future Vol, veh/h	61	5	38	1	8	1	31	25	1	1	17	165
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	66	5	41	1	9	1	34	27	1	1	18	179
	141 0											
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	210	206	108	229	295	28	198	0	0	28	0	0
Stage 1	110	110	-	95	95	-	-	-	-	-	-	-
Stage 2	100	96	-	134	200	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518		3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	747	691	946	726	616	1047	1375	-	-	1585	-	-
Stage 1	895	804	-	912	816	-	-	-	-	-	-	-
Stage 2	906	815	-	869	736	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	723	673	946	676	600	1047	1375	-	-	1585	-	-
Mov Cap-2 Maneuver	723	673	-	676	600	-	-	-	-	-	-	-
Stage 1	873	803	-	889	796	-	-	-	-	-	-	-
Stage 2	873	795	-	825	735	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
	10.3			10.8			4.2			0		
HCM Control Delay, s HCM LOS	10.3 B			10.8 B			4.2			0		
	В			В								
Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn1	SBL	SBT	SBR					
Capacity (veh/h)	1375	_	-	788 634	1585	-	-					
HCM Lane V/C Ratio	0.025	-	_	0.143 0.017		-	-					
HCM Control Delay (s)	7.7	0	-	100 100	7.3	0	-					
HCM Lang LOS	1.1	0		R R	1.5	٥ ٨						

В

0.1

А

0

А

-

В

0.5

-

HCM Lane LOS

HCM 95th %tile Q(veh)

А

0.1

А

-

## Lanes, Volumes, Timings 2: Highway 2A & East Access

	٦	$\mathbf{F}$	•	1	ţ	~
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	ካካ	1	<u>`````````````````````````````````````</u>	1	1	1
Traffic Volume (vph)	233	180	312	962	560	208
Future Volume (vph)	233	180	312	962	560	200
Ideal Flow (vphpl)	1850	1850	1850	1850	1850	1850
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
Storage Length (m)	50.0	0.0	60.0	5.7	5.7	60.0
Storage Lanes	2	0.0	1			1
Taper Length (m)	30.0	1	30.0			1
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	1.00
Frt	0.97	0.850	1.00	0.95	0.95	0.850
	0.050	0.850	0.050			0.850
Fit Protected	0.950	4550	0.950	2404	0447	4505
Satd. Flow (prot)	3380	1559	1742	3484	3417	1525
Flt Permitted	0.950	4550	0.278	0.40.4	0447	4505
Satd. Flow (perm)	3380	1559	510	3484	3417	1525
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		196				226
Link Speed (k/h)	50			60	60	
Link Distance (m)	336.5			588.3	280.9	
Travel Time (s)	24.2			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	2%	2%	2%	4%	2%
Adj. Flow (vph)	253	196	339	1046	609	226
Shared Lane Traffic (%)						
Lane Group Flow (vph)	253	196	339	1046	609	226
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4	I CIIII	рш+рі 5	2	6	CIIII
Protected Phases Permitted Phases	4	٨		2	0	e
	4	4	2	0	0	6
Detector Phase	4	4	5	2	6	6
Switch Phase		10.0		1 = 0	1	1 = 0
Minimum Initial (s)	10.0	10.0	6.0	15.0	15.0	15.0
Minimum Split (s)	16.0	16.0	10.5	21.0	21.0	21.0
Total Split (s)	17.0	17.0	20.0	43.0	23.0	23.0
Total Split (%)	28.3%	28.3%	33.3%	71.7%	38.3%	38.3%
Maximum Green (s)	11.0	11.0	15.5	37.0	17.0	17.0
Yellow Time (s)	4.0	4.0	3.5	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	1.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	4.5	6.0	6.0	6.0
Lead/Lag	0.0	0.0	Lead	0.0	Lag	Lag
Lead-Lag Optimize?			Yes		Yes	Yes
•	2.0	2.0	2.0	2.0	2.0	2.0
Vehicle Extension (s)						
Recall Mode	None	None	None	Min	Min	Min
Act Effct Green (s)	10.2	10.2	33.8	32.3	15.8	15.8
Actuated g/C Ratio	0.19	0.19	0.62	0.59	0.29	0.29
v/c Ratio	0.40	0.43	0.58	0.51	0.62	0.38
Control Delay	22.6	7.5	9.2	7.4	20.5	5.0
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	22.6	7.5	9.2	7.4	20.5	5.0
LOS	С	А	Α	А	С	А

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Approach Delay	16.0			7.9	16.3	
Approach LOS	В			А	В	
Queue Length 50th (m)	11.2	0.0	12.9	26.6	27.1	0.0
Queue Length 95th (m)	21.8	14.1	24.6	39.8	45.2	13.0
Internal Link Dist (m)	312.5			564.3	256.9	
Turn Bay Length (m)	50.0		60.0			60.0
Base Capacity (vph)	684	471	667	2372	1069	632
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.37	0.42	0.51	0.44	0.57	0.36
Intersection Summary						

Area Type:OtherCycle Length: 60Actuated Cycle Length: 54.6Natural Cycle: 55Control Type: Actuated-UncoordinatedMaximum v/c Ratio: 0.62Intersection Signal Delay: 11.9Intersection Capacity Utilization 55.7%Analysis Period (min) 15

Intersection LOS: B ICU Level of Service B

Splits and Phases: 2: Highway 2A & East Access



Intersection							
Int Delay, s/veh	4.7						
Movement	EBL	EBT	WBT		SBL	SBR	
Lane Configurations	ሻ	- 11	<u>^</u>	1	Y		
Traffic Vol, veh/h	92	359	305	138	122	75	
Future Vol, veh/h	92	359	305	138	122	75	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	600	-	-	300	0	-	
Veh in Median Storage, #	-	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	5	9	11	5	5	5	
Mvmt Flow	100	390	332	150	133	82	
Major/Minor	Major1		Major2		Minor2		
Conflicting Flow All	332	0	-	0	727	166	
Stage 1	-	-	-	-	332	-	
Stage 2	-	-	-	-	395	-	
Critical Hdwy	4.2	-	-	-	6.9	7	
Critical Hdwy Stg 1	-	-	-	-	5.9	-	
Critical Hdwy Stg 2	-	-	-	-	5.9	-	
Follow-up Hdwy	2.25	-	-	-	3.55	3.35	
Pot Cap-1 Maneuver	1203	-	-	-	353	840	
Stage 1	-	-	-	-	690	-	
Stage 2	-	-	-	-	641	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	1203	-	-	-	324	840	
Mov Cap-2 Maneuver	-	-	-	-	324	-	
Stage 1	-	-	-	-	690	-	
Stage 2	-	-	-	-	588	-	
Approach	EB		WB		SB		
HCM Control Delay, s	1.7		0		21.9		
HCM LOS					С		
M <sup>1</sup>		FDT					

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR SBLn1	
Capacity (veh/h)	1203	-	-	- 423	
HCM Lane V/C Ratio	0.083	-	-	- 0.506	
HCM Control Delay (s)	8.3	-	-	- 21.9	
HCM Lane LOS	А	-	-	- C	
HCM 95th %tile Q(veh)	0.3	-	-	- 2.8	

Intersection													
Int Delay, s/veh	9.3												
Movement	EBL	EBT	EBR	W			R	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		- <b>4</b> >				÷.			- <b>4</b> >			- <b>4</b> 2	
Traffic Vol, veh/h	212	10	69		1	4	1	65	32	1	1	37	63
Future Vol, veh/h	212	10	69		1	4	1	65	32	1	1	37	63
Conflicting Peds, #/hr	0	0	0		0		0	0	0	0	0	0	C
Sign Control	Stop	Stop	Stop	St	op Sto	op Sto	р	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None		-	- Nor	е	-	-	None	-	-	None
Storage Length	-	-	-		-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-		-	0	-	-	0	-	-	0	-
Grade, %	-	0	-		-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92				2	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2		2	2	2	2	2	2	2	2	2
Mvmt Flow	230	11	75		1	4	1	71	35	1	1	40	68
Major/Minor	Minor2			Mino	r1			Major1			Major2		
Conflicting Flow All	256	254	74	2	97 28	38 3	5	109	0	0	36	0	C
Stage 1	77	77	-	1	77 1	77	-	-	-	-	-	-	-
Stage 2	179	177	-	1	<u>2</u> 0 1 <sup>-</sup>	1	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.	12 6.	52 6.2	2	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.	12 5.5	52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.	12 5.5	52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.5	18 4.0	8 3.31	8	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	697	650	988	6	55 62		8	1481	-	-	1575	-	-
Stage 1	932	831	-		25 7		-	-	-	-	-	-	-
Stage 2	823	753	-	8	34 80	)4	-	-	-	-	-	-	-
Platoon blocked, %									-	-		-	-
Mov Cap-1 Maneuver	666	618	988	5	74 59		8	1481	-	-	1575	-	-
Mov Cap-2 Maneuver	666	618	-	5	74 59		-	-	-	-	-	-	-
Stage 1	886	830	-		35 7 <sup>-</sup>		-	-	-	-	-	-	-
Stage 2	777	716	-	8	)5 80	)3	-	-	-	-	-	-	-
Approach	EB				/B			NB			SB		
HCM Control Delay, s	13.9			10				5			0.1		
HCM LOS	В				В								
Minor Lane/Major Mvmt		NBT		EBLn1WBL	n1 SE		T SBF	2					
	NBL	IND I	INDK				I SBF	1					
Capacity (veh/h)	1481	-	-		33 15		-	-					
HCM Lane V/C Ratio	0.048	-			0.00		-	-					
HCM Long LOS	7.6	0	-	13.9 10	./ / D	.3	0	-					

HCM Lane LOS

HCM 95th %tile Q(veh)

А

0.1

А

-

В

2.2

-

В

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А

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А

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### Lanes, Volumes, Timings 2: Highway 2A & E-W Collector Road

	٦	$\mathbf{r}$	1	1	ţ	~
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	ካካ	1	<u> </u>	<b>1</b>	1001 101	 7
Traffic Volume (vph)	95	256	96	400	1562	157
Future Volume (vph)	95	250	90 96	400	1562	157
Ideal Flow (vphpl)	1850	1850	1850	1850	1850	1850
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
				3.1	3.1	
Storage Length (m)	50.0	40.0	60.0			60.0
Storage Lanes	0	1	1			1
Taper Length (m)	30.0		30.0			
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	1.00
Frt		0.850				0.850
Flt Protected	0.950		0.950			
Satd. Flow (prot)	3380	1559	1742	3322	3484	1525
Flt Permitted	0.950		0.089			
Satd. Flow (perm)	3380	1559	163	3322	3484	1525
Right Turn on Red		Yes			2.01	Yes
Satd. Flow (RTOR)		179				171
Link Speed (k/h)	50	119		60	60	1/1
,	50 64.5			588.3	280.9	
Link Distance (m)						
Travel Time (s)	4.6			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	2%	2%	7%	2%	2%
Adj. Flow (vph)	103	278	104	435	1698	171
Shared Lane Traffic (%)						
Lane Group Flow (vph)	103	278	104	435	1698	171
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4		5	2	6	
Permitted Phases		4	2			6
Detector Phase	4	4	5	2	6	6
Switch Phase	•	•	Ū	-	Ū	Ū
Minimum Initial (s)	10.0	10.0	8.0	15.0	15.0	15.0
.,	16.0	16.0	12.5	21.0	21.0	21.0
Minimum Split (s)						
Total Split (s)	16.0	16.0	12.5	64.0	51.5	51.5
Total Split (%)	20.0%	20.0%	15.6%	80.0%	64.4%	64.4%
Maximum Green (s)	10.0	10.0	8.0	58.0	45.5	45.5
Yellow Time (s)	4.0	4.0	3.5	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	1.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	4.5	6.0	6.0	6.0
Lead/Lag			Lead		Lag	Lag
Lead-Lag Optimize?			Yes		Yes	Yes
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0
Recall Mode	None	None	None	Min	Min	Min
Act Effct Green (s)	10.5	10.5	50.9	49.4	40.2	40.2
( )						
Actuated g/C Ratio	0.15	0.15	0.70	0.68	0.56	0.56
v/c Ratio	0.21	0.74	0.35	0.19	0.88	0.19
Control Delay	32.6	27.0	7.9	4.0	20.9	2.0
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	32.6	27.0	7.9	4.0	20.9	2.0
LOS	С	С	А	А	С	Α

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EBL	EBR	NBL	NBT	SBT	SBR	
28.5			4.7	19.1		
С			А	В		
7.4	14.3	3.4	8.9	105.1	0.0	
14.3	#51.2	10.7	13.0	138.3	7.4	
40.5			564.3	256.9		
50.0	40.0	60.0			60.0	
488	378	297	2620	2291	1061	
0	0	0	0	0	0	
0	0	0	0	0	0	
0	0	0	0	0	0	
0.21	0.74	0.35	0.17	0.74	0.16	
Other						
ordinated						
.6			In	itersectior	n LOS: B	
on 73.1%			IC	CU Level o	of Service D	
ceeds ca	pacity, que	eue may	be longer			
n after two	cycles.					
WOV 2A 0		otor Doo	d			
way ZA &			iu			
						<b>√</b> Ø4
	28.5 C 7.4 14.3 40.5 50.0 488 0 0 0 0.21 Other ordinated 6 on 73.1%	28.5 C 7.4 14.3 14.3 #51.2 40.5 50.0 40.0 488 378 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	28.5 C 7.4 14.3 3.4 14.3 #51.2 10.7 40.5 50.0 40.0 60.0 488 378 297 0	28.5         4.7           C         A           7.4         14.3         3.4         8.9           14.3         #51.2         10.7         13.0           40.5         564.3         50.0         40.0         60.0           488         378         297         2620         0         0         0         0           0         17          0         14         3         14         14         14         15         14         14         15         15         14         14         15         16         16         16         16 <t< td=""><td>28.5       4.7       19.1         C       A       B         7.4       14.3       3.4       8.9       105.1         14.3       #51.2       10.7       13.0       138.3         40.5       564.3       256.9         50.0       40.0       60.0         488       378       297       2620       2291         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0.21       0.74       0.35       0.17       0.74         Other         Other         Code scapacity, queue may be longer.         after two cycles.</td><td>28.5       4.7       19.1         C       A       B         7.4       14.3       3.4       8.9       105.1       0.0         14.3       #51.2       10.7       13.0       138.3       7.4         40.5       564.3       256.9       50.0       40.0       60.0       60.0         488       378       297       2620       2291       1061         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0.21       0.74       0.35       0.17       0.74       0.16</td></t<>	28.5       4.7       19.1         C       A       B         7.4       14.3       3.4       8.9       105.1         14.3       #51.2       10.7       13.0       138.3         40.5       564.3       256.9         50.0       40.0       60.0         488       378       297       2620       2291         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0       0       0       0       0         0.21       0.74       0.35       0.17       0.74         Other         Other         Code scapacity, queue may be longer.         after two cycles.	28.5       4.7       19.1         C       A       B         7.4       14.3       3.4       8.9       105.1       0.0         14.3       #51.2       10.7       13.0       138.3       7.4         40.5       564.3       256.9       50.0       40.0       60.0       60.0         488       378       297       2620       2291       1061         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0       0       0       0       0       0         0.21       0.74       0.35       0.17       0.74       0.16

1 2/2		+ <b>2</b> 4	
64 s		16 s	
▲ ø5			
12.5 s	51.5 s		

Intersection										
Int Delay, s/veh	3.2									
Movement	EBL	EBT				WBT	WBR	SBL	. SBR	
Lane Configurations	ሻ	<b>^</b>				<b>^</b>	1	Y		
Traffic Vol, veh/h	46	318				304	69	100		
Future Vol, veh/h	46	318				304	69	100		
Conflicting Peds, #/hr	0	0				0	0	C		
Sign Control	Free	Free				Free	Free	Stop		
RT Channelized	-					-	None		- None	
Storage Length	650	-				-	300	C		
Veh in Median Storage, #		0				0	-	C		
Grade, %	-	0				0	-	C		
Peak Hour Factor	92	92				92	92	92		
Heavy Vehicles, %	5	8				8	5	5		
Mvmt Flow	50	346				330	75	109		
Major/Minor	Majort				Ν	laior?		Minor		
Major/Minor	Major1	0			N	/lajor2		Minor2		
Conflicting Flow All	330	0				-	0	603		
Stage 1	-	-				-	-	330		
Stage 2	-	-				-	-	273		
Critical Hdwy	4.2	-				-	-	6.9		
Critical Hdwy Stg 1	-	-				-	-	5.9		
Critical Hdwy Stg 2	-	-				-	-	5.9		
Follow-up Hdwy	2.25	-				-	-	3.55		
Pot Cap-1 Maneuver	1205	-				-	-	424		
Stage 1	-	-				-	-	692		
Stage 2	-	-				-	-	739	-	
Platoon blocked, %		-				-	-			
Mov Cap-1 Maneuver	1205	-				-	-	406		
Mov Cap-2 Maneuver	-	-				-	-	406		
Stage 1	-	-				-	-	692		
Stage 2	-	-				-	-	708	-	
Approach	EB					WB		SB		
HCM Control Delay, s	1					0		15.9		
HCM LOS								C		
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR \$	SBLn1					
Capacity (veh/h)	1205	-	-	-	501					
HCM Lane V/C Ratio	0.041	-	-	-	0.343					
HCM Control Delay (s)	8.1	-	-	-						
HCM Lane LOS	A	-	-	-	С					
	• •									

- 1.5

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HCM 95th %tile Q(veh)

0.1

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Intersection												
Int Delay, s/veh	4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		- 4			- 4			- 43			- 44	
Traffic Vol, veh/h	61	5	38	1	8	1	31	25	1	1	17	165
Future Vol, veh/h	61	5	38	1	8	1	31	25	1	1	17	165
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	66	5	41	1	9	1	34	27	1	1	18	179
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	210	206	108	229	295	28	198	0	0	28	0	0
Stage 1	110	110	-	95	95	-	-	-	-	-	-	-
Stage 2	100	96	-	134	200	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	747	691	946	726	616	1047	1375	-	-	1585	-	-
Stage 1	895	804	-	912	816	-	-	-	-	-	-	-
Stage 2	906	815	-	869	736	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	723	673	946	676	600	1047	1375	-	-	1585	-	-
Mov Cap-2 Maneuver	723	673	-	676	600	-	-	-	-	-	-	-
Stage 1	873	803	-	889	796	-	-	-	-	-	-	-
Stage 2	873	795	-	825	735	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	10.3			10.8			4.2			0		
HCM LOS	В			В								
		NDT	NDD		0.51	057	000					
Minor Lane/Major Mvmt	NBL	NBT		EBLn1WBLn1	SBL	SBT	SBR					
Capacity (veh/h)	1375	-	-	788 634	1585	-	-					
HCM Lane V/C Ratio	0.025	-	-	0.143 0.017		-	-					
HCM Control Delay (s)	7.7	0	-	10.3 10.8	7.3	0	-					
HCM Lane LOS	A	A	-	B B	A	A	-					
HCM 95th %tile Q(veh)	0.1	-	-	0.5 0.1	0	-	-					

### Lanes, Volumes, Timings 2: Highway 2A & E-W Collector Road

	۶	$\mathbf{i}$	1	1	ţ	~
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	ሻሻ	1	<u>102</u>	<b>1</b>	1001 101	
Traffic Volume (vph)	233	180	312	1201	693	208
Future Volume (vph)	233	180	312	1201	693	200
Ideal Flow (vphpl)	1850	1850	1850	1850	1850	1850
Lane Width (m)	3.7	3.7	3.7	3.7	3.7	3.5
Storage Length (m)	50.0	30.0	60.0	5.7	5.7	60.0
Storage Lanes	0	30.0	1			00.0
		I	•			I
Taper Length (m)	30.0 0.97	1.00	30.0 1.00	0.95	0.05	1.00
Lane Util. Factor	0.97	1.00	1.00	0.95	0.95	
Frt Flt Droto stad	0.050	0.850	0.050			0.850
Fit Protected	0.950	4550	0.950	2404	2447	1505
Satd. Flow (prot)	3380	1559	1742	3484	3417	1525
Flt Permitted	0.950	4==0	0.213	0.40.4	0.1.1-	4505
Satd. Flow (perm)	3380	1559	391	3484	3417	1525
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		196				226
Link Speed (k/h)	50			60	60	
Link Distance (m)	71.0			588.3	280.9	
Travel Time (s)	5.1			35.3	16.9	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	2%	2%	2%	4%	2%
Adj. Flow (vph)	253	196	339	1305	753	226
Shared Lane Traffic (%)	200		000	1000		220
Lane Group Flow (vph)	253	196	339	1305	753	226
Turn Type	Prot	Perm	pm+pt	NA	NA	Perm
Protected Phases	4	Fenn		2	6	renn
	4	1	5	2	0	6
Permitted Phases	4	4	2	0	<u> </u>	6
Detector Phase	4	4	5	2	6	6
Switch Phase		10.0				
Minimum Initial (s)	10.0	10.0	8.0	15.0	15.0	15.0
Minimum Split (s)	16.0	16.0	12.5	21.0	21.0	21.0
Total Split (s)	16.0	16.0	18.0	44.0	26.0	26.0
Total Split (%)	26.7%	26.7%	30.0%	73.3%	43.3%	43.3%
Maximum Green (s)	10.0	10.0	13.5	38.0	20.0	20.0
Yellow Time (s)	4.0	4.0	3.5	4.0	4.0	4.0
All-Red Time (s)	2.0	2.0	1.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.0	6.0	4.5	6.0	6.0	6.0
Lead/Lag	0.0	0.0	Lead	0.0	Lag	Lag
Lead-Lag Optimize?			Yes		Yes	Yes
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0
( )						
Recall Mode	None	None	None	Min	Min	Min
Act Effct Green (s)	10.1	10.1	34.6	33.1	17.4	17.4
Actuated g/C Ratio	0.18	0.18	0.63	0.60	0.32	0.32
v/c Ratio	0.41	0.44	0.66	0.63	0.70	0.36
Control Delay	23.4	7.8	12.8	8.5	20.9	4.3
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	23.4	7.8	12.8	8.5	20.9	4.3
LOS	С	А	В	А	С	А

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Approach Delay	16.6			9.4	17.1	
Approach LOS	В			А	В	
Queue Length 50th (m)	11.7	0.0	12.9	37.2	34.5	0.0
Queue Length 95th (m)	22.3	14.4	32.4	52.1	52.8	12.0
Internal Link Dist (m)	47.0			564.3	256.9	
Turn Bay Length (m)	50.0	30.0	60.0			60.0
Base Capacity (vph)	616	444	577	2412	1245	699
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.41	0.44	0.59	0.54	0.60	0.32
Intersection Summary						
Area Type:	Other					
Cycle Length: 60						
Actuated Cycle Length: 55	5.2					
Natural Cycle: 60						

Natural Cycle: 60 Control Type: Actuated-Uncoordinated Maximum v/c Ratio: 0.70 Intersection Signal Delay: 12.9 Intersection Capacity Utilization 59.5% Analysis Period (min) 15

Intersection LOS: B ICU Level of Service B

Splits and Phases: 2: Highway 2A & E-W Collector Road



Intersection							
Int Delay, s/veh	5.1						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	ሻ	<b>††</b>	<b>^</b>	1	Υ		
Traffic Vol, veh/h	92	438	371	138	122	75	
Future Vol, veh/h	92	438	371	138	122	75	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	650	-	-	300	0	-	
Veh in Median Storage, #	£ _	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	5	9	11	5	5	5	
Mvmt Flow	100	476	403	150	133	82	
Major/Minor	Major1		Major2		Minor2		
Conflicting Flow All	403	0	-	0	841	202	
Stage 1	-	-	-	-	403	-	
Stage 2	-	-	-	-	438	-	
Critical Hdwy	4.2	-	-	-	6.9	7	
Critical Hdwy Stg 1	-	-	-	-	5.9	-	
Critical Hdwy Stg 2	-	-	-	-	5.9	-	
Follow-up Hdwy	2.25	-	-	-	3.55	3.35	
Pot Cap-1 Maneuver	1131	-	-	-	298	796	
Stage 1	-	-	-	-	635	-	
Stage 2	-	-	-	-	609	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	1131	-	-	-	272	796	
Mov Cap-2 Maneuver	-	-	-	-	272	-	

Approach	EB	WB	SB	
HCM Control Delay, s	1.5	0	28.2	
HCM LOS			D	

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635

555

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Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)	1131	-	-	-	363
HCM Lane V/C Ratio	0.088	-	-	-	0.59
HCM Control Delay (s)	8.5	-	-	-	28.2
HCM Lane LOS	А	-	-	-	D
HCM 95th %tile Q(veh)	0.3	-	-	-	3.6

Stage 1

Stage 2

-

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Intersection												
Int Delay, s/veh	9.3											
Movement	EBL	EBT	EBR	WBI	_ WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		÷			<b>.</b>			4			\$	
Traffic Vol, veh/h	212	10	69		4	1	65	32	1	1	37	63
Future Vol, veh/h	212	10	69		4	1	65	32	1	1	37	63
Conflicting Peds, #/hr	0	0	0	(	) 0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Sto	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None			None	-	-	None	-	-	None
Storage Length	-	-	-			-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-		- 0	-	-	0	-	-	0	-
Grade, %	-	0	-		- 0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	2 92	92	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2		2 2	2	2	2	2	2	2	2
Mvmt Flow	230	11	75		4	1	71	35	1	1	40	68
Major/Minor	Minor2			Minor			Major1			Major2		
Conflicting Flow All	256	254	74	29		35	109	0	0	36	0	0
Stage 1	77	77	-	17		-	-	-	-	-	-	-
Stage 2	179	177	-	120	) 111	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	2 6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	2 5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	2 5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	8 4.018	3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	697	650	988	65	5 622	1038	1481	-	-	1575	-	-
Stage 1	932	831	-	82	5 753	-	-	-	-	-	-	-
Stage 2	823	753	-	884	804	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	666	618	988	574	591	1038	1481	-	-	1575	-	-
Mov Cap-2 Maneuver	666	618	-	574	591	-	-	-	-	-	-	-
Stage 1	886	830	-	78	5 716	-	-	-	-	-	-	-
Stage 2	777	716	-	80	5 803	-	-	-	-	-	-	-
Approach	EB			WE			NB			SB		
HCM Control Delay, s	13.9			10.1	7		5			0.1		
HCM LOS	В			E	3							
Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn <sup>·</sup>	I SBL	SBT	SBR					
Capacity (veh/h)	1481	-	-	720 633	3 1575	-	-					
HCM Lane V/C Ratio	0.048	-	-		0.001	-	-					
HCM Control Delay (s)	7.6	0	-	13.9 10.1		0	-					
HCM Lane LOS	A		-	BE		-	-					
	0.4											

2.2

0

0

0.1

HCM 95th %tile Q(veh)

# Site: Highway 2A / 597 (2018 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use an	nd Perf <u>o</u> r	mance	•										
	Demand		Can	Deg.	Lane	Average	Level of	95% Back of		Lane	Lane	Cap.	Prob.
	Total veh/h	HV %	Cap. veh/h	Satn v/c	Util. %	Delay sec	Service	Veh	Dist m	Config	Length m	Adj. %	Block. %
South: NB Hig		/0	VCII/II	V/C	/0	360			111		111	/0	/0
Lane 1 (LT)	230	14.2	1091	0.211	100	5.2	LOS A	1.1	8.7	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	266	9.0	1260	0.211	100	4.7	LOS A	1.1	8.6	Full	500	0.0	0.0
Approach	496	11.4		0.211		4.9	LOS A	1.1	8.7				
East: WB High	nway 597												
Lane 1 (LT)	138	6.6	981	0.141	100	5.0	LOS A	0.6	4.6	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	164	2.0	1164	0.141	100	4.3	LOS A	0.6	4.6	Full	500	0.0	0.0
Approach	302	4.1		0.141		4.6	LOS A	0.6	4.6				
North: SB Hig	hway 2A												
Lane 1 (LT)	677	2.0	1097	0.617	100	11.5	LOS B	4.9	35.2	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	770	2.8	1248	0.617	100	10.5	LOS B	4.9	35.3	Full	500	0.0	0.0
Approach	1447	2.4		0.617		11.0	LOS B	4.9	35.3				
West: EB High	1way 597												
Lane 1 (LT)	110	6.1	469	0.234	73 <sup>5</sup>	11.2	LOS B	1.1	8.1	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	208	10.0	647	0.321	100	9.8	LOS A	1.7	13.2	Full	500	0.0	0.0
Approach	318	8.7		0.321		10.3	LOS B	1.7	13.2				
Intersection	2562	5.1		0.617		9.0	LOS A	4.9	35.3				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

5 Lane under-utilisation found by the program

d Dominant lane on roundabout approach

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### W Site: Highway 2A / 597 (2018 Combined Traffic PM Peak)

EF: 1.1 Roundabout

Lane Use ar	nd Perfor	mance	<b>)</b>										
	Demand Total veh/h	Flows HV %	Cap. veh/h	Deg. Satn v/c	Lane Util. %	Average Delay sec	Level of Service	95% Back of Veh	Queue Dist m	Lane Config	Lane Length m	Cap. Adj. %	Prob. Block. %
South: NB Hig	ghway 2A												
Lane 1 (LT)	486	4.1	989	0.492	100	9.6	LOS A	3.1	22.5	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	568	3.3	1156	0.492	100	8.5	LOS A	3.1	22.6	Full	500	0.0	0.0
Approach	1054	3.7		0.492		9.0	LOS A	3.1	22.6				
East: WB Hig	hway 597												
Lane 1 (LT)	148	10.8	564	0.262	100	9.9	LOS A	1.2	9.4	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	199	8.4	759	0.262	100	7.7	LOS A	1.3	10.1	Full	500	0.0	0.0
Approach	347	9.4		0.262		8.7	LOS A	1.3	10.1				
North: SB Hig	hway 2A												
Lane 1 (LT)	323	2.8	1030	0.313	100	6.6	LOS A	1.7	12.0	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	361	4.9	1152	0.313	100	6.1	LOS A	1.7	12.5	Full	500	0.0	0.0
Approach	684	3.9		0.313		6.4	LOS A	1.7	12.5				
West: EB Hig	hway 597												
Lane 1 (LT)	207	5.7	838	0.247	100	6.9	LOS A	1.2	8.7	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	232	14.6	938	0.247	100	6.3	LOS A	1.2	9.6	Full	500	0.0	0.0
Approach	439	10.4		0.247		6.6	LOS A	1.2	9.6				
Intersection	2524	5.7		0.492		7.8	LOS A	3.1	22.6				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / 597 (2025 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use ar	nd Perfor	mance	9										
	Demand Total veh/h	Flows HV %	Cap. veh/h	Deg. Satn v/c	Lane Util. %	Average Delay sec	Level of Service	95% Back of Veh	Queue Dist m	Lane Config	Lane Length m	Cap. Adj. %	Prob. Block. %
South: NB Hig		70	VCII/II	V/C	/0	360						/0	/0
Lane 1 (LT)	266	14.3	1057	0.252	100	5.8	LOS A	1.4	10.8	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	310	9.0	1230	0.252	100	5.2	LOS A	1.4	10.7	Full	500	0.0	0.0
Approach	576	11.4		0.252		5.5	LOS A	1.4	10.8				
East: WB Hig	hway 597												
Lane 1 (LT)	155	6.7	932	0.166	100	5.5	LOS A	0.8	5.6	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	186	2.0	1121	0.166	100	4.7	LOS A	0.8	5.6	Full	500	0.0	0.0
Approach	341	4.1		0.166		5.0	LOS A	0.8	5.6				
North: SB Hig	hway 2A												
Lane 1 (LT)	771	2.0	1061	0.727	100	15.5	LOS C	7.5	53.6	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	884	2.7	1216	0.727	100	14.0	LOS B	7.6	54.4	Full	500	0.0	0.0
Approach	1655	2.4		0.727		14.7	LOS B	7.6	54.4				
West: EB Hig	hway 597												
Lane 1 (LT)	126	6.3	385	0.327	66 <sup>5</sup>	15.5	LOS C	1.7	12.2	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	268	10.0	544	0.493	100	15.3	LOS C	3.2	24.3	Full	500	0.0	0.0
Approach	395	8.8		0.493		15.4	LOS C	3.2	24.3				
Intersection	2967	5.2		0.727		11.9	LOS B	7.6	54.4				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

5 Lane under-utilisation found by the program

d Dominant lane on roundabout approach

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### W Site: Highway 2A / 597 (2025 Combined Traffic PM Peak)

EF: 1.1 Roundabout

Lane Use an	d Perfor	mance	)										
	Demand Total veh/h	Flows HV %	Cap. veh/h	Deg. Satn v/c	Lane Util. %	Average Delay sec	Level of Service	95% Back of Veh	<sup>:</sup> Queue Dist m	Lane Config	Lane Length m	Cap. Adj. %	Prob. Block. %
South: NB High		/0			,,,							,,,	
Lane 1 (LT)	609	4.5	942	0.647	100	13.8	LOS B	5.5	39.9	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	724	3.2	1119	0.647	100	12.1	LOS B	5.6	40.6	Full	500	0.0	0.0
Approach	1333	3.8		0.647		12.9	LOS B	5.6	40.6				
East: WB High	way 597												
Lane 1 (LT)	169	10.7	440	0.384	100	15.1	LOS C	2.0	15.3	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	239	8.5	623	0.384	100	11.2	LOS B	2.3	16.9	Full	500	0.0	0.0
Approach	408	9.4		0.384		12.8	LOS B	2.3	16.9				
North: SB High	way 2A												
Lane 1 (LT)	376	2.8	948	0.396	100	8.3	LOS A	2.2	16.0	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	429	4.8	1082	0.396	100	7.5	LOS A	2.3	16.8	Full	500	0.0	0.0
Approach	804	3.9		0.396		7.8	LOS A	2.3	16.8				
West: EB High	way 597												
Lane 1 (LT)	248	5.6	761	0.326	100	8.6	LOS A	1.6	12.1	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	275	18.6	843	0.326	100	7.9	LOS A	1.7	13.8	Full	500	0.0	0.0
Approach	523	12.5		0.326		8.3	LOS A	1.7	13.8				
Intersection	3067	6.0		0.647		10.8	LOS B	5.6	40.6				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / 597 (2035 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use ar	nd Perfor	mance	e										
	Demand Total veh/h	Flows HV %	Cap. veh/h	Deg. Satn v/c	Lane Util. %	Average Delay sec	Level of Service	95% Back o Veh	f Queue Dist m	Lane Config	Lane Length m	Cap. Adj. %	Prob. Block. %
South: NB Hig		70	VCH/H	10	70	000						70	, ,,
Lane 1 (LT)	313	14.1	1015	0.309	100	6.7	LOS A	1.8	14.1	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	367	9.0	1189	0.309	100	5.9	LOS A	1.9	14.1	Full	500	0.0	0.0
Approach	680	11.4		0.309		6.3	LOS A	1.9	14.1				
East: WB Hig	hway 597												
Lane 1 (LT)	183	6.8	871	0.210	100	6.3	LOS A	1.0	7.3	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	224	2.0	1067	0.210	100	5.3	LOS A	1.0	7.3	Full	500	0.0	0.0
Approach	407	4.2		0.210		5.7	LOS A	1.0	7.3				
North: SB Hig	hway 2A												
Lane 1 (LT)	891	2.0	1007	0.885	100	27.8	LOS D	14.4	102.8	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	1032	2.7	1167	0.885	100	25.1	LOS D	14.8	106.0	Full	500	0.0	0.0
Approach	1923	2.4		0.885		26.4	LOS D	14.8	106.0				
West: EB Higl	hway 597												
Lane 1 (LT)	145	6.3	281	0.516	69 <sup>5</sup>	28.3	LOS D	3.0	22.1	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	302	10.0	404	0.747	100	34.7	LOS D	6.2	46.9	Full	500	0.0	0.0
Approach	447	8.8		0.747		32.6	LOS D	6.2	46.9				
Intersection	3457	5.2		0.885		20.8	LOS C	14.8	106.0				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

5 Lane under-utilisation found by the program

d Dominant lane on roundabout approach

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### W Site: Highway 2A / 597 (2035 Combined Traffic PM Peak)

EF: 1.1 Roundabout

Lane Use an	nd Perfor	mance	e										
	Demand Total veh/h	Flows HV %	Cap. veh/h	Deg. Satn v/c	Lane Util. %	Average Delay sec	Level of Service	95% Back of Veh	f Queue Dist m	Lane Config	Lane Length m	Cap. Adj. %	Prob. Block. %
South: NB Hig	hway 2A												
Lane 1 (LT)	713	4.4	875	0.815	100	23.5	LOS C	9.7	70.2	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	860	3.2	1055	0.815	100	20.5	LOS C	10.1	72.9	Full	500	0.0	0.0
Approach	1573	3.7		0.815		21.8	LOS C	10.1	72.9				
East: WB High	nway 597												
Lane 1 (LT)	195	10.5	334	0.584	100	27.8	LOS D	3.5	26.8	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	288	8.7	493	0.584	100	20.0	LOS C	4.1	31.2	Full	500	0.0	0.0
Approach	483	9.4		0.584		23.1	LOS C	4.1	31.2				
North: SB Hig	hway 2A												
Lane 1 (LT)	440	2.8	885	0.497	100	10.5	LOS B	3.3	23.6	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	509	4.8	1025	0.497	100	9.4	LOS A	3.4	24.6	Full	500	0.0	0.0
Approach	949	3.9		0.497		9.9	LOS A	3.4	24.6				
West: EB High	nway 597												
Lane 1 (LT)	284	5.7	669	0.425	100	11.4	LOS B	2.4	17.9	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	326	17.5	768	0.425	100	10.2	LOS B	2.5	20.4	Full	500	0.0	0.0
Approach	610	12.0		0.425		10.8	LOS B	2.5	20.4				
Intersection	3614	5.9		0.815		17.0	LOS C	10.1	72.9				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / East Access (2018 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use an	d Perfor	mance	e										
	Demand I		Con	Deg.	Lane	Average	Level of	95% Back o		Lane	Lane	Cap.	Prob.
	Total veh/h	HV %	Cap. veh/h	Satn v/c	Util. %	Delay	Service	Veh	Dist	Config	Length	Adj. %	Block. %
South: NB Hig	-	70	ven/n	V/C	70	sec			m	_	m	70	70
Lane 1 (LT)	188	4.8	1339	0.141	100	3.8	LOS A	0.8	5.6	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	205	7.0	1456	0.141	100	3.6	LOS A	0.8	5.8	Full	500	0.0	0.0
Approach	393	6.0		0.141		3.7	LOS A	0.8	5.8				
North: SB High	nway 2A												
Lane 1 (T)	623	2.0	1364	0.457	100	7.1	LOS A	3.1	22.1	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	702	2.0	1538	0.457	100	6.6	LOS A	3.1	22.2	Full	500	0.0	0.0
Approach	1326	2.0		0.457		6.8	LOS A	3.1	22.2				
West: EB East	Access												
Lane 1 (L)	60	2.0	551	0.109	100	7.9	LOS A	0.4	3.1	Full	50	0.0	0.0
Lane 2 (R) <sup>d</sup>	237	2.0	881	0.269	100	6.9	LOS A	1.3	9.0	Full	50	0.0	0.0
Approach	297	2.0		0.269		7.1	LOS A	1.3	9.0				
Intersection	2016	2.8		0.457		6.3	LOS A	3.1	22.2				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / East Access (2018 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use an	d Dorfor												
			;									-	
	Demand I		Cap.	Deg.	Lane	Average	Level of	95% Back of		Lane	Lane	Cap.	Prob.
	Total veh/h	HV %	veh/h	Satn v/c	Util.	Delay	Service	Veh	Dist	Config	Length	Adj.	Block.
South: NB Hig		70	ven/n	V/C	%	sec	_		m	_	m	%	%
Lane 1 (LT)	552	3.4	1208	0.457	100	7.7	LOS A	3.2	23.2	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	613	5.0	1341	0.457	100	7.2	LOS A	3.3	24.0	Full	500	0.0	0.0
Approach	1164	4.3		0.457		7.5	LOS A	3.3	24.0				
North: SB High	nway 2A												
Lane 1 (T)	315	2.0	1092	0.288	100	6.1	LOS A	1.7	11.9	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	351	2.0	1216	0.288	100	5.6	LOS A	1.7	12.2	Full	500	0.0	0.0
Approach	666	2.0		0.288		5.8	LOS A	1.7	12.2				
West: EB East	Access												
Lane 1 (L) <sup>d</sup>	182	2.0	1100	0.166	100	4.7	LOS A	0.8	5.6	Full	50	0.0	0.0
Lane 2 (R)	159	2.0	951	0.167	100	5.4	LOS A	0.8	5.5	Full	50	0.0	0.0
Approach	341	2.0		0.167		5.0	LOS A	0.8	5.6				
Intersection	2171	3.2		0.457		6.6	LOS A	3.3	24.0				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / East Access (2025 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use an	d Perfor	mance	<b>;</b>										
	Demand I		0	Deg.	Lane	Average	Level of	95% Back of		Lane	Lane	Cap.	Prob.
	Total	HV	Cap.	Satn	Util.	Delay	Service	Veh	Dist	Config	Length	Adj.	Block.
South: NB Hig	veh/h hway 2A	%	veh/h	v/c	%	sec	_	_	m	_	m	%	%
Lane 1 (LT)	224	4.6	1270	0.176	100	4.3	LOS A	1.0	7.2	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	243	7.0	1376	0.176	100	4.1	LOS A	1.0	7.5	Full	500	0.0	0.0
Approach	467	5.9		0.176		4.2	LOS A	1.0	7.5				
North: SB High	nway 2A												
Lane 1 (T)	743	2.0	1329	0.559	100	8.9	LOS A	4.5	31.8	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	839	2.0	1502	0.559	100	8.2	LOS A	4.5	32.1	Full	500	0.0	0.0
Approach	1582	2.0		0.559		8.5	LOS A	4.5	32.1				
West: EB East	Access												
Lane 1 (L)	106	2.0	534	0.198	100	9.4	LOS A	0.9	6.1	Full	50	0.0	0.0
Lane 2 (R) <sup>d</sup>	284	2.0	782	0.364	100	9.0	LOS A	2.0	13.9	Full	50	0.0	0.0
Approach	390	2.0		0.364		9.1	LOS A	2.0	13.9				
Intersection	2439	2.7		0.559		7.8	LOS A	4.5	32.1				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# Site: Highway 2A / East Access (2025 Combined Traffic PM Peak)

EF: 1.1 Roundabout

Lane Use an	d Perfor	mance	2										
	Demand I			Deg.	Lane	Average	Level of	95% Back o	f Queue	Lane	Lane	Cap.	Prob.
	Total	ΗV	Cap.	Satn	Util.	Delay	Service	Veh	Dist	Config	Length	Adj.	Block.
	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: NB Hig	hway 2A												
Lane 1 (LT)	668	3.4	1119	0.597	100	10.9	LOS B	5.0	36.1	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	748	5.0	1252	0.597	100	10.0	LOS B	5.0	36.8	Full	500	0.0	0.0
Approach	1416	4.3		0.597		10.4	LOS B	5.0	36.8				
North: SB High	nway 2A												
Lane 1 (T)	401	2.0	1023	0.392	100	7.7	LOS A	2.6	18.3	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	452	2.0	1152	0.392	100	7.1	LOS A	2.7	19.0	Full	500	0.0	0.0
Approach	853	2.0		0.392		7.4	LOS A	2.7	19.0				
West: EB East	Access												
Lane 1 (L) <sup>d</sup>	259	2.0	1021	0.253	100	6.0	LOS A	1.3	9.3	Full	50	0.0	0.0
Lane 2 (R)	200	2.0	851	0.235	100	6.7	LOS A	1.1	8.1	Full	50	0.0	0.0
Approach	459	2.0		0.253		6.3	LOS A	1.3	9.3				
Intersection	2728	3.2		0.597		8.8	LOS A	5.0	36.8				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / East Access (2035 Combined Traffic AM Peak)

EF: 1.1 Roundabout

Lane Use an	d Perfori	mance	•										
	Demand I		0	Deg.	Lane	Average	Level of	95% Back o		Lane	Lane	Cap.	Prob.
	Total	HV	Cap.	Satn	Util.	Delay	Service	Veh	Dist	Config	Length	Adj.	Block.
South: NB Hig	veh/h	%	veh/h	v/c	%	sec		_	m		m	%	%
0	•												
Lane 1 (LT)	264	5.0	1268	0.208	100	4.6	LOS A	1.2	9.0	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	287	7.0	1382	0.208	100	4.3	LOS A	1.3	9.3	Full	500	0.0	0.0
Approach	551	6.0		0.208		4.5	LOS A	1.3	9.3				
North: SB High	hway 2A												
Lane 1 (T)	895	2.0	1333	0.671	100	11.4	LOS B	6.6	46.8	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	1015	2.0	1513	0.671	100	10.4	LOS B	6.6	47.0	Full	500	0.0	0.0
Approach	1910	2.0		0.671		10.9	LOS B	6.6	47.0				
West: EB East	t Access												
Lane 1 (L)	106	2.0	455	0.232	100	11.4	LOS B	1.1	7.6	Full	50	0.0	0.0
Lane 2 (R) <sup>d</sup>	284	2.0	664	0.428	100	11.6	LOS B	2.6	18.3	Full	50	0.0	0.0
Approach	390	2.0		0.428		11.5	LOS B	2.6	18.3				
Intersection	2851	2.8		0.671		9.7	LOS A	6.6	47.0				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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# V Site: Highway 2A / East Access (2035 Combined Traffic PM Peak)

EF: 1.1 Roundabout

Lane Use ar	nd Perfori	mance	<b>;</b>										
	Demand I Total	HV	Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back o Veh	Dist	Lane Config	Lane Length	Cap. Adj.	Prob. Block.
South: NB Hig	veh/h ghway 2A	%	veh/h	v/c	%	sec	_	_	m	_	m	%	%
Lane 1 (LT)	791	3.7	1115	0.709	100	14.2	LOS B	8.0	57.8	Full	500	0.0	0.0
Lane 2 (T) <sup>d</sup>	890	5.0	1255	0.709	100	13.1	LOS B	8.0	58.3	Full	500	0.0	0.0
Approach	1681	4.4		0.709		13.6	LOS B	8.0	58.3				
North: SB Hig	hway 2A												
Lane 1 (T)	470	2.0	1014	0.463	100	8.9	LOS A	3.3	23.5	Full	500	0.0	0.0
Lane 2 (TR) <sup>d</sup>	531	2.0	1146	0.463	100	8.1	LOS A	3.4	24.5	Full	500	0.0	0.0
Approach	1001	2.0		0.463		8.5	LOS A	3.4	24.5				
West: EB Eas	t Access												
Lane 1 (L) <sup>d</sup>	259	2.0	940	0.275	100	6.7	LOS A	1.4	10.3	Full	50	0.0	0.0
Lane 2 (R)	200	2.0	765	0.261	100	7.7	LOS A	1.3	9.1	Full	50	0.0	0.0
Approach	459	2.0		0.275		7.1	LOS A	1.4	10.3				
Intersection	3141	3.3		0.709		11.0	LOS B	8.0	58.3				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

d Dominant lane on roundabout approach

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